



**Development of Plant Growth Model and
Computer Software to Control Environmental
Conditions to get Yield**

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가

· (,)

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· (computer)

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가 .

(dynamical mathematic model)

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dynamic

optimal control theory

가

가

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,

(dynamical mathematic model of crop growth and

development)

,

,

가 (validation of model),

가 (expert system) ,

Optimal control theory ,

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1.

· ,
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2.

1)

2)

3)

4) , , CO2

가

5)

6)

7) N

가

8) 가

9)

10)

11)

1.

가.

, 1-2W 가
 1-2W 가 , 6 14
 가 1-2W , 7 12
 1-2W 가 .
 가
 ,
 1-2W 가 ,
 . 10 4 1-2W 가
 , 11 1 .
 .
 , 1-2W
 , 가 8 9

(2)
 1-2W 20cm 53.7kg 가
 , 49.9kg , 1-2W
 가 . (5) 1-2W

, , 15cm(34 /bench)
 25cm(20 /bench) 가 , 15cm 20cm(26 /bench)
 20cm 25cm 가 .
 15cm 20cm 25cm ,
 15cm 20cm 가 .
 15cm 20cm .

, , 가
 , 가 40% .
 20% ,

가 가 가 , 가
 , 가 가

, 가 , 가 .

가, , 가 ,
 가, 가

, , CO2 가

10 $20\mu\text{mol s}^{-1}\text{m}^{-2}$, $700\mu\text{mol s}^{-1}\text{m}^{-2}$

$$\text{GPR} = 21.4512 \text{ PPF} / (287.784 + \text{PPF})$$

가 , 24 32 . CO2
20 40ppm , CO2 1200 1300ppm ,

$$\text{GPR} = 15.5554 (1 - 0.9636 \exp(-0.0024 \text{ CO}_2))$$

가 가 가 ,
가 logistic

$$\text{GPR} = 24.743 / (1 + 6.0343 \exp(-0.3689 \text{ N}))$$

, , CO2 (GPR)

$$\text{GPR} = 69.4119T / (7.5397 + T) \cdot \text{PPF} / (240.149 + \text{PPF}) \\ (1 - 0.8865 \exp(-0.0018 \text{ CO}_2)) \cdot (1 + 5.1729 \exp(-0.4161 \text{ N}))$$

가 ,
(Resp)

$$\text{Resp} = 0.0734 dW/dt + 7.6618 \exp(0.093 \text{ temp}) \cdot W$$

14.6%

0.5552g CH₂O/(gN)

(LDW) 0.3427 (Ws)
(t)가

$$LDW = (0.7372 - 0.00193t) W_s$$

(LAI), (LDW) (PS)
LAI = (11.831 + 1.6832 LDW) / PS 가
(Pg)

$$Pg = \int_0^{LAI} GPR \, dl$$
$$= 69.4119T / (7.5397 + T)(1 - 0.8865 \exp(-0.0018 CO_2))$$
$$1 / (1 + 5.1729 \exp(1 - 0.4161N)) \cdot \int_0^{LAI} I / (240.1694 + I) dt$$

가
가 N

가 ,

가

가

4 5 g d-1 가 ,

20 , 2

가

가

가

50%

15%

133mg CH₂O h-1

Simplex , Runge-

Kutta fourth-order , , ,

가

가

simulation 73 y gm-2

$$y + 218.5275 = 0.2170 \text{ Rad} + 29.7863 \text{ Temp} + 0.1271 \text{ CO}_2$$

$$+ 0.0032 (\text{Rad})(\text{Temp}) - 0.000034 (\text{Rad})(\text{CO}_2) + 0.00167 (\text{Temp})(\text{CO}_2) \\ - 0.000113 (\text{Rad})^2 - 0.4316 (\text{Temp})^2 - 0.00006 (\text{CO}_2)^2$$

(RS485)

10

MS Visual BASIC

가

가

2.

1. (, , , CO2 , N , pH EC)

2. ,
2 , 가 가
output 가 input 가

SUMMARY

The region around Sunchon in Chonnam province produces about 90% of cucumber crop in Republic of Korea, and most of the cucumber fruits are produced in greenhouse or glasshouse. To maximize the profits from the crops grown in the closed environmental condition, such as greenhouse or glasshouse, it is necessary to know how the climatic conditions varies inside the closed system, how the crops inside the closed system will response to the environmental conditions, how to sense and control the climatic condition automatically by computer through opening or closing side windows, screens and burning oils etc., and how to get an optimal yields of the crop by proper management of environmental control system. Knowing all of these will finally help farmers to save human labors, prevent environment from pollution, and save fuel energy.

The purpose of the study consist of investigating the temporal and spatial variations of climatic factors inside two differant types of greenhouse, investigating how cucumber plants response to the varying environmental conditions, developing mathematical growth and yield model of cucumber crop by investigating plant response to environmental conditions, conducting validation of the model, gathering the experiances from experts in cucumber cultivation, constructing optimal environmental conditions for the cucumber growth by optimal control theory, and finally developing EXPERT system for the cucumber cultivation. The results are summarized as follows

1. Effects of environmental conditions on the growth of cucumber plants

In summer growth period of cucumber, two types of greenhouse, 1-2w and postless, showed significantly different irradiance inside the house. 1-2w type showed highly significantly greater irradiance than that of postless type for the whole growing period. Leaf dry weight of the plants

grown in 1-2w type greenhouse appeared to be significantly higher than that of the plants in postless greenhouse. The plants grown in postless type showed larger leaf area than those in 1-2w type at the earlier growth stage, but at the later growth stage, the plants in 1-2w type showed large leaf area.

Average daily mean temperature for the whole growth period showed significantly positive correlation coefficient with relative growth rate, and also net assimilation rate correlated positively with leaf nitrogen content. Accumulated temperature can be used to predict how many leaves emerge and when plants start to flower.

In autumn growth period of cucumber, 1-2w type greenhouse showed significantly higher irradiance than postless type greenhouse, but there was no significant differences in leaf dry weight between the plants. At the later stage of growth, plants in postless greenhouse showed larger leaf area, which seemed to be attributed from the difference in irradiance. 1-2w type greenhouse showed higher irradiance inside the house, so that plants grown in 1-2w type showed higher net assimilation rate, while plants grown inside postless type had larger specific leaf area. Number of leaves can be predicted accurately by the accumulated temperature, and plants began to flower when number of leaves was 8 or 9.

2. Effects of planting space on growth and yield of cucumber plants

In spring growth period, there was no significant differences in yield among plant densities, but as plant density became greater, yield increased progressively. Postless type greenhouse showed too higher air temperature as time passed, so that 1-2w type showed higher fruit yield than postless

type. In summer growth period, treatment of planting space, 15cm showed significantly higher fruit yield compared with that of plating space, 25cm. Judging from the results, the proper planting space in cucumber seemed to be existed from 15cm to 20cm of planting space.

3. Variation in sex expression of several varieties of cucumber due to different growth periods.

In autumn growth period, varietal group, Hukjinjoo and cultivar Ibchubakdadaki showed the higher ratio of female flowers, cultivar Jangilnakhap showed relatively higher ratio of female flowers, and cultivar Gaulnakhap showed more or less lower ratio of female flowers. However, varietal group of Hukjinjoo showed fruit abortion more than 20%, while cultivar Jangilnakhap had few aborted fruits, so that Jangilnakhap would have a higher yield potential than varietal group, Hukjinjoo. In the earlier winter growth period, cultivar Ibchubakdadaki showed the greatest number of female flowers per plant and varietal group, Chungjang showed the lowest ratio of female flowers. In the later winter growth period, varietal group, Banbak and Hukjinjoo showed higher ratio of female flowers, and group Chungjang showed lower ratio of female flowers. In summer growth period, varietal group Hukjinjoo showed highest number of female flowers, and varietal group Chungjang also the lowest number of female flowers.

In general, ratio of female flowers strongly positively correlated with the number of aborted fruits. Yields of varieties were determined by several factors such as ratio of female flowers, ratio of aborted fruits, cold tolerance or heat tolerance. Varieties in group Hukjinjoo were susceptible to low temperature so that they were not proper to grow at the growing

season with low temperature. Judging from the results, varieties in group Nakhap, Hukjinjoo or Ibchubakdadaki were proper to grow in the autumn growth period, cultivar Chungjang, Ibchubakdadaki and Gaulnakhap were proper to the earlier winter growing season, varieties in group Chungjang and Nakhap were proper to the later winter growing season, and cultivar Namboochungjang or Gaulnakhap were proper to the summer growing season.

4. Effects of irradiance, temperature, CO₂ concentration and leaf nitrogen content on photosynthetic rate

The light compensation point was 10 20 μmol m⁻² s⁻¹ and light saturation point was higher than 700 μmol m⁻² s⁻¹. Gross photosynthetic rate (GPR) was dependent on the amount of solar radiation (PPF) and could be expressed as an equation

$$\text{GPR} = 21.4512 \text{ PPF} / (287.784 + \text{PPF})$$

The rate of photosynthesis increased as temperature increased, however, no significant changes in the rate was observed in a temperature range of 24 to 32 . CO₂ compensation point was 20 40ppm and CO₂ saturation point was 1200 1300ppm. The effect of CO₂ concentration on gross photosynthetic rate could be expressed as an equation,

$$\text{GPR} = 15.5554 (1 - 0.9636 \exp(-0.0024 \text{ CO}_2))$$

Gross photosynthetic rate increased logistically as leaf nitrogen content increased, and could be expressed as an equation,

$$\text{GPR} = 24.743 / (1 + 6.0343 \exp(-0.3689 \text{ N}))$$

The effects of solar radiation, temperature, atmospheric CO₂ concentration

and leaf nitrogen content could be summarized as an equation,

$$\text{GPR} = 69.4119 \frac{T}{(7.5397 + T)} \cdot \text{PPF} / (240.149 + \text{PPF}) \cdot (1 - 0.8865 \exp(-0.0018 \text{ CO}_2)) \cdot (1 + 5.1729 \exp(-0.4161 \text{ N}))$$

5. Effects of environmental factors on respiration rate

Respiration rate increased as temperature increased, and the respiration rate of a whole plant could be expressed as an equation,

$$\text{Resp} = 0.0734 \frac{dW}{dt} + 7.6618 \exp(0.093 \text{ Temp}) \cdot W$$

Total respiration rate of plant comprised 14.6% of the gross photosynthetic rate of plant. At night, the respiration rate decreased as time passed, which seemed to be due to the decrease in the level of respiration substrates in the plant, especially starch concentration. Energy cost for nitrogen uptake in root was estimated to be 0.5552 g CH₂O (g N)⁻¹.

6. Gross photosynthetic rate in the plant community

The extinction coefficient in the cucumber community was estimated to be 0.3427. The ratio of leaf dry weight (LDW) to shoot dry weight (Ws) decreased as the plant grew, and estimated to be

$$\text{LDW} = (0.7372 - 0.00193 t) W_s, \text{ (t in days after transplant).}$$

Leaf area index (LAI) can be estimated by LDW and planting space (Ps),

$$\text{LAI} = (11.831 + 1.6832 \text{ LDW}) / P_s$$

By using these estimates, gross photosynthetic rate (Pg) in a community could be expressed as the following equation

$$P_g = \int_0^{LAI} GPL(I) dl,$$

where l is the cumulative leaf area index.

7. Effects of day/night temperature change, nitrogen concentration in nutrient solution and irradiance on cucumber growth

No significant effects of day/night temperature change on cucumber growth was observed. When effects of nitrogen concentration in nutrient solution and irradiance on shoot:root ratio were compared, the ratio could relatively easily be predicted by the hypothesis of functional equilibrium. In all the experimental conditions, exponential growth model was found to be appropriate to describe the growth of plant organs.

8. Characteristics of the increase in fruit dry weight

The increase in fruit dry weight was determined by a nondestructive measuring method. During the rapid growth of fruit, dry weight increased at a rate of 4–5 g d⁻¹. This amount was equivalent to the amount of photosynthetic product by 20 leaves, and was equivalent to the amount of assimilate demand for two fast growing fruits. The increase of fruit dry weight could easily be predicted by an exponential growth curve.

9. Photosynthesis, respiration in fruits, and translocation rate of assimilate from shoot to fruit

The photosynthetic and respiration rate in fruits increased as temperature increased, and respiration rate was more sharply increased by temperature than photosynthetic rate. The amount of photosynthesis in fruits could compensate only 50% of the energy loss caused by respiration in fruits. The amount of respiration in fruit was equivalent to 15% of the amount of

assimilate translocated to fruit from shoot. The translocation rate of assimilate to fruits from shoot was about 133 mg CH₂O h⁻¹.

10. Mathematical model of growth and yield for the cucumber plant

Mathematical model for cucumber growth and yield was obtained by using the hypothesis of functional equilibrium. In the process, parameters were estimated by Simplex method, and the solutions for the system of differential equations were obtained by Runge-Kutta fourth-order method. In the validation process, predicted values for leaf, stem, root and fruit agreed fairly well with the actual measured values. Therefore, the model could be used to predict plant growth in controlled environmental condition. In a simulation study for finding an optimal environmental conditions, the yield contour surface to obtain yield of Y(g m⁻²) for 73 days after transplant was found to be expressed as the following equation.

$$Y+218.5275 = 0.2170 \text{ Rad} + 29.7863 \text{ Temp} + 0.1271 \text{ CO}_2 + \\ 0.0032 (\text{Rad})(\text{Temp}) - 0.000034 (\text{Rad})(\text{CO}_2) + 0.00167 (\text{Temp})(\text{CO}_2) - \\ 0.000113 (\text{Rad})^2 - 0.4316 (\text{Temp})^2 - 0.00006 (\text{CO}_2)^2$$

11. Environmental measurement and control in cultivation under structure

A measurement and control system was developed based on RS485 serial communication. The measurement system automatically saves environmental data on both outside and inside of greenhouse to a set of databases at intervals of 10 minutes.

The measurement and control software was written in MS Visual BASIC as a Windows application. The real-time greenhouse environment and saved data can be displayed on the monitor screen as numerical data or graphical form.

Spatial distribution of solar radiation under various environmental conditions were analyzed. Also ventilation rates of greenhouses were measured for various settings of top and side vent openings. The practice of cucumber growers in environment control and cultivation was investigated and the results were utilized in developing the control algorithm.

The greenhouse environment can be controlled in manual or automatic mode by user's selection. In automatic mode, the various environmental factors and the stage of cucumber growth were incorporated to maintain optimum settings.

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3	33
2	55
1	55
2	55
3	56
3	67
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4 , , CO2 가	79
1	79
2	80
3	81

5		93
1		93
2		93
3		94
6		103
1		103
2		103
3		104
7	N	가	. 111
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2		129
3		130
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2		139
3		140
10		147

1	147	
2	148	
3	166	
11	175	
1	175	
2	176	
3	186	
4	가	209
5	212	
12	231	
	237	
A.	가	241
B.	245	

가 .
 300ppm 가 가 , 가
 3 5 900 1500ppm .
 , , , , ,

2

1. 1996

1996 5 3 10
 30 가 5 10
 . 1 2 5 23
 5 31 1 7 5
 , , , .
 , glucose .
 가 4
 가 .
 1-2W 2 .
 15m 24m , 1-2W 2 14
 m 26m . ELDER- GAL GAL
 compact 1996 4 22
 6 ,
 4 , 20 .

pH 5.9 6.2가
 , EC 2.2

1. (: ppm)

Ca	Mg	K	NH4	NO3	PO4	SO4	Fe	Mn	Cu	Zn	B	Mo
162	50	314	19	226	42	65	3	0.5	0.02	0.05	0.5	0.01

1 50ml 7 5 30 21
 1 1050ml ,
 가 .
 4 (, ,
 ,) 6
 가 , 가 10
 , , , , ,
 PC .

1- 2W

I	II
IV	III

I	II
IV	III

(RGR : relative growth rate, g g-1 d-1), (NAR : net assimilation rate, g dm-2 d-1), (LAR : leaf area ratio, dm g-1), (SLA : specific leaf area , dm g-1), (LWR : leaf weight ratio, g g-1), (CGR : crop growth rate, g m-2 d-1), (LAI : leaf area ind

ex), (RGRA : relative growth rate of leaves, dm² dm⁻²
d-l), (RARN, relative accumulation rate of nitroge
n, g N g⁻¹N)

$$RGR = (\ln W_2 - \ln W_1) / (t_2 - t_1),$$

$$NAR = (W_2 - W_1)(\ln A_2 - \ln A_1) / ((A_2 - A_1)(t_2 - t_1))$$

$$CGR = 1/P * (W_2 - W_1) / (t_2 - t_1),$$

$$NAR = (W_2 - W_1) / (A_2 - A_1) \times (\ln A_2 - \ln A_1) / (t_2 - t_1),$$

$$LAR = (A_1 + A_2) / (W_1 + W_2),$$

$$SLA = (A_1 + A_2) / (LW_1 + LW_2),$$

$$LWR = (LW_1 + LW_2) / (W_1 + W_2),$$

$$RGRA = (\ln A_2 - \ln A_1) / (t_2 - t_1)$$

$$RARN = (\ln N_2 - \ln N_1) / (t_2 - t_1)$$

Wi, Ai, Li, Ni, LW1 ti
, , , N , P
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, 10 .

2. 1996

1996 8 31 10 30
가 9 7

1
9 16 , 9 20 1
1

3

1. 1996

가.

, ,
, 1-1 ,

1-2W 가 1-2W
3

, 1-2W
2 가 , 3

, ,
1-2 .

1-2. 1996

		()	(%)	(mmol m-2 d-1)
1-2W	1	25.43	62.85	128.04
	2	25.87	68.21	142.64
	3	25.54	62.18	126.77
	4	25.61	69.24	131.88
	1	25.17	63.41	104.63
	2	25.68	59.35	92.02
	3	26.20	65.95	107.31
	4	25.75	68.72	98.60

, ,
 1-3 . 5
 5
 6 7 6 14
 가 1-2W
 가 6 14
 가 1-2W 7 12 1-2W
 가

1- 1. , ,

			()	(%)	(mmol m-2 d-1)
5/24 5/31	1- 2W	1	26.15	55.33	27.50
		2	26.58	56.96	30.31
		3	27.40	49.04	27.95
		4	26.47	57.77	29.63
		1	26.20	53.84	23.22
		2	27.59	47.59	20.40
		3	28.03	49.49	23.16
		4	26.70	57.91	24.64
6/ 1 6/ 7	1- 2W	1	26.45	54.11	26.40
		2	26.82	58.34	29.89
		3	26.11	54.23	27.40
		4	26.84	61.64	28.49
		1	26.10	55.97	22.37
		2	26.33	50.49	20.95
		3	26.78	59.22	22.86
		4	26.53	60.12	20.21
6/ 8 6/14	1- 2W	1	24.69	68.58	17.64
		2	25.07	73.14	19.53
		3	25.04	68.46	17.11
		4	24.74	74.45	17.68
		1	24.42	67.40	14.18
		2	24.78	63.40	12.43
		3	25.29	71.52	14.70
		4	24.98	73.15	12.25
6/15 6/22	1- 2W	1	25.53	66.55	20.52
		2	26.03	72.23	22.83
		3	25.32	65.92	19.80
		4	25.72	73.18	20.47
		1	25.27	67.20	16.28
		2	25.69	63.58	14.27
		3	26.14	71.10	17.03
		4	25.84	73.29	15.06

1- 1.

			()	(%)	(mmol m-2 d-1)
6/23 6/28	1- 2W	1	24.20	69.19	18.28
		2	24.63	75.64	19.87
		3	24.04	68.57	16.76
		4	24.28	75.58	17.32
		1	23.81	69.53	13.84
		2	24.23	66.99	11.51
		3	24.76	73.83	14.70
		4	24.45	76.55	12.70
6/29 7/ 5	1- 2W	1	25.74	62.96	17.70
		2	26.30	72.46	20.21
		3	25.50	66.46	17.75
		4	25.78	72.49	18.29
		1	25.41	66.18	14.74
		2	25.70	63.55	12.46
		3	26.39	70.14	14.86
		4	26.17	70.86	13.74
7/ 6 7/12	1- 2W	1	26.87	49.64	26.05
		2	25.00	64.31	32.72
		3	24.29	59.91	29.80
		4	24.73	65.85	30.56
		1	24.21	60.89	23.45
		2	24.61	57.22	21.69
		3	25.15	64.45	23.82
		4	24.74	67.62	22.15

1- 3.

			(cm)	(plant-1)	(dm ² /plant)	(g/plant)	(g/plant)	(g/plant)
5 31	1-2W	1	20.5	5.6	6.1	1.8	.6	-
		2	19.4	5.4	5.6	2.0	.6	-
		3	20.3	5.4	5.9	2.0	.7	-
		4	18.3	5.2	5.3	1.6	.5	-
		1	18.2	5.6	5.3	1.5	.4	-
		2	19.8	5.8	5.8	1.7	.5	-
		3	17.0	5.2	4.7	1.5	.4	-
		4	18.5	5.4	5.7	1.8	.5	-
6 7	1-2W	1	49.3	11.4	14.9	4.7	2.0	-
		2	52.2	11.2	14.5	5.1	2.2	-
		3	63.6	12.0	18.8	6.6	2.9	-
		4	54.7	11.6	16.8	5.5	2.6	-
		1	63.8	12.0	19.0	6.2	2.7	-
		2	55.7	11.6	17.4	5.4	2.4	-
		3	53.5	11.0	17.2	5.3	2.4	-
		4	52.5	11.0	17.5	5.6	2.4	-
6 14	1-2W	1	105.3	17.8	35.5	12.2	5.8	-
		2	102.0	17.0	34.0	10.7	5.2	-
		3	114.0	17.6	40.3	13.2	6.2	-
		4	93.0	15.2	36.4	12.0	5.4	-
		1	110.2	17.8	42.2	13.0	6.1	-
		2	114.2	18.4	43.6	12.4	5.9	-
		3	106.2	15.6	38.3	10.2	4.8	-
		4	117.5	18.0	46.9	13.2	6.4	-
6 22	1-2W	1	180.7	25.8	74.2	26.6	9.4	6.6
		2	177.6	23.6	71.5	25.9	8.2	13.3
		3	182.2	24.2	71.9	26.6	10.5	15.9
		4	180.4	24.4	75.8	27.4	10.2	8.3
		1	184.9	24.6	78.2	24.5	10.0	7.5
		2	171.9	22.2	73.5	22.4	10.1	8.7
		3	177.5	23.6	73.0	23.2	9.2	8.0
		4	190.0	24.8	81.8	26.0	9.9	6.5

1- 3.

			(cm)	(plant-1)	(dm ² plant)	(g/plant)	(g/plant)	(g/plant)
6 28	1- 2W	1	212.4	29.2	93.7	26.4	17.0	84.4
		2	225.8	28.8	101.6	29.0	18.1	330.2
		3	232.2	28.4	105.5	30.0	19.4	93.5
		4	232.9	29.0	109.0	31.4	20.5	97.4
		1	240.0	30.0	110.9	27.8	17.9	78.2
		2	236.9	28.8	107.8	27.6	18.0	96.0
		3	228.6	26.8	101.1	26.7	15.9	88.3
		4	226.0	27.0	104.8	25.4	17.1	36.4
7 5	1- 2W	1	245.8	31.8	110.1	43.4	20.7	557.1
		2	249.5	33.4	117.4	45.0	20.9	602.3
		3	272.6	33.8	122.6	45.1	23.2	782.3
		4	258.6	31.8	107.8	40.2	20.8	586.2
		1	261.0	30.8	102.3	36.9	18.9	393.6
		2	276.7	31.6	120.9	42.0	20.3	504.4
		3	270.1	31.2	114.6	36.6	19.4	426.4
		4	263.5	32.2	115.1	39.9	19.9	454.7
7 12	1- 2W	1	268.4	32.6	103.6	45.2	22.2	1301.6
		2	284.5	33.8	108.8	42.1	22.4	697.9
		3	287.0	33.2	109.6	40.4	19.9	994.0
		4	278.2	31.8	98.6	36.3	19.3	1120.8
		1	281.6	32.0	85.5	34.2	16.4	937.3
		2	292.8	29.0	90.7	31.3	19.7	1304.8
		3	285.7	32.8	96.3	35.1	19.6	1056.9
		4	301.6	32.6	95.6	33.6	18.8	923.1

1- 4

가

(RARN)

(RGR)

(1- 5).

1-4. , , (%)

			5/31	6/ 7	6/14	6/22	6/28	7/ 5	7/15
			1-2W	1	5.736	5.006	4.350	4.242	3.828
	2	5.756	4.772	4.268	4.295	3.938	3.916	3.120	
	3	5.186	4.862	4.513	4.439	4.222	4.076	3.776	
	4	5.418	4.102	4.852	4.234	3.952	3.778	3.300	
	1	5.434	4.570	4.568	4.199	3.850	3.944	2.830	
	2	6.334	4.614	3.528	4.260	3.895	3.928	3.262	
	3	5.636	4.920	4.355	4.293	3.934	3.616	3.298	
	4	5.296	4.866	4.622	4.423	4.168	3.807	3.776	
	1-2W	1	3.904	4.210	4.136	2.708	4.005	3.230	3.208
		2	4.160	4.172	4.038	2.762	3.658	3.372	3.384
		3	4.540	4.540	4.476	3.048	3.980	3.440	3.476
		4	4.168	4.060	4.432	3.158	4.232	3.892	3.404
		1	4.288	4.514	4.568	3.076	3.418	3.392	2.582
		2	4.540	4.236	4.100	3.120	3.806	3.953	3.262
		3	4.618	4.348	4.124	3.078	4.344	4.108	3.270
		4	4.506	4.312	4.316	2.788	3.704	3.760	2.824

1-5

. CGR LAI
. CGR
가 7 6 7 12
6 8 LAI SLA
1-2W
가 ,

RGR (RGR) 가 (Harvest index)가
 가 RGR
 1-6 RGR, NAR LAR

$$RGR = NAR \times LAR$$

(NAR,)
 (LAR) 가

$$RGR = 0.9149 NAR + 0.1256 LAR, \quad (R^2 = 0.9826, df=45)$$

RGR 가 LAR NAR

(NAR) (LN) 가

NAR LN Fig. 1-1 LN 가

NAR 가 (LAR)

(SLA) (LWR) 가

$$LAR = SLA \times LWR$$

LAR SLA LWR

$$LAR = 0.5116 SLA + 0.6936 LWR, \quad (R^2 = 0.9970)$$

LAR LWR 가

1- 5.

			RGR	NAR	LAR	SLA	LWR	CGR	LAI	RGRA	
			RARN								
6 7	1- 2W	1	.1427	.0617	2.2831	3.2049	.7124	1.6356	.2830	.1288	.1287
		2	.1495	.0727	2.0264	2.8194	.7187	1.8377	.2714	.1361	.1262
		3	.1791	.0871	2.0211	2.8776	.7024	2.6165	.3330	.1645	.1717
		4	.1921	.0860	2.1586	3.1199	.6919	2.3204	.2989	.1645	.1605
		1	.2176	.0929	2.2385	3.1338	.7143	2.6875	.3280	.1836	.1990
		2	.1817	.0756	2.3326	3.2793	.7113	2.1500	.3123	.1569	.1425
		3	.1998	.0859	2.2831	3.2645	.6994	2.2371	.2960	.1857	.1813
		4	.1791	.0779	2.2515	3.1513	.7145	2.2086	.3131	.1614	.1667
6 14	1- 2W	1	.1407	.0678	2.0417	2.9808	.6849	4.3439	.6804	.1238	.1253
		2	.1107	.0536	2.0849	3.0676	.6796	3.3137	.6552	.1217	.0977
		3	.1020	.0502	2.0436	2.9919	.6830	3.8180	.7970	.1093	.0939
		4	.1082	.0519	2.0893	3.0444	.6863	3.5550	.7190	.1104	.1288
		1	.1089	.0500	2.1848	3.1821	.6866	3.9275	.8260	.1136	.1093
		2	.1228	.0529	2.3412	3.4284	.6829	4.0686	.8230	.1317	.0953
		3	.0944	.0391	2.4536	3.5989	.6818	2.7823	.7491	.1140	.0799
		4	.1273	.0551	2.3399	3.4415	.6799	4.4434	.8702	.1407	.1219
6 22	1- 2W	1	.1011	.0503	2.0144	2.8289	.7121	7.1332	1.4805	.1053	.0837
		2	.1122	.0538	2.0736	2.8806	.7198	7.3337	1.4244	.1061	.0996
		3	.0957	.0484	1.9587	2.8257	.6932	7.1332	1.5146	.0828	.0772
		4	.1126	.0553	2.0212	2.8478	.7098	8.0278	1.5150	.1046	.0849
		1	.0866	.0390	2.2236	3.2074	.6933	6.1384	1.6240	.0882	.0610
		2	.0847	.0369	2.2793	3.3646	.6774	5.7066	1.5811	.0746	.0894
		3	.1135	.0481	2.3202	3.3302	.6967	6.9790	1.5011	.0921	.0995
		4	.0886	.0382	2.3054	3.2885	.7010	6.4700	1.7379	.0794	.0683
6 28	1- 2W	1	.0328	.0161	2.0385	3.1690	.6433	3.6244	2.2657	.0333	.0288
		2	.0528	.0261	2.0234	3.1535	.6417	6.0305	2.3364	.0502	.0421
		3	.0455	.0231	1.9712	3.1388	.6280	5.4752	2.3941	.0547	.0438
		4	.0508	.0255	1.9950	3.1417	.6350	6.2849	2.4947	.0519	.0500
		1	.0443	.0194	2.2844	3.6149	.6319	4.9046	2.5514	.0499	.0328
		2	.0531	.0238	2.2360	3.6238	.6170	5.7451	2.4472	.0547	.0468
		3	.0440	.0197	2.2332	3.4881	.6402	4.5884	2.3489	.0466	.0437
		4	.0269	.0116	2.3272	3.6331	.6406	2.9073	2.5182	.0353	.0244

1- 5.

			RGR	NAR	LAR	SLA	LWR	CGR	LAI	RGRA	RARN
7	1- 2W	1	.0733	.0432	1.6635	2.9182	.5700	11.8604	2.7505	.0231	.0357
		5	.0705	.0422	1.6409	2.9611	.5542	12.4542	2.9563	.0207	.0452
		3	.0768	.0465	1.6143	3.0397	.5311	14.2896	3.0775	.0215	.0371
		4	.0490	.0294	1.6517	3.0296	.5452	8.5984	2.9258	-.0017	.0144
7	1- 2W	1	.0467	.0248	1.8708	3.2945	.5678	7.1178	2.8766	-.0115	.0316
		2	.0661	.0353	1.8408	3.2864	.5601	10.8810	3.0859	.0163	.0473
		3	.0616	.0321	1.8914	3.4092	.5548	9.3387	2.9114	.0179	.0285
		4	.0729	.0379	1.8807	3.3669	.5586	11.2512	2.9670	.0134	.0423
12	1- 2W	1	.0331	.0267	1.2338	2.4103	.5119	7.6962	2.8845	-.0087	-.0036
		2	.0175	.0136	1.2812	2.5970	.4933	4.1643	3.0533	-.0109	-.0246
		3	-.0068	-.0051	1.3328	2.7154	.4908	-1.5886	3.1331	-.0160	-.0243
		4	.0062	.0047	1.3150	2.6978	.4874	1.3033	2.7852	-.0126	-.0320
7	1- 2W	1	.0070	.0051	1.3835	2.6395	.5242	1.2801	2.5341	-.0256	-.0580
		2	-.0202	-.0137	1.4854	2.8872	.5145	-3.8712	2.8545	-.04111	-.0551
		3	.0186	.0131	1.4258	2.9423	.4846	3.7170	2.8462	-.0249	-.0233
		4	.0113	.0082	1.3851	2.8652	.4834	2.3135	2.8428	-.0266	-.0327

1- 6.

	NAR	LAR	SLA	LWR	CGR	LAI	RGRA	RARN
RGR	0.9858**	0.6421**	0.1826	0.7911**	-0.0405	-0.8813**	0.9404**	0.9694**
NAR		0.5642**	0.1014	0.7450**	0.0711	-0.8338**	0.9009**	0.9477**
LAR			0.7600**	0.8770**	-0.0524	-0.6800**	0.7736**	0.7431**
SLA				0.3587**	0.0976	-0.1470	0.2691	0.2839
LWR					-0.1119	-0.8577**	0.9088**	0.8635**
CGR						0.3832**	-0.1882	-0.0548
LAI							-0.9484**	-0.8912**
RGRA								0.9634**

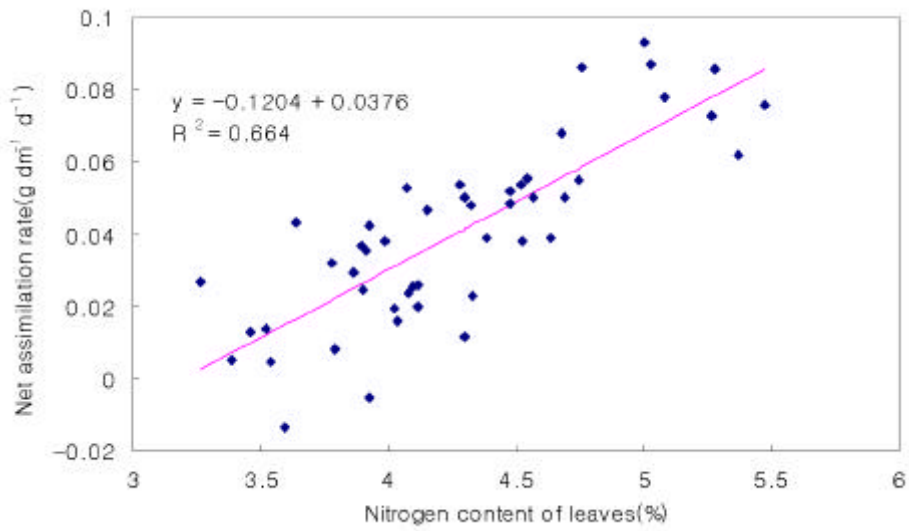


Fig. 1-1. Relationship between net assimilation rate and nitrogen content of leaves

(RGR) (NAR)
 \bar{N} (1-7),
 (DSR, Daily Solar Radiation) LAR SLA

$$\text{LAR} = 2.5975 - 0.00025 \text{ DSR}, \quad (R^2 = 0.2663, \text{ DF} = 46)$$

$$\text{SLA} = 3.9001 - 0.00031 \text{ DSR}, \quad (R^2 = 0.6003, \text{ DF} = 46)$$

1-7.

	RGR	NAR	LAR	SLA	LWR	CGR	LAI	RGRA	RARN
	0.600**	0.641**	0.105	-0.125	0.249	0.247	-0.349*	0.380*	0.488**
	0.061	0.087	-0.516**	-0.773**	-0.188	-0.395*	-0.101	-0.016	-0.050

(translocation)

(Accumulated temperature ; AT)

AT = 1260

가 8 10

Fig. 1-2

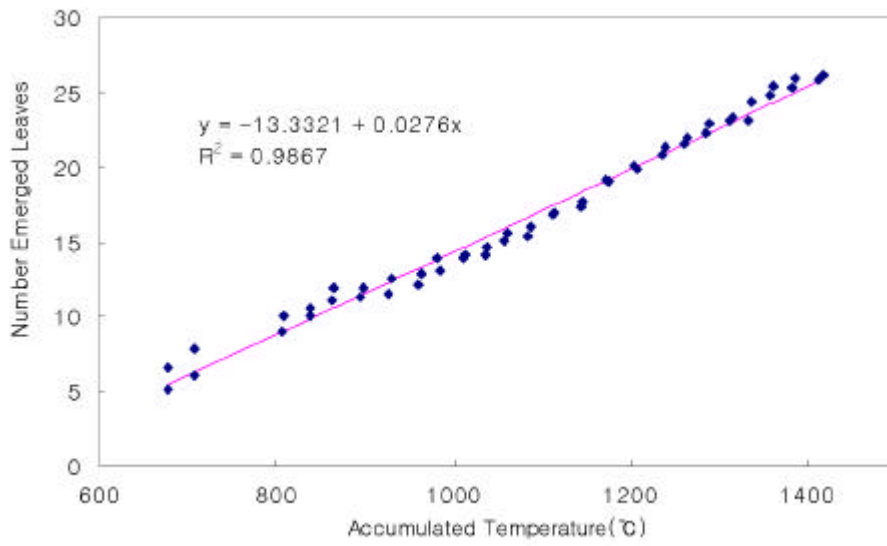


Fig. 1-2. Comparisons of observed and predicted number of emerged leaves

7 5 7 12 2
가 1-8 가

1- 9. 1996 9

			()	()	()	(%)	(%)	(%)	(mmol m-2l-1)
9/20	1-2w	1	27.84	18.87	41.09	33.10	8.66	55.83	22.6
9/26		2	25.58	17.57	36.35	44.47	11.75	69.95	33.1
		3	27.99	18.81	41.67	36.16	8.56	57.26	28.9
		4	25.14	16.97	36.65	49.61	28.11	69.95	32.6
		1	25.25	17.39	36.58	41.87	13.07	62.82	23.2
		2	25.88	17.94	37.35	37.35	10.02	58.11	21.7
		3	26.25	18.33	37.19	42.52	11.34	65.12	20.9
		4	28.73	20.25	41.40	39.54	10.15	59.52	20.6
9/27	1-2w	1	26.12	19.79	35.43	38.10	12.36	57.73	17.5
10/ 4		2	24.07	18.63	31.49	53.46	31.91	71.55	23.8
		3	26.15	19.88	35.74	42.56	20.51	58.53	19.4
		4	23.50	17.97	31.45	55.74	35.97	71.57	22.6
		1	23.54	18.27	31.01	50.34	33.11	64.48	16.0
		2	24.09	18.82	31.44	45.59	27.47	60.29	14.5
		3	24.51	19.30	31.46	51.94	32.63	67.22	15.5
		4	26.77	21.01	35.08	47.46	29.05	61.87	14.1
10/ 5	1-2w	1	21.70	15.66	31.47	44.54	15.56	61.48	18.5
10/11		2	20.16	14.35	28.66	58.76	29.39	74.43	23.7
		3	21.83	15.75	31.92	47.82	21.36	61.66	19.5
		4	19.76	14.10	28.49	60.41	36.26	73.04	22.6
		1	20.17	15.21	27.53	54.45	32.02	66.40	15.7
		2	20.56	15.48	28.11	50.24	26.91	63.15	14.3
		3	20.94	15.99	28.26	56.94	32.04	69.95	15.3
		4	22.77	17.36	31.17	52.85	28.82	66.13	13.7
10/12	1-2w	1	22.14	16.06	29.72	43.06	12.68	64.60	23.9
10/18		2	23.21	16.65	31.12	50.08	21.70	71.08	26.5
		3	22.11	15.98	29.64	48.44	21.05	65.88	23.4
		4	22.44	16.12	31.13	53.70	31.90	71.34	25.2
		1	21.38	15.85	31.14	53.67	25.33	67.93	18.0
		2	21.89	16.27	31.47	49.41	20.33	65.29	16.1
		3	22.23	16.73	31.41	55.69	24.71	71.95	16.9
		4	21.82	16.41	31.12	59.31	27.98	74.95	15.5

1- 9.

			()	()	()	(%)	(%)	(%)(mmol m-2 d-l)		
10/19 10/25	1-2w	1	21.98	16.71	28.21	46.94	21.67	68.56	22.3	
		2	23.41	17.73	30.10	56.20	32.30	74.81	24.5	
		3	21.86	16.56	28.03	55.75	33.18	70.47	21.9	
		4	22.66	17.02	29.86	59.46	36.58	75.42	23.3	
	10/26 11/01	1-2w	1	22.41	16.68	31.41	53.05	30.32	67.25	16.8
			2	21.55	16.10	29.26	54.14	30.93	67.94	15.0
			3	23.34	17.64	31.83	55.83	31.53	71.34	14.4
			4	21.48	16.01	28.46	63.47	39.22	76.21	14.4
10/26 11/01	1-2w	1	20.18	14.49	28.43	39.40	19.86	57.92	20.4	
		2	21.76	15.60	31.38	50.18	25.45	68.24	21.5	
		3	20.07	14.38	28.32	50.22	28.36	65.92	18.8	
		4	21.00	14.94	30.60	54.50	35.66	69.61	19.7	
	10/26 11/01	1-2w	1	20.48	14.30	29.49	49.03	28.79	65.61	17.2
			2	23.68	16.81	35.16	38.26	16.20	54.41	12.4
			3	21.39	15.24	29.84	50.13	27.92	69.12	13.3
			4	20.93	14.91	29.15	53.21	30.53	71.52	12.4

1- 10.

			()	()	()	(%)	(%)	(%) (mmol m-2 d-l)		
1-2W		1	23.3	16.9	32.4	40.9	15.1	61.0	125.2	
		2	23.0	16.8	31.5	52.2	25.4	71.7	153.1	
		3	23.3	16.9	32.6	46.8	22.2	63.3	131.9	
		4	22.4	16.2	31.4	55.6	34.1	71.8	146.0	
			1	22.2	16.3	31.2	50.4	27.1	65.7	106.9
			2	22.9	16.9	32.1	45.8	22.0	61.5	94.0
			3	23.1	17.2	31.7	52.2	26.7	69.1	96.3
			4	23.8	17.7	32.7	52.6	27.6	68.4	90.7

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1-11). 10 4 , 10 11 , 10 18 11 1
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. NAR 10 4 , 10 11 10 18

1-2W

. LAR 10 4 1-2W
10 18

가

가 ,

1-13

가

2 가

$$RGR = 0.9929 NAR + 0.5168 LAR (R^2 = 0.9548, df=45)$$

$$LAR = 1.1127 SLA + 1.0540 LWR (R^2 = 0.9758)$$

1-14

가 , ,

가 .

1- 14.

	RGR	NAR	LAR	SLA	LWR	CGR	LAI	RGRA
	0.786**	0.409**	0.575**	- 0.177	0.607**	- 0.256	- 0.618**	0.342*
	0.291*	0.356*	0.029	- 0.101	0.398**	- 0.140	- 0.315*	0.176

1- 11. 1996 9

			(cm)	(plant-1)	(dm ² /plant)	(g/plant)	(g/plant)	(g/plant)
9 20	1- 2W	1	11.0	5.0	2.0	.50	.11	.0
		2	11.7	4.8	1.9	.52	.09	.0
		3	10.5	5.0	2.4	.60	.13	.0
		4	11.1	5.0	1.9	.50	.14	.0
		1	10.5	4.6	2.2	.52	.12	.0
		2	12.4	4.8	2.2	.48	.10	.0
		3	10.9	4.4	2.0	.50	.14	.0
		4	10.2	4.2	1.8	.46	.10	.0
9 26	1- 2W	1	24.7	6.2	6.8	2.12	.62	.0
		2	24.8	6.4	6.1	2.04	.56	.0
		3	22.9	6.2	4.9	1.96	.56	.0
		4	24.8	6.2	6.4	2.04	.60	.0
		1	24.7	6.0	6.8	1.76	.48	.0
		2	25.5	5.8	6.9	1.90	.60	.0
		3	23.0	6.0	6.1	1.72	1.44	.0
		4	21.9	5.6	5.9	1.67	.54	.0
10 4	1- 2W	1	74.5	12.6	23.9	7.82	3.36	.0
		2	74.0	13.0	21.5	7.60	3.12	.0
		3	65.6	12.2	20.7	6.98	2.70	.0
		4	68.3	13.0	22.4	7.68	3.08	.0
		1	79.9	12.4	8.2	7.54	3.12	.0
		2	76.4	12.6	10.1	6.40	2.84	.0
		3	74.4	12.6	8.6	6.64	2.72	.0
		4	75.1	13.2	7.9	7.84	3.36	.0
10 11	1- 2W	1	99.6	16.2	37.4	12.90	6.58	.0
		2	104.8	15.8	33.6	11.70	6.92	.0
		3	99.1	16.0	41.0	14.58	7.22	.0
		4	102.0	16.2	37.1	15.12	7.84	.0
		1	578.4	16.6	45.2	13.92	7.18	.0
		2	529.4	16.4	47.7	13.08	7.36	.0
		3	116.6	16.6	45.0	11.74	7.60	.0
		4	119.2	16.8	49.4	14.88	8.08	.0

1- 11.

			(cm)	(plant-l)	(dm ² plant)	(g/plant)	(g/plant)	(g/plant)
10 18	1-2W	1	160.0	20.0	62.8	18.94	12.52	29.0
		2	157.0	21.2	79.8	25.32	13.40	30.5
		3	158.4	21.2	90.0	26.30	15.02	94.0
		4	163.7	21.2	80.5	24.58	14.66	68.1
		1	168.4	21.4	86.7	22.58	14.10	21.2
		2	173.9	22.0	84.0	21.82	12.98	82.1
		3	161.9	21.2	81.1	19.94	12.16	13.4
		4	163.5	19.8	76.1	17.74	11.34	31.2
10 25	1-2W	1	217.9	25.0	113.1	28.02	16.80	251.9
		2	198.2	24.0	103.3	26.48	15.28	295.0
		3	205.6	24.6	101.4	42.32	32.82	289.4
		4	199.2	24.4	102.9	30.18	27.06	257.3
		1	208.0	22.8	110.5	25.30	14.88	341.6
		2	202.5	22.6	95.7	21.38	12.90	292.2
		3	199.6	22.6	104.7	23.16	15.42	247.1
		4	221.6	23.6	122.9	29.98	17.24	310.3
11 1	1-2W	1	229.8	27.4	124.7	32.08	18.94	928.7
		2	224.6	26.8	117.7	32.68	17.72	660.2
		3	241.2	27.6	121.7	32.84	21.72	776.5
		4	221.7	27.6	114.3	29.02	16.38	1143.5
		1	275.6	27.8	156.7	34.90	22.58	697.3
		2	254.6	29.0	141.6	29.42	23.14	938.8
		3	260.2	28.4	140.4	34.74	22.18	643.4
		4	267.0	29.2	159.0	37.18	22.78	894.3

			RGR	NAR	LAR	SLA	LWR	CGR	LAI	RGRA
9 26	1- 2W	1	.2146	.0772	2.6333	3.3670	.7821	.8213	.1190	.1727
		2	.2071	.0799	2.4693	3.0963	.7975	.7673	.1070	.1694
		3	.1770	.0728	2.2571	2.8654	.7877	.6902	.0990	.1041
		4	.2024	.0766	2.5366	3.2757	.7744	.7712	.1123	.1697
		1	.1790	.0561	3.1291	3.9526	.7917	.6169	.1216	.1633
		2	.2087	.0673	2.9378	3.8018	.7727	.7403	.1221	.1661
		3	.2281	.0973	2.1452	3.6720	.5842	.9717	.1100	.1597
		4	.1961	.0676	2.7945	3.6341	.7690	.6362	.1045	.1655
10 4	1- 2W	1	.2009	.0887	2.2031	3.0852	.7141	3.2543	.4139	.1795
		2	.2024	.0950	2.0714	2.8622	.7237	3.1309	.3724	.1808
		3	.1923	.0928	2.1049	2.8724	.7328	2.7607	.3465	.2047
		4	.2007	.0909	2.1497	2.9636	.7254	3.1309	.3887	.1797
		1	.2229	.1603	1.1670	1.6187	.7209	3.2466	.2032	.0264
		2	.1868	.1150	1.4435	2.0417	.7070	2.5988	.2287	.0539
		3	.1551	.1210	1.1804	1.7678	.6677	2.3906	.1994	.0486
		4	.2318	.1876	1.0281	1.4497	.7092	3.4664	.1861	.0418
10 11	1- 2W	1	.0793	.0393	1.9985	2.9573	.6758	3.2003	.8269	.0641
		2	.0789	.0416	1.8799	2.8578	.6578	3.0461	.7443	.0638
		3	.1160	.0582	1.9618	2.8645	.6849	4.6732	.8334	.0975
		4	.1083	.0597	1.7668	2.6130	.6762	4.7041	.8040	.0721
		1	.0975	.0687	1.6819	2.4892	.6757	4.0254	.7209	.2435
		2	.1134	.0662	1.9463	2.9654	.6563	4.3185	.7796	.2225
		3	.1037	.0647	1.8685	2.9176	.6404	3.8481	.7237	.2358
		4	.1025	.0742	1.6773	2.5219	.6651	4.5344	.7732	.2620
10 18	1- 2W	1	.0750	.0392	1.9107	3.1457	.6074	5.1899	1.3517	.0739
		2	.1087	.0567	1.9404	3.0643	.6333	8.1820	1.5309	.1234
		3	.1019	.0520	1.9767	3.2048	.6168	8.7449	1.7681	.1122
		4	.0853	.0478	1.8193	2.9641	.6138	7.2335	1.5880	.1105
		1	.0822	.0368	2.2506	3.6133	.6229	6.3235	1.7798	.0930
		2	.0884	.0390	2.2559	3.7750	.5976	6.7554	1.7779	.0809
		3	.0772	.0323	2.3999	3.9801	.6030	5.3441	1.7016	.0842
		4	.0416	.0179	2.3372	3.8462	.6077	2.9921	1.6931	.0616

1- 12.

			RGR	NAR	LAR	SLA	LWR	CGR	LAI	RGRA
10 25	1- 2W	1	.0850	.0448	1.8975	3.7449	.5067	10.3335	2.3733	.0841
		2	.0622	.0341	1.8055	3.5344	.5108	8.3748	2.4707	.0368
		3	.1085	.0756	1.3715	2.7890	.4918	19.5026	2.5828	.0171
		4	.0737	.0441	1.6430	3.3490	.4906	10.8656	2.4749	.0350
		1	.0913	.0488	1.8170	4.1190	.4411	12.9323	2.6615	.0347
		2	.0522	.0266	1.9398	4.1607	.4662	6.4546	2.4257	.0186
		3	.0613	.0275	2.2069	4.3113	.5119	6.8633	2.5077	.0365
		4	.1232	.0616	1.9225	4.1696	.4611	16.2175	2.6852	.0686
11 1	1- 2W	1	.0165	.0088	1.8752	3.9564	.4740	2.8224	3.2089	.0139
		2	.0056	.0032	1.7601	3.7355	.4712	.9408	2.9824	.0187
		3	-.0349	-.0264	1.3157	2.9680	.4433	-7.9352	3.0104	.0260
		4	.0202	.0140	1.4439	3.6683	.3936	4.0871	2.9307	.0151
		1	.0115	.0064	1.8054	4.4392	.4067	2.2903	3.6064	.0499
		2	.0545	.0310	1.7602	4.6716	.3768	9.8014	3.2027	.0560
		3	.0433	.0212	2.0416	4.2341	.4822	6.9713	3.3084	.0419
		4	.0113	.0061	1.8605	4.1981	.4432	2.3058	3.8049	.0368

1- 13. 1996

	NAR	LAR	SLA	LWR	CGR	LAI	RGRA
RGR	0.8428**	0.2282	- 0.5252**	0.7941**	- 0.3847**	- 0.8537**	0.4961**
NAR		- 0.2905	- 0.7988**	0.6031**	- 0.2046	- 0.7211**	0.2706
LAR			0.4954**	0.4026**	- 0.3649*	- 0.2545	0.4332**
SLA				- 0.5855**	0.2120	0.6614**	- 0.2138
LWR					- 0.6117**	- 0.9406**	0.6236**
CGR						0.5840**	- 0.3970**
LAI							- 0.6227**

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 180cm × 15cm(3,700 /10a)가 29% , 180 × 20cm(2,700 /10a)
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			()	()	()	(%)	(%)	(%)	(mmol m-2l-1)
4/25 4/30	1- 2w	1	23.26	17.17	31.33	38.97	17.88	57.46	7.1
		2	24.87	18.87	33.02	43.50	19.76	62.16	7.2
		3	23.89	18.16	31.40	40.90	18.52	57.72	6.8
		4	23.93	17.38	32.99	52.96	25.76	65.59	7.4
		1	23.56	17.13	33.12	42.48	19.86	57.91	8.1
		2	24.09	17.54	33.64	38.33	16.93	54.78	7.6
		3	24.37	18.02	33.46	42.70	18.67	60.13	7.4
		4	23.77	17.60	32.35	45.52	19.45	62.35	8.0
5/01 5/02	1- 2w	1	21.79	17.29	27.24	51.87	17.27	64.98	40.2
		2	23.71	19.15	28.88	56.58	27.71	68.69	42.7
		3	22.15	18.34	27.28	53.58	24.47	62.09	41.0
		4	21.94	17.49	28.49	67.12	38.68	70.10	44.3
		1	21.67	17.12	27.64	54.73	31.92	63.66	49.1
		2	22.22	17.45	28.26	49.80	22.67	59.88	45.2
		3	22.55	17.88	28.30	55.22	26.95	65.98	42.6
		4	21.98	17.36	27.36	57.34	26.49	69.48	48.9
5/03 5/06	1- 2w	1	24.52	19.12	33.40	52.73	19.15	66.59	36.4
		2	25.76	20.43	35.06	57.02	26.15	70.14	36.3
		3	24.55	19.66	33.18	54.42	24.82	65.20	34.2
		4	25.06	19.21	35.49	66.11	35.82	72.38	36.9
		1	25.35	19.48	35.36	55.56	32.10	65.01	41.2
		2	25.99	20.17	35.70	50.77	22.59	62.31	36.8
		3	26.20	20.55	35.13	55.75	25.70	67.75	36.6
		4	25.61	20.11	34.04	58.03	27.75	70.70	40.3
5/07 5/08	1- 2w	1	22.41	19.65	25.27	67.31	51.61	70.17	26.7
		2	23.72	20.99	26.74	70.60	56.85	73.59	26.0
		3	22.59	20.24	25.50	66.81	53.46	68.41	23.8
		4	22.61	19.80	25.60	77.51	61.35	75.63	25.6
		1	23.74	20.02	28.21	65.09	56.26	66.69	26.1
		2	24.60	20.74	29.27	61.81	51.47	64.24	23.2
		3	25.06	21.17	29.59	67.25	56.07	69.89	23.1
		4	24.49	20.71	28.79	68.96	56.83	71.71	24.8
5/09 5/10	1- 2w	1	22.30	15.95	30.81	58.23	24.89	72.56	26.1
		2	23.81	17.34	32.69	62.83	25.99	74.98	25.6
		3	22.42	16.74	30.65	59.60	35.27	70.71	23.5
		4	22.67	15.85	32.46	70.67	41.28	77.46	25.6
		1	23.45	16.68	32.61	59.00	36.86	67.60	24.8
		2	24.07	17.20	33.72	55.39	31.35	65.33	20.5
		3	24.11	17.62	32.42	61.23	35.76	70.65	19.0
		4	23.66	17.28	31.28	62.61	36.34	72.48	23.2

2- 1.

			()	()	()	(%)	(%)	(%) (mmol m-2l-l)	
5/11 5/15	1- 2w	1	23.29	19.83	29.35	62.60	48.78	72.24	18.6
		2	24.85	21.24	31.41	64.82	48.84	74.70	17.2
3		23.45	20.02	29.49	61.32	49.68	69.25	14.6	
4		23.48	19.80	29.99	71.78	51.55	75.74	16.4	
1		23.75	20.19	29.68	59.38	48.42	66.76	17.0	
2		24.56	20.88	30.64	55.92	45.26	64.25	15.0	
3		24.90	21.30	30.52	61.59	51.01	70.17	15.4	
4		24.32	20.88	29.66	63.14	51.09	71.84	16.3	
5/16 5/19	1- 2w	1	23.35	15.45	31.90	43.05	11.86	75.52	19.1
		2	26.08	17.90	37.14	47.59	15.86	75.40	17.6
3		23.39	15.66	31.92	46.12	15.08	70.67	14.6	
4		23.65	15.49	33.18	54.57	29.32	79.10	16.0	
1		24.97	17.89	34.94	47.55	18.13	68.21	17.5	
2		25.57	18.31	35.98	44.09	14.76	65.86	14.7	
3		25.56	18.60	35.31	48.31	16.42	71.26	16.5	
4		25.10	18.38	34.12	49.44	15.49	72.90	16.9	
5/20 5/22	1- 2w	1	20.92	14.88	29.51	43.60	8.98	72.58	41.7
		2	22.71	16.64	31.41	43.75	14.27	74.92	39.4
3		20.96	14.36	29.64	46.03	15.68	68.35	38.2	
4		21.15	14.58	30.01	55.97	24.13	77.36	41.2	
1		22.02	17.45	30.58	47.84	19.87	66.05	47.4	
2		22.81	17.95	31.43	43.76	15.01	64.32	42.5	
3		22.98	18.22	31.49	48.60	17.88	69.68	39.6	
4		22.38	17.94	31.29	49.35	16.26	70.97	46.8	

2- 2. 1997 4

			()	()	()	(%)	(%)	(%) (mmol m-2 d-l)	
1- 2W	1		22.7	17.4	29.9	52.3	25.1	69.0	215.9
	2		24.4	19.1	32.0	55.8	29.4	71.8	212.0
	3		22.9	17.9	29.9	53.6	29.6	66.5	196.7
	4		23.1	17.4	31.0	64.6	38.5	74.2	213.4
	1		23.6	18.2	31.5	54.0	32.9	65.2	231.2
	2		24.2	18.8	32.3	50.0	27.5	62.6	205.5
	3		24.5	19.2	32.0	55.1	31.1	68.2	200.2
	4		23.9	18.8	31.1	56.8	31.2	70.3	225.2

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1- 2W									
	(/)	(kg)				(/)	(kg)		
1	15	136.0	192.0	43.3	1	15	130.0	161.0	46.7
	20	188.0	228.0	52.7		20	151.0	187.0	55.8
	25	174.0	220.0	55.2		25	183.0	231.0	56.4
2	15	145.0	192.0	55.1	2	15	145.0	187.0	50.4
	20	177.0	223.0	53.9		20	124.0	155.0	41.7
	25	185.0	235.0	61.5		25	178.0	235.0	61.4
3	15	99.0	125.0	43.0	3	15	158.0	197.0	57.2
	20	151.0	192.0	51.1		20	151.0	187.0	51.9
	25	143.0	188.0	56.2		25	129.0	149.0	38.9
4	15	160.0	217.0	59.1	4	15	125.0	155.0	47.2
	20	186.0	234.0	59.1		20	128.0	151.0	48.2
	25	163.0	198.0	56.7		25	120.0	141.0	43.4

2- 4.

		(kg)*		
1- 2W	15	135.0	181.5	50.1
	20	175.5	219.5	54.2
	25	166.2	210.2	57.4
	15	139.5	175.0	50.4
	20	138.5	170.0	49.4
	25	152.2	189.0	50.0

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		()	()	()	(%)	(%)	(%)	(mmol m-2 d-1)
1-2W	1	27.33	22.65	34.58	50.94	29.47	62.07	28.44
	2	29.79	24.86	37.37	52.63	30.12	66.08	24.98
	3	27.45	22.83	34.56	50.81	29.72	62.00	23.83
	4	30.92	24.91	40.51	48.23	28.83	59.11	23.29
	1	27.71	22.65	35.81	50.58	31.73	61.31	26.77
	2	28.82	23.71	36.95	45.68	24.87	57.21	22.26
	3	28.95	23.98	36.55	51.26	29.72	63.93	22.39
	4	28.10	23.22	35.52	49.97	26.70	63.17	24.64

			()	()	()	(%)	(%)	(%)	(mmol m-2l-l)
6/ 3 6/22	1- 2w	1	25.75	20.16	34.98	48.37	22.10	60.60	28.44
		2	28.02	22.13	37.53	50.11	22.53	64.61	25.34
		3	25.89	20.33	34.84	48.16	22.18	60.25	24.24
		4	29.49	22.44	40.66	45.19	20.99	57.16	23.58
		1	26.29	20.18	35.96	46.72	23.04	58.89	26.49
		2	27.27	21.11	37.05	41.56	16.48	53.94	22.30
		3	27.39	21.39	36.60	47.30	20.65	61.54	22.12
		4	26.68	20.77	35.86	45.76	17.35	60.63	23.71
6/23 6/29	1- 2w	1	26.78	23.35	31.74	54.97	42.21	63.18	21.40
		2	29.22	25.58	34.43	56.78	43.24	67.32	18.04
		3	26.84	23.56	31.59	55.08	43.08	63.21	16.02
		4	29.97	25.64	36.97	53.04	42.61	60.34	15.29
		1	26.95	23.43	32.61	55.27	45.27	63.15	18.55
		2	28.09	24.50	33.81	50.45	38.03	59.29	14.39
		3	28.27	24.73	33.68	56.58	44.47	66.15	14.65
		4	27.39	23.94	32.42	55.10	42.19	64.69	16.52
6/30 7/ 6	1- 2w	1	29.51	25.81	35.28	55.07	36.28	64.41	31.81
		2	32.18	28.29	38.12	56.84	37.17	68.62	27.71
		3	29.61	25.97	35.21	55.10	37.17	64.77	26.96
		4	33.15	28.12	41.82	53.02	36.53	62.24	26.64
		1	29.79	25.76	36.83	55.84	40.63	64.80	30.91
		2	30.97	26.98	37.77	51.37	33.53	61.69	25.66
		3	31.15	27.30	37.45	56.86	39.22	66.96	26.21
		4	30.15	26.37	36.24	55.57	35.89	66.27	29.08
7/ 7 7/13	1- 2w	1	30.16	26.18	36.01	51.75	31.31	62.48	31.87
		2	32.83	28.66	39.12	53.31	32.08	66.26	27.99
		3	30.29	26.38	36.20	51.63	31.27	62.94	27.33
		4	33.64	28.47	42.01	49.26	30.49	60.38	27.04
		1	30.42	26.16	37.65	52.39	33.69	62.42	30.78
		2	31.68	27.37	38.83	48.58	28.19	59.57	25.67
		3	31.79	27.62	38.30	53.53	32.55	65.26	26.24
		4	30.81	26.73	37.13	52.14	28.80	64.93	29.65
7/14 7/21	1- 2w	1	28.14	23.35	34.35	50.40	31.32	63.22	29.83
		2	30.81	25.83	37.57	51.86	31.95	67.24	26.09
		3	28.26	23.59	34.60	50.13	31.26	63.03	24.90
		4	31.75	25.50	41.33	47.55	30.48	60.08	24.44
		1	28.46	23.25	36.04	51.48	35.16	63.02	29.17
		2	29.69	24.48	37.40	45.76	26.39	59.21	24.45
		3	29.77	24.72	36.89	50.94	31.55	65.27	24.62
		4	28.82	23.80	35.54	50.83	29.73	65.22	27.70

2-7

4 1 2

3 4 6

(bed)가 , 3 2

29.5 27.5

1-2W 가 31.4 29.7

가 7.5kg 1-2W 7.4kg

1-2W

(2-8).

2-8. 1998 6

1-2W							
	(kg)				(kg)		
1	29.2	31.2	7.1	1	27.8	30.5	7.7
2	27.8	30.2	7.0	2	24.8	26.7	6.6
3	31.2	32.5	7.8	3	24.8	26.7	7.3
4	29.7	31.2	7.9	4	32.3	34.8	8.4
LSD005	7.92	9.46	2.99	LSD005	8.29	9.76	2.79

2-9. 1998 6

1-2W							
(cm)	(kg)			(cm)	(kg)		
15	35.0	36.5	8.56	15	34.8	37.6	9.42
20	29.0	31.5	7.59	20	29.5	32.5	8.32
25	24.4	26.1	6.21	25	18.1	18.9	4.83
LSD005	6.86	8.20	1.49	LSD005	7.18	8.46	2.41

2-7.

1-2W											
	(cm)		(kg)				(cm)		(kg)		
1	15	1	29.0	29.0	6.21	1	15	1	42.0	45.0	11.24
		2	27.0	27.0	6.76			2	28.0	29.0	7.26
	20	1	28.0	28.0	7.11		20	1	31.0	32.0	8.18
		2	30.0	32.0	7.11			2	31.0	40.0	10.48
	25	1	32.0	41.0	7.76		25	1	13.0	13.0	3.20
		2	29.0	30.0	7.68			2	22.0	24.0	5.66
2	15	1	31.0	32.0	7.59	2	15	1	13.0	14.0	2.80
		2	33.0	36.0	7.81			2	45.0	50.0	12.70
	20	1	24.0	25.0	6.96		20	1	26.0	26.0	5.73
		2	20.0	26.0	6.53			2	26.0	28.0	7.43
	25	1	34.0	37.0	6.93		25	1	19.0	20.0	5.18
		2	25.0	25.0	6.36			2	20.0	22.0	6.03
3	15	1	37.0	38.0	10.73	3	15	1	32.0	34.0	7.51
		2	47.0	48.0	10.21			2	35.0	38.0	11.70
	20	1	35.0	37.0	8.70		20	1	28.0	31.0	8.48
		2	32.0	36.0	7.76			2	26.0	29.0	8.19
	25	1	21.0	21.0	5.71		25	1	17.0	17.0	4.99
		2	15.0	15.0	3.64			2	11.0	11.0	3.05
4	15	1	37.0	40.0	9.26	4	15	1	44.0	50.0	12.02
		2	39.0	42.0	9.90			2	39.0	41.0	10.11
	20	1	35.0	38.0	8.74		20	1	39.0	43.0	10.58
		2	28.0	30.0	7.82			2	29.0	31.0	7.51
	25	1	18.0	18.0	4.54		25	1	25.0	25.0	5.50
		2	21.0	22.0	7.06			2	18.0	19.0	5.00

(2-9). 1-2W

15cm(34 /bed) 25cm (20 /bed) 가 ,
 15cm 20cm (26 /bed) 20cm 25cm 가 .
 15cm 20cm 25cm
 15cm 20cm 가 .
 가 가 , 가 15cm

20cm

가

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15cm

15cm 20cm

.

3

1

가 ,

가 ,

1

171

. 1996 8

76 가 , 25 ,

50 , 20 , 95

(55%) . 52 64% ,

61 72% , 46 59% , 25 40% .

5 6

3 4 .

model ,

4

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2

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 4 2 (1-2W
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 20

가.

1)

4 , 4
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 1997 8 10 9
 10 . 10 6 11 30 .
 , 10 14 11 30 .

2)

1)

4 2 1997 11 17
 12 17 , 12 26 1998 2 7

, 1998 2 9 2 21 .

가, 가 , 1998 2 7 3

7 , 3 12 5 5 , 98 4 28

5 10 , 4 20 5 8

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. 1998 5 13 10

25 38 . 5 15

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, 5 17 2-3 가

6 2 . bench

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8 20 .

6 23 7 21 1 , , ,

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4 3 5 , 6 6 7
16 4 2 . 7 9
7 22 2 4 .
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, , , ,
5가 . 10 11
1 2 1 2 3 4
, 2 3 4 5 , 4
5 6 7 8 9
10 12 . 가
가

가 .

가

가

4가

4가 ,

, 가 ,

1.

3-1, 3-2, 3-3, 3-4
 가 1-2W
 1 2
 가 가
 가
 가 1-2W 가
 2 3mmol m-2 d-1
 1-2W
 1 2
 1 4

3-1. 1997 9 9 11 10 27

		()	()	()	(%)	(%)	(%)	(mmol m-2 d-1)
1-2W	1	21.60	15.81	30.89	37.50	9.81	60.29	28.13
	2	23.07	16.90	33.07	47.29	13.58	67.15	24.22
	3	21.57	15.69	31.05	45.44	13.33	63.51	22.93
	4	21.83	15.79	31.73	51.82	21.65	69.38	25.03
	1	22.49	16.25	32.88	44.46	14.89	61.22	25.60
	2	23.29	17.12	33.69	40.06	11.49	57.15	20.73
	3	23.37	17.45	32.99	44.60	13.12	63.32	20.80
	4	22.63	16.75	32.09	45.91	12.49	64.59	20.17

3-2. 1997 12

12 26 2 8

		()	()	()	(%)	(%)	(%)	(mmol m-2 d-1)
1-2W	1	20.04	12.51	26.41	26.20	13.98	39.62	21.50
	2	22.65	13.79	28.83	26.51	16.80	37.87	17.32
	3	21.44	13.28	27.08	25.21	16.22	37.79	14.91
	4	19.99	13.25	27.38	32.99	23.54	45.10	16.53
	1	20.25	13.41	30.40	32.67	18.97	46.64	15.75
	2	22.86	14.39	31.49	24.09	11.61	39.99	11.71
	3	22.59	14.52	30.97	28.51	14.83	45.12	11.69
	4	21.38	13.72	29.80	31.55	15.78	49.14	12.30

3-3. 1998 3

3 12 5 2

		()	()	()	(%)	(%)	(%)	(mmol m-2 d-1)
1-2W	1	21.61	16.06	32.33	48.18	23.55	61.86	28.47
	2	23.83	18.10	34.96	50.54	23.99	66.01	25.37
	3	22.00	16.57	32.36	48.28	23.70	62.05	24.19
	4	22.09	16.25	33.25	55.09	27.08	65.98	26.41
	1	22.67	17.34	33.01	50.55	27.65	62.99	24.34
	2	23.64	18.21	34.11	45.73	22.65	59.21	20.07
	3	25.15	19.60	35.55	45.56	22.07	60.11	19.97
	4	22.83	17.78	32.57	51.94	26.10	66.20	20.32

3-4. 1998 6

6 3 7 21

		()	()	()	(%)	(%)	(%)	(mmol m-2 d-1)
1-2W	1	27.33	22.65	34.58	50.94	29.47	62.07	28.44
	2	29.79	24.86	37.37	52.63	30.12	66.08	24.98
	3	27.45	22.83	34.56	50.81	29.72	62.00	23.83
	4	30.92	24.91	40.51	48.23	28.83	59.11	23.29
	1	27.71	22.65	35.81	50.58	31.73	61.31	26.77
	2	28.82	23.71	36.95	45.68	24.87	57.21	22.26
	3	28.95	23.98	36.55	51.26	29.72	63.93	22.39
	4	28.10	23.22	35.52	49.97	26.70	63.17	24.64

2.

, ,
3-5 . 가
가 40% 2
가 20
3 4 가 3 ,
가 가
가 20% 가
가 가
8 가 . 가
3-6 가
8 . 가
1-2W , 가 ,
, , , , ,
가 1-2W
2 3 , 가

가 , 가
 가 가 가
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 가 가 가 가 12
 1 .
 1-2W
 12 , 1
 4 15 .
 18 21 가 .
 가 가 1-2W
 가 가
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 가
 가 67 74%
 가 .

가 가
가 . 가
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가
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가 가 , 가 가
가 37.8
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가
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,
가 ,
, 가 가
가 가
가 가 .

3- 5.

		1- 2W							
가		4.9	1.3	79.9	20.4	4.4	1.3	77.9	22.5
		4.5	1.0	82.5	22.4	3.9	1.0	79.5	37.1
		1.5	5.3	23.6	.0	1.9	5.1	27.4	11.6
		2.0	4.5	31.0	1.7	1.5	5.0	23.4	2.8
		1.6	4.5	27.3	.0	2.1	4.0	35.3	3.7
		4.3	.6	88.9	14.1	4.5	.1	98.1	27.7
		3.5	2.7	59.1	.0	3.0	3.6	47.6	.0
		2.6	4.4	40.1	2.9	2.1	3.4	39.0	.0
가		4.0	2.8	58.7	9.9	5.3	4.0	56.3	13.9
		4.0	4.1	49.8	13.5	3.6	6.7	34.1	5.4
		5.3	10.7	32.8	1.3	6.5	9.3	40.5	.0
		4.8	8.0	37.1	.0	5.6	7.8	40.8	.0
		8.6	7.4	53.0	2.1	9.2	5.9	60.3	.0
		9.7	2.6	78.7	18.6	8.9	3.0	74.1	18.4
		5.6	5.9	48.9	3.0	6.8	6.1	52.7	5.1
		5.6	7.0	44.6	2.0	6.0	6.4	48.7	.0
가		17.4	1.6	29.9	91.7	21.3	1.2	40.6	94.5
		19.4	3.5	29.2	84.6	19.6	1.1	42.1	94.8
		11.9	28.3	9.8	30.1	13.8	38.4	13.1	28.2
		13.1	24.5	14.7	35.8	13.8	25.1	17.2	37.0
		21.9	.0	30.1	100.0	27.5	.6	27.0	98.1
		20.3	.3	28.7	98.5	25.2	.0	41.0	100.0
		18.1	6.3	21.5	74.1	20.4	8.2	41.3	71.9
		17.2	8.3	17.4	67.5	18.8	7.0	28.1	73.3
가		22.2	.1	99.7	43.1	20.7	1.6	92.8	43.1
		23.9	.5	97.8	49.6	18.5	1.2	94.1	40.0
		5.3	22.3	18.8	5.5	4.3	22.0	16.0	3.6
		5.8	25.0	18.5	20.5	4.4	24.2	14.7	14.6
		23.3	4.9	83.0	50.0	20.6	7.6	73.5	46.0
		21.2	6.8	75.2	31.9	21.8	4.5	83.0	37.5
		11.2	15.4	42.2	30.8	9.5	16.3	36.2	37.0
		19.1	6.5	74.2	36.1	17.8	8.6	66.8	30.7

3- 6.

		1- 2W					
가		17.2	4.0	0.66	19.8	4.6	0.96
		18.5	4.4	0.72	21.8	4.6	0.90
		21.2	3.5	0.62	23.7	3.6	0.71
		23.2	3.5	0.63	23.5	4.0	0.75
		22.3	4.3	0.64	23.0	5.3	0.85
		21.5	5.4	0.85	23.5	5.2	0.88
		20.3	4.4	0.79	21.8	5.1	0.96
		21.5	4.7	0.81	23.7	4.8	0.98
		12.0	0.0	0.00	14.2	0.0	0.00
		12.0	1.5	0.18	14.8	2.0	0.25
가		20.4	1.5	0.26	21.4	2.5	0.46
		18.4	1.0	0.17	18.8	1.0	0.13
		21.4	2.0	0.31	20.8	2.5	0.49
		16.4	3.0	0.41	16.4	3.0	0.48
		16.2	1.5	0.22	17.4	2.5	0.40
		17.4	2.0	0.37	16.4	2.5	0.42
		17.8	2.9	0.39	21.0	2.3	0.40
		19.5	3.2	0.61	20.8	3.6	0.67
		28.8	4.5	0.86	30.8	3.0	0.60
		27.0	3.4	0.61	29.5	4.3	0.85
가		25.8	2.7	0.42	28.5	4.2	0.70
		22.3	4.5	0.67	23.3	3.8	0.72
		22.8	3.9	0.70	24.0	3.5	0.74
		25.8	3.2	0.61	24.5	3.8	0.74
		26.0	1.5	0.33	27.0	1.6	0.35
		28.3	2.0	0.51	28.5	1.9	0.44
		33.8	2.9	0.50	33.3	1.6	0.28
		37.8	2.2	0.60	35.8	2.1	0.59
		33.8	2.1	0.48	34.5	1.7	0.32
		35.3	2.4	0.50	32.5	1.9	0.39
가		33.0	2.5	0.51	34.8	2.2	0.46
		31.5	3.3	0.68	32.5	1.8	0.40

4 , , CO2
가

1

가 , Sink-Source ratio,
가 , CO2
Water Potential
가 , 가 , 가
가

Diurnal Variation

Lamber (1983) (Maintenance
Respiration), (Growth Respiration), (Ion
Uptake Respiration) . Szaniawski Kielkiewicz(1982)
가

McCree(1970)

R

$$R = P_g + W,$$

Pg , W

. Thornley(1970) McCree

$$R = Gr \frac{dw}{dt} + W,$$

, $\frac{dw}{dt}$ 가 , Gr

$$Gr = \frac{R}{(1 -)},$$

Szaniawski Kielkiewicz(1982)

Lamber (1983)

(Rr)

$$Rr = Gr \frac{dW_r}{dt} + m W_r + e \frac{dN}{dt},$$

, e

CO2
 Heinz Walz GmbH
 Gas Exchange Measuring Station
 4
 CO2 20ppm 1200ppm
 12 32 4 가 ,
 CO2 CO2
 CO2
 44

3

1.

가.

가 가 가
 PPF(photosynthetic photon flux) PPF
 (gross photosynthetic rate, GPR)

Michaelis- Menten . ,

$$GPR = 21.4513 \text{ PPF} / (287.784 + \text{PPF}) \text{ (}\mu\text{mol CO}_2 \text{ m}^{-2}\text{-l)},$$

(Fig. 4-1).

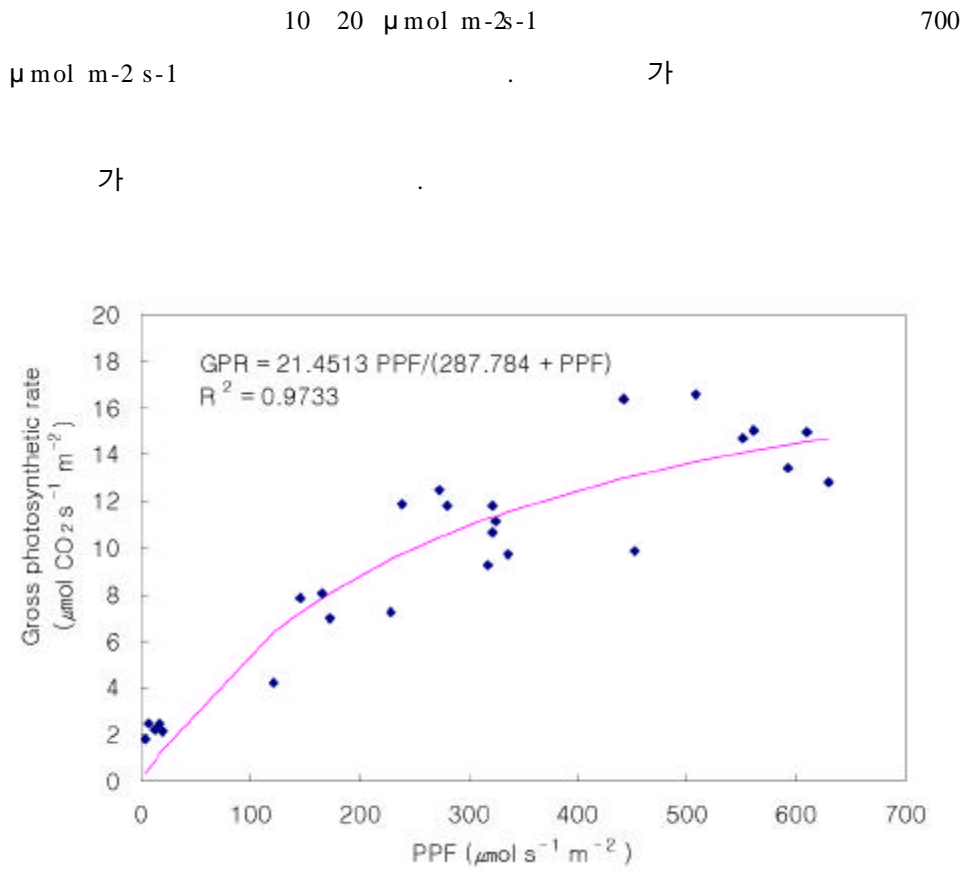


Fig. 4-1. Comparison of observed values of gross photosynthetic rate with predicted values by the model

12 . 12 32 4

$$\text{GPR} = 19.071 (1 - 1.3704 \exp(-0.0571T)),$$

, T (Fig. 4- 2).
 가 . Acock (1990)
 20 가 가
 Kitroongruang (1992) 50 heat stress
 . 24 32
 가
 CO2
 92% 가 CO2
 CO2
 CO2 CO2
 CO2 CO2
 CO2 CO2
 negative exponential

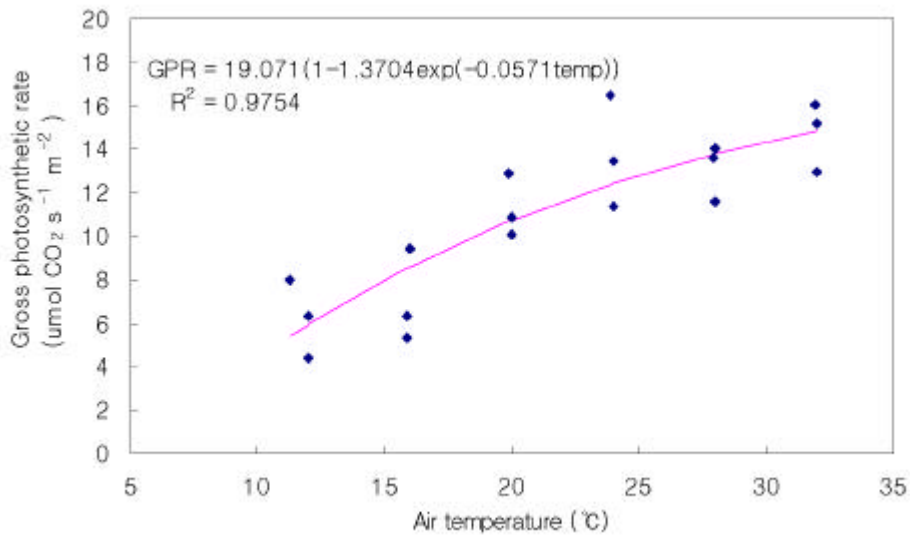


Fig. 4- 2. Responses of gross photosynthetic rate due to variation of air temperature

$$GPR = 15.5554 (1 - 0.9636 \exp(-0.0024 \text{ CO}_2)),$$

(Fig. 4-3), CO₂ CO₂ ppm
 CO₂ 20 40ppm
 , CO₂ 1200 1300ppm

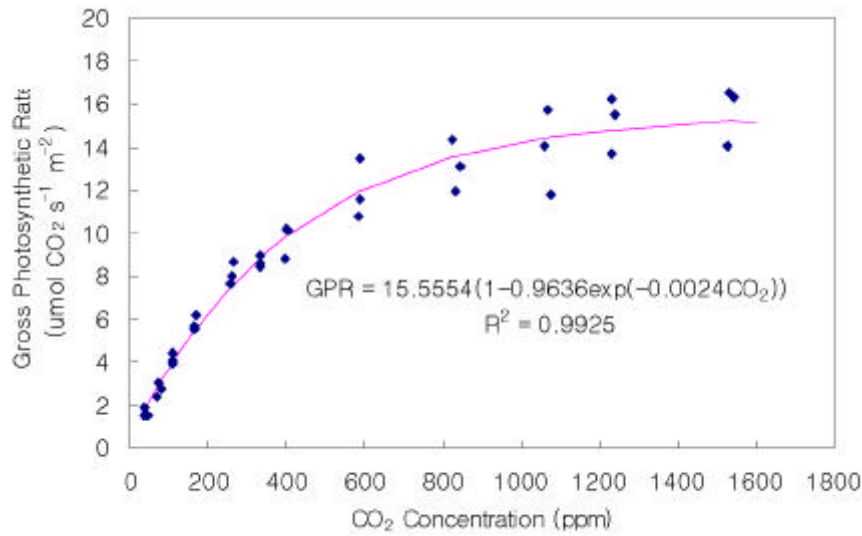


Fig. 4-3. Responses of gross photosynthetic rate under various CO₂ concentration

C3 RUBP
 Carboxylase 가 .
 가
 가 .
 logistic curve

$$GPR = 24.743 / (1 + 6.0343 \exp(-0.3689N)),$$

(Fig. 4-4) N (%) .

(Tolley-Henry and Raper, 1986; Boote et al. , 1978; Lugg and Sinclair, 1981).

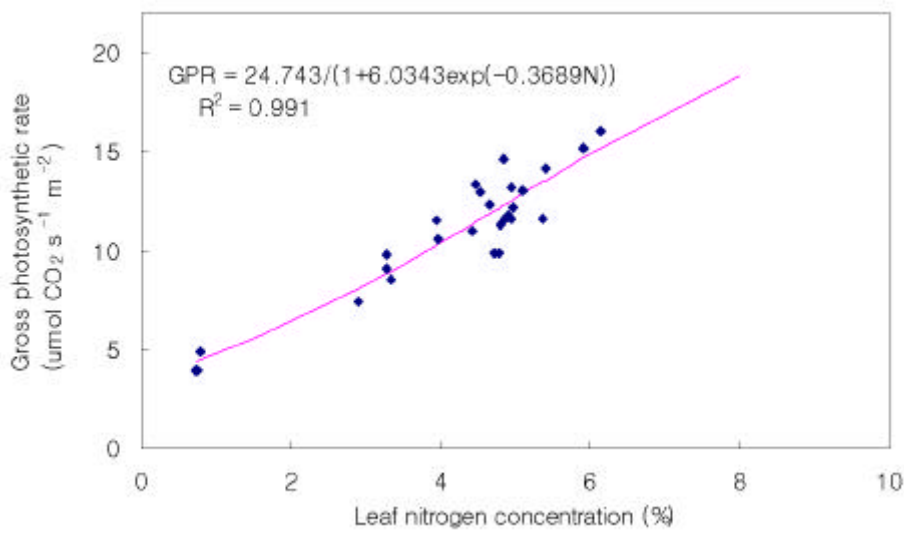


Fig. 4-4. Responses of gross photosynthetic rate due to various content of leaf nitrogen

12 가
 가
 가
 (Fig. 4-5, 4-6, 4-7, 4-8, 4-9, 4-10). 12 600 µmol CO₂
 m-2-1 9.41 µmol CO₂ m-2 s-1

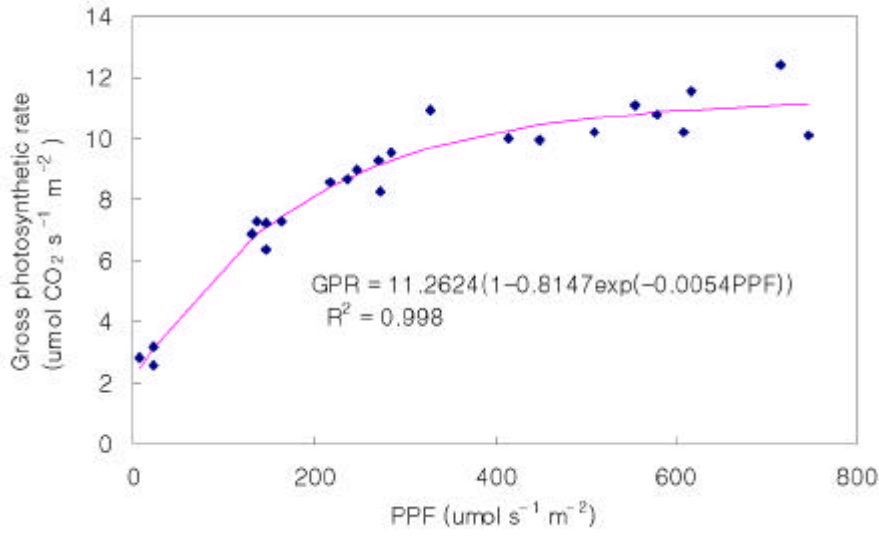


Fig. 4-6. Responses of gross photosynthetic rate of cucumber leaves to the different PPF at 16. C of air temperature

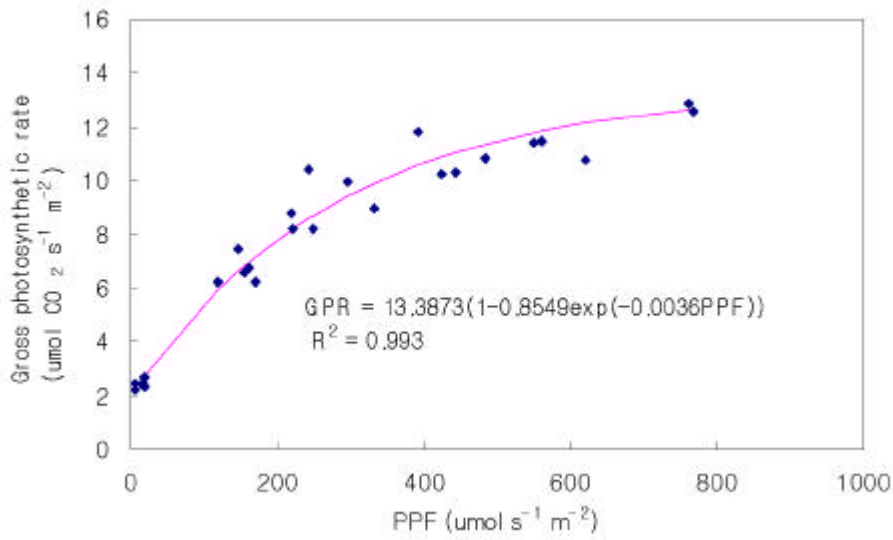


Fig. 4-7. Responses of gross photosynthetic rate of cucumber leaves to the different PPF at 20. C of air temperature

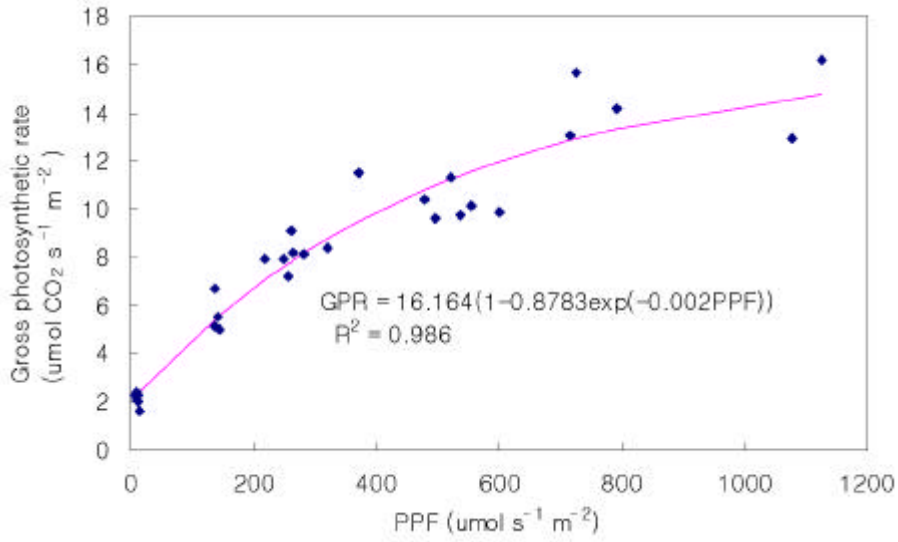


Fig. 4-8. Responses of gross photosynthetic rate of cucumber leaves to the different PPF at 24. C of air temperature

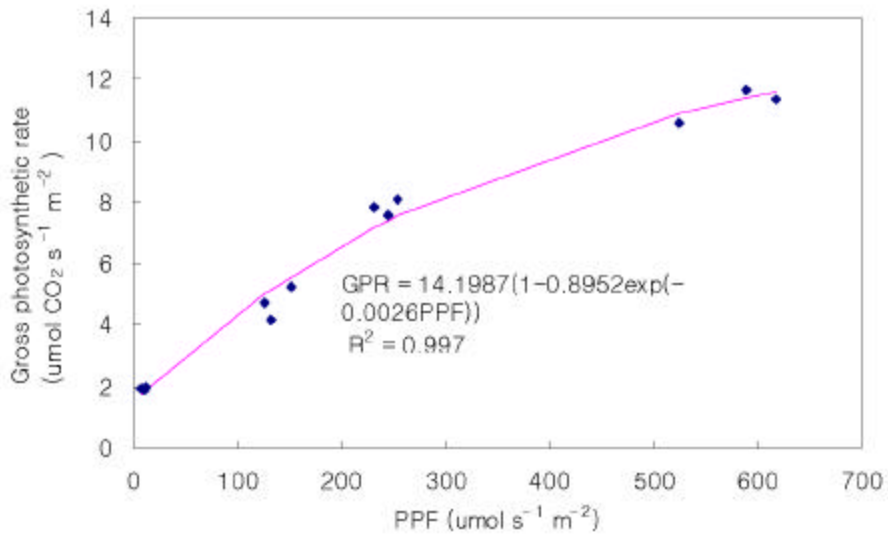


Fig. 4-9. Responses of gross photosynthetic rate of cucumber leaves to the different PPF at 28. C of air temperature

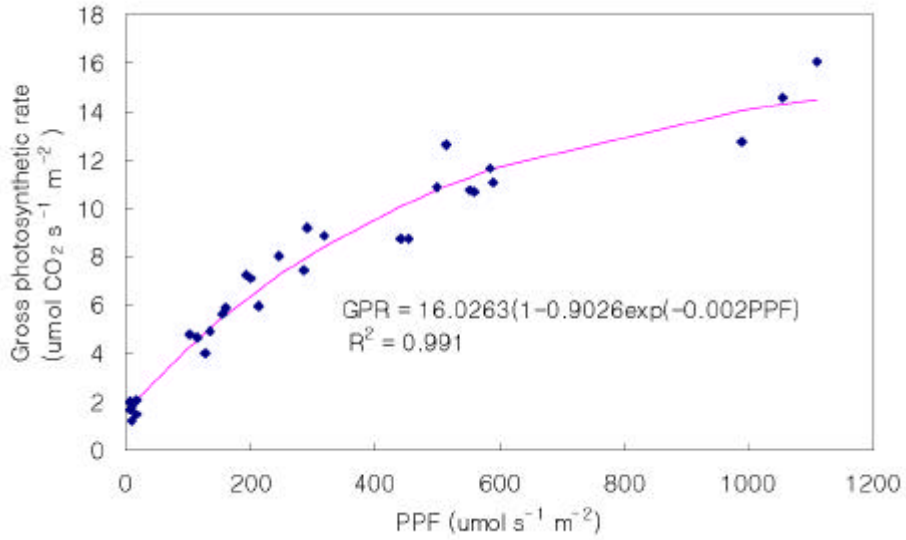


Fig. 4-10. Responses of gross photosynthetic rate of cucumber leave different PPF at 32, C of air temperature

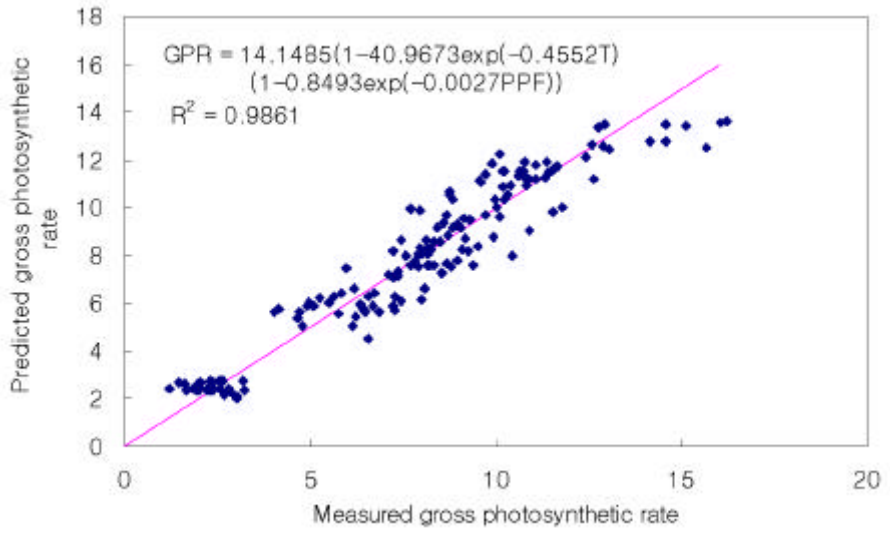


Fig. 4-11. Comparisons of observed value of leaf gross photosynthetic rate with predicted values by the equation

CO2

CO2

CO2

CO2

(Fig. 4- 12).

$$GPR=32.9352(1-0.952\exp(-0.0022PPF))(1-0.8093\exp(-0.017CO_2)) \text{----- (1)}$$

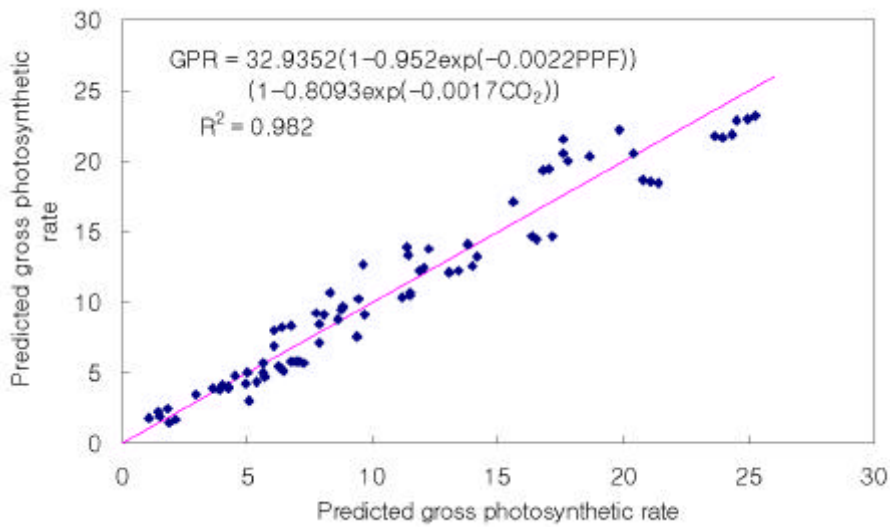


Fig. 4- 12. Comparisons of values of leaf gross photosynthetic rate with predicted values by the equation

, CO2 ,

Michaelis- Menten (1)

, , CO2

(SAS Nlin DUD)

$$GPR = 33.562T / (7.3775 + T)(1 - 0.853\exp(-0.0026PPF))(1 - 0.888\exp(-0.0018 CO_2)),$$

(Fig. 4- 13).

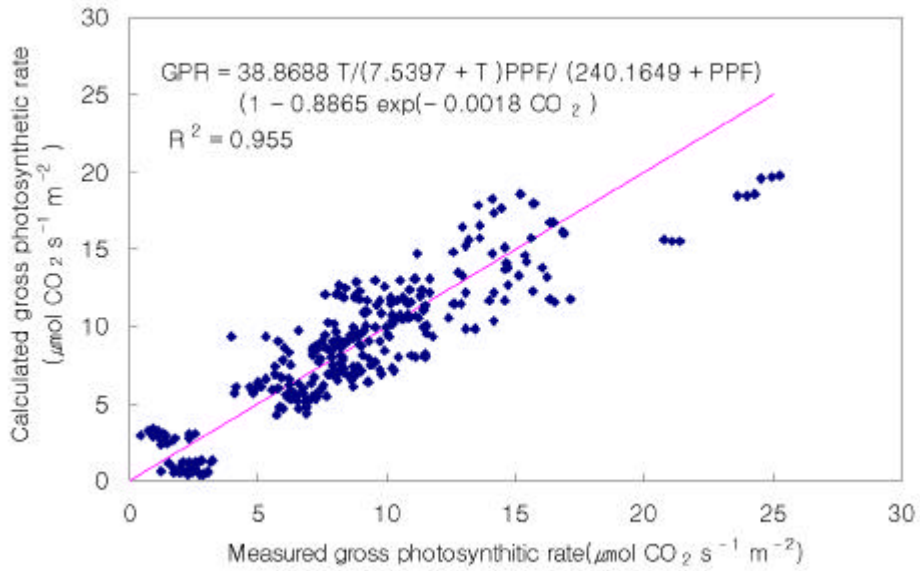


Fig. 4- 13. Comparisons of observed value of leaf gross photosynthetic rate with predicted values by the equation

diurnal variation

44

(Fig 4- 14).

	11:00		15:00
가	가	23:00	6:00 가
14:00		가	19:00 가
23:00			
8	$8.5 \mu\text{mol CO}_2 \text{ m}^{-2} \text{ s}^{-1}$,	350 400 μ

mol m⁻² s⁻¹

4)

(

35

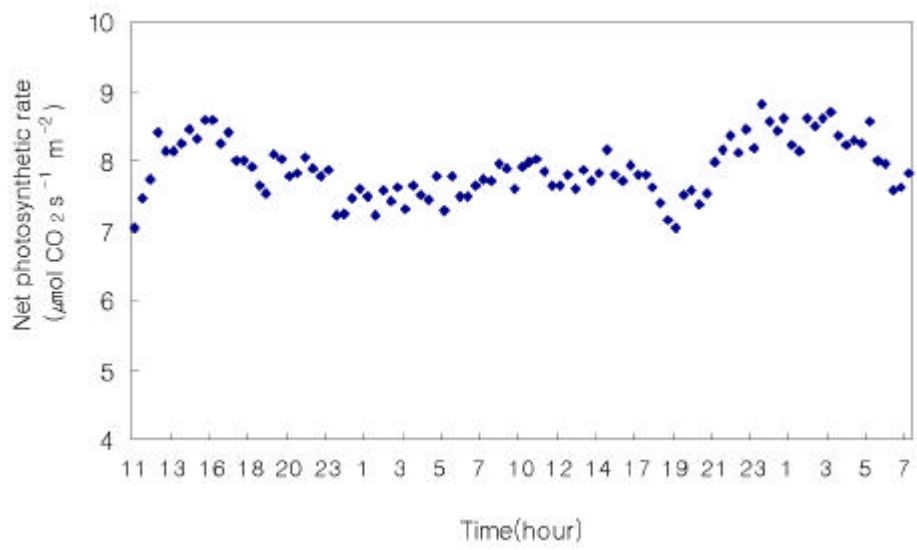


Fig. 4-14. Diurnal variations in net photosynthetic rate of cucumber leaves

1

, O₂ CO₂
 , CO₂ O₂
 H₂O
 가 Szaniawski Kielkiewicz
 (1982) 가가 가
 0.000625 0.00121(g CH₂ g⁻¹ h⁻¹)
 . glucose sugar

(Salisbury and Ross,1992).

(Veen,1981). Penning de Vries(1975)

, DIRKS ,

2

12 32 4

CO2 ,

.

, glucose

/ 26/14 20/14

18:00 , 21:00 , 23:00 , 06:00 08:00

, / 26/26 N

가 3, 6, 11mmol 09:00

18:00 12

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3

1.

(T) (RESP)

$$RESP = -0.0081 + 0.00043 T + 11.9762T^2 ,$$

(Fig. 5-1).

가 Szaniawski Kielkiewicz(1982)

가가 가

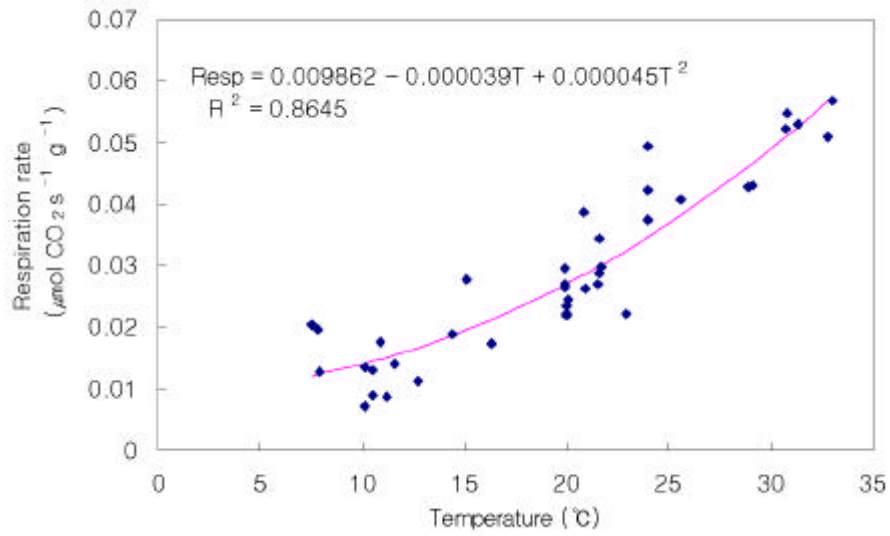


Fig. 5-1. Variations in shoot respiration rate due to variations in air temperature.

2.

, CO₂

(RESP)

(W)

(T)

$$\text{RESP} = 0.0684 \text{ GPR} + 7.6618 \exp(0.093 \text{ temp}) \text{ W}, (\mu\text{mol CO}_2 \text{ plant}^{-1} \text{ s}^{-1})$$

(Fig. 5-2).

6.84% 가

가

가

. Heiman (1977)

26% 가

$$\text{RESP} = 0.26 \text{ GPR} + 4.46$$

Thornley (1970)

$$\text{Gr} = 0.0684 / (1 - 0.0684) = 0.0734$$

$$\text{RESP} = 0.0734 \text{ dW/dt} + 7.6618 \exp(0.093 \text{ temp}) \text{ W}, (\mu\text{mol CO}_2 \text{ plant}^{-1} \text{ s}^{-1})$$

가	Hesketh (1971)	Gr	0.36	0.38
Kielkiewicz (1982)		0.32	0.34	
	25			78.345($\mu\text{mol CO}_2\text{g}^{-1}$
s-1)	0.00234 g CH ₂ O g ⁻¹ s ⁻¹			Szaniawski Kielkiewicz
(1982)				0.000625 0.00121(g CH ₂ O
g-lh-1)				
898.54($\mu\text{mol CO}_2 \text{ plant}^{-1}\text{h}^{-1}$)				131.38($\mu\text{mol CO}_2 \text{ plant}^{-1}$
h-1)			14.6%	, Marcellis
(1994)가		13	15%	

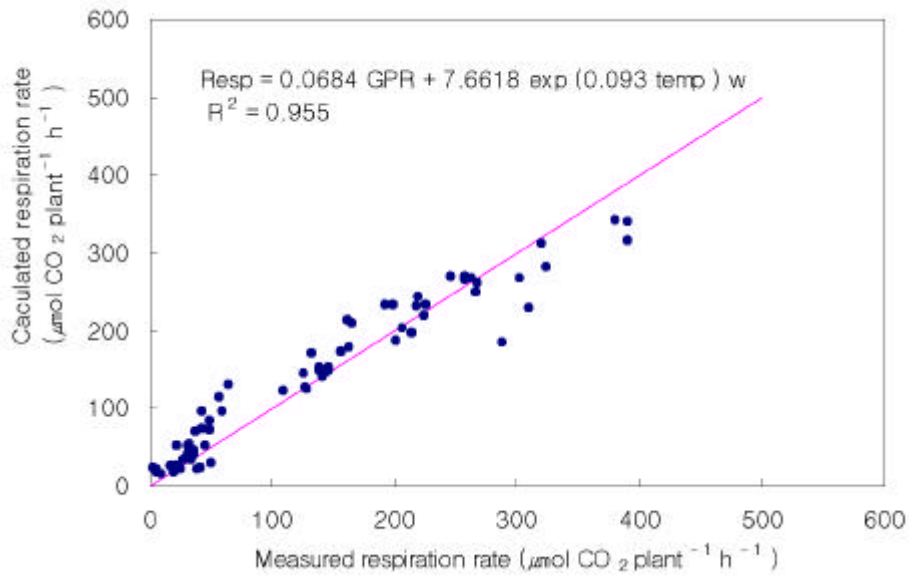


Fig. 5-2. Comparisons of measured values of shoot respiration rate with predicted values by the equation

3.

. glucose sugar

(Salisbury and Ross, 1992).

6:30 , 18:00

Fig. 5-3 .

glucose / 26/14

20/14 18:00 , 21:00

, 23:00 , 06:00 , 08:00

5-1 . glucose

가 가

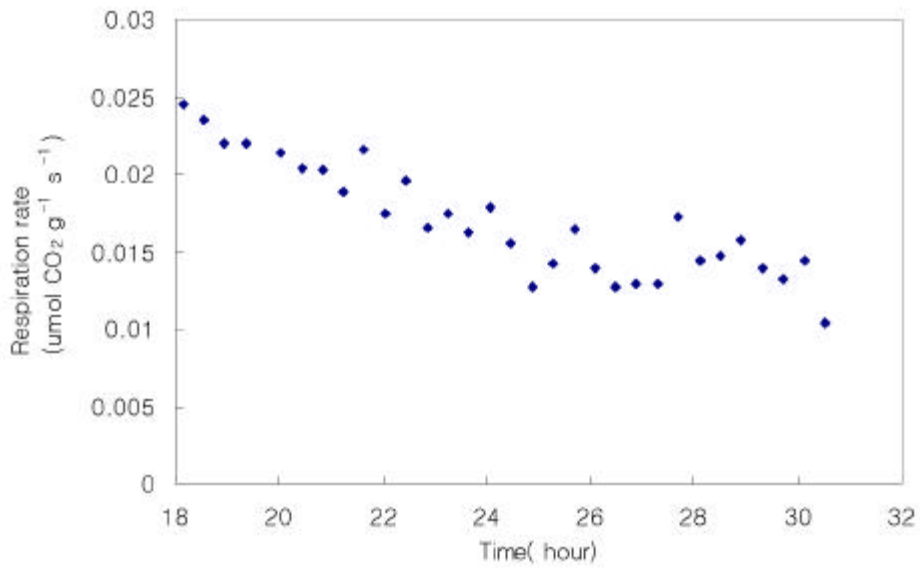


Fig. 5-3. Variations of shoot respiration of cucumber in dark period

5-1. glucose

	26/14		20/14	
	Glucose (%)	Starch (%)	Glucose (%)	Starch (%)
18:00	2.6	19.3	2.4	9.6
21:00	3.2	19.2	4.4	8.9
23:00	2.9	20.0	2.5	7.5
06:00	7.7	16.7	7.6	7.2
08:00	5.1	15.7	5.5	6.0

4.

/ 26/26 N 가 3, 6, 11mmol
09:00 18:00

12 ,
 5-2 . 가
 (luxury absorption) ,
 . 가
 . 가
 가
 (Fig. 5-3)
 19:00 0.025 ($\mu\text{mol CO}_2\text{g}^{-1}\text{s}^{-1}$)
) (Fig. 5-3) 0.021 ($\mu\text{mol CO}_2\text{g}^{-1}\text{s}^{-1}$) (5-2)
 가

(Veen, 1981). Penning de Vries (1975)

(shoot) ,

, Fig. 5-3

0.010($\mu\text{mol CO}_2\text{g}^{-1}\text{s}^{-1}$)

/ 26/26 N 3, 6,

11mmol ,

5-3

5-4 .

5-4

RGRn,

$$dN/dt = RGRn N,$$

N (g plant-l) .

dN/dt N 09:00

5- 5 .

5- 2. N

	N (mmol)	(μ mol CO ₂ g ⁻¹ s ⁻¹)
09:00	11	.01502
	6	.01701
	3	.01896
18:00	11	.02125
	6	.01582
	3	.02023
		.01805

5- 3. / 26/26 N

	N (mmol)	_____ (%)		
1 23	3	3.72	3.28	3.71
	6	4.23	3.35	3.57
	11	4.91	3.96	4.46
26	3	4.18	3.40	3.89
	6	5.25	4.35	3.20
	11	6.02	4.75	4.65
29	3	4.20	3.76	3.82
	6	4.88	4.17	4.07
	11	5.08	5.03	4.24
2 1	3	4.28	3.16	4.23
	6	3.82	3.25	3.04
	11	4.06	3.79	3.63
4	3	4.62	3.57	4.35
	6	4.85	3.54	4.13
	11	5.50	4.71	4.65

5- 4.

(g plant-1)

		N		
		3mmol	6mmol	11mmol
1	23	.157	.189	.114
	26	.298	.375	.269
	29	.392	.580	.326
2	1	.507	.610	.362
	4	.860	1.121	.658
RGRn (gN gN-1d-1)		0.1311	0.1349	0.1268

5- 5.

09:00

		N (mmol)	(mmol CO2 d-1)	dN/dt (g N d-1)
1	26	3	0.72743	.033687
		6	0.65734	.044058
		11	0.41820	.025913
1	29	3	1.29988	.049919
		6	1.36120	.066037
		11	0.57355	.037908
2	4	3	4.63677	.109618
		6	6.15484	.148356
		11	1.31378	.081122

5- 5

09:00

0.010 ($\mu\text{mol CO}_2 \text{ g}^{-1} \text{ s}^{-1}$)

dN/dt

(R)

$$R = 18.556 \text{ dN/dt}$$

, mmol CO₂ 18.556 mmol CO₂
 0.5552 g CH₂O가 1g N ,
 가 .

6

1

2

canopy

, canopy

LI-COR

LAI-1800 Plant canopy analyser

3

1.

(shoot dry weight)
(leaf weight ratio)

. 98 5 (Ws)
(LDW) (Fig. 6- 1).

$$LDW = 0.6584 Ws$$

0.6589 , 1996 9 0.6116 , 97 12
0.6907 , 98 3 0.6423 .
Marcelis (1994) 가 가
, Horie (1979)
. 97 12 가
가 .

leaf/shoot
가 가

4

(Tilman, 1988).

/ (Rls) (t) /

$$R_{1s} = 0.7372 - 0.00193 t$$

(WL)

$$WL = R_{1s} \cdot W_s$$

(LA)

(LDW)

(Fig. 6-2).

$$LA = 432.23 LDW - 4.241 LDW^2$$

가

(SLA)

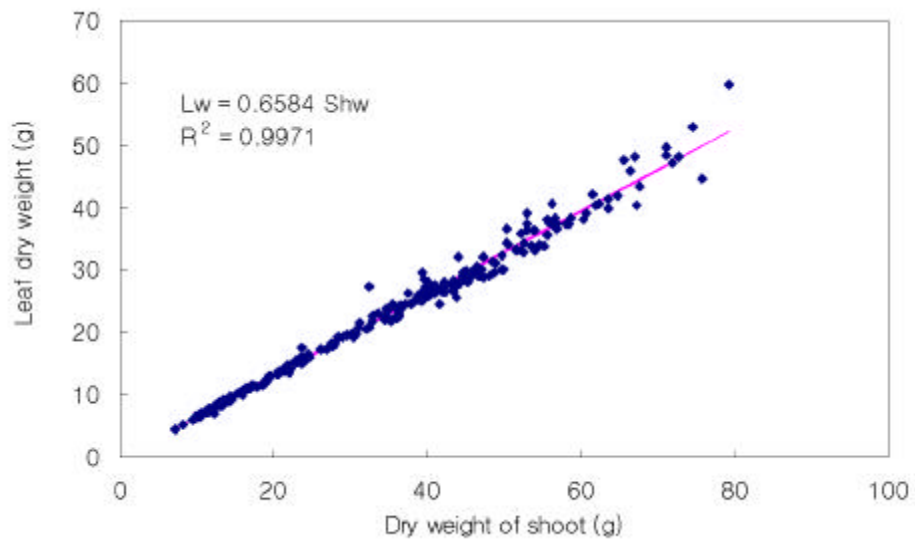


Fig. 6-1. Estimation of leaf dry weight by leaf weight ratio

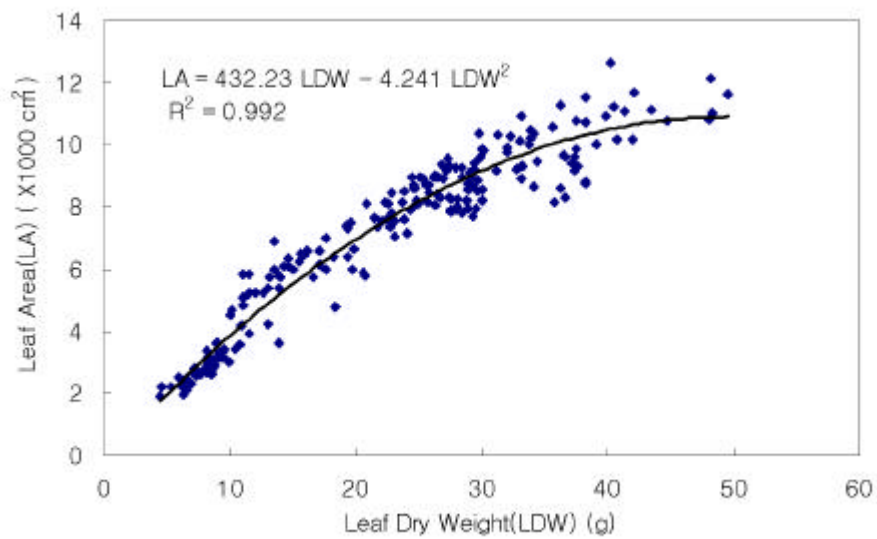


Fig. 6-2. Relationship between leaf area and leaf dry weight

2. (LAI)

canopy

,
canopy

. Lambert- Beer

canopy

(I)

canopy

I_0

$$I = I_0 \exp(-k \text{ LAI})$$

, , k (extinction coefficient) ,

LAI

가 (LDW)

(P_s)

$$\text{LAI} = (11.831 + 1.6832 \text{ LDW})/P_s$$

(Fig. 6-3).

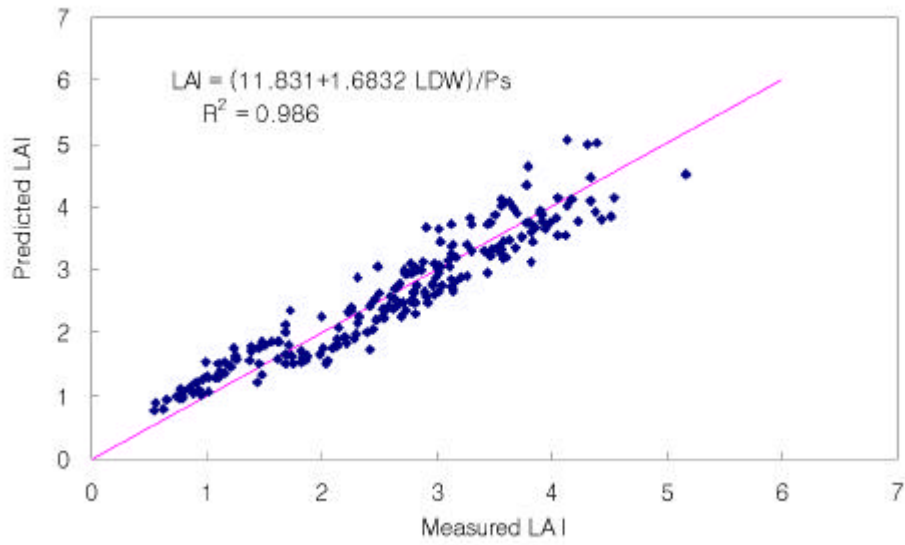


Fig. 6-3. Comparisons of measured values of leaf area index with predicted values by the equation

Plant canopy analyser

$$k = - 0.3427$$

canopy

Fig. 6-4.

3.

(Pg)

$$P_g = \int_0^{LAI} GPL(I) dl$$

$$GPL = \frac{I}{(240.1649 + I)} (1 - 0.8865 \exp(-0.0018 CO_2))$$

(GPL1)

$$GPL1 = 38.8688 \frac{T}{(7.5397 + T)} \frac{L}{(240.1649 + L)} (1 - 0.8865 \exp(-0.0018 CO_2)),$$

$$GPL2 = 24.743 / (1 + 6.0343 \exp(-0.3689 N_s))$$

$$GPL = GPL1 \cdot GPL2$$

$$GPL = 1.7858 / (1 + 5.1729 \exp(-0.4161 N_s)) \cdot GPL1, (\mu mol CO_2 (m^2 leaf)^{-1} s^{-1}),$$

N_s

$$P_g = \int_0^{LAI} 1.7858 / (1 + 5.1729 \exp(-0.4161 N_s)) \cdot GPL1 dl$$

$$= 69.4119 \frac{T}{(7.5397 + T)} (1 - 0.8865 \exp(-0.0018 CO_2)) \cdot$$

$$\frac{1}{(1 + 5.1729 \exp(-0.4161 N_s))} \int_0^{LAI} \frac{I}{(240.1649 + I)} dl$$

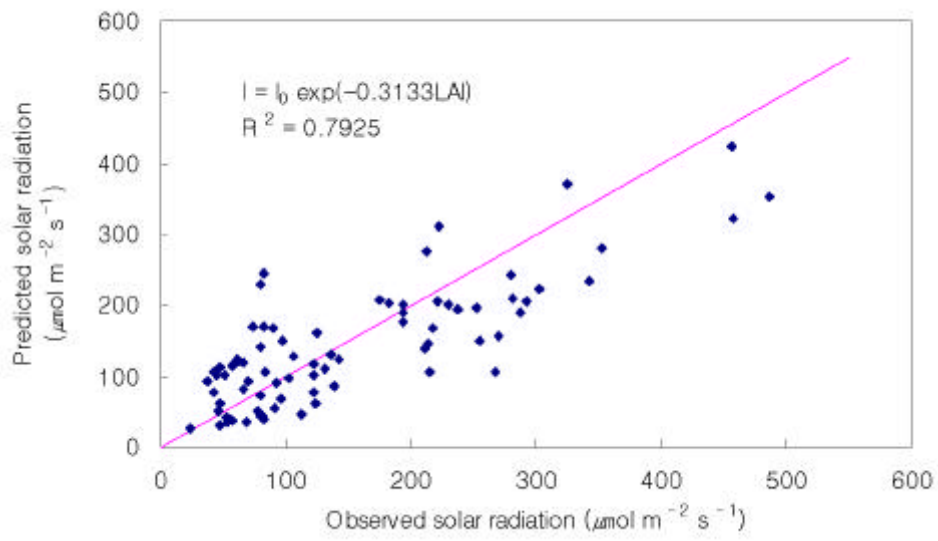


Fig. 6-4. Comparisons of measured values of solar radiation under differdnt LAI with predicted values by the equations

7

N

가

1

70%

25 28

가

23 25

가

1

6 18

4 6

12 13

가

가

N

가

Shoot/Root

(Brouwer and de

Wit, 1969)

(functional

equilibrium)

가

가

N

가

가

가 가

가

S/R

가

(Brouwer and

de Wit, 1969 ; Thornley 1972a, 1972b).

가 가

가

100Klux 가 가 50

60Klux CO2

40 60Klux

60 80%

가 가

가 , ,

가 N

가

2

1.

가. / 23/16 N

1997 6 2 (F1 HYBRID

WINTER LONG GREEN)

CG 108 Growth chamber ()

15 6 20 48l 6 N 60

400 $\mu\text{mol m}^{-2} \text{s}^{-1}$, CO2

340 \pm 10ppm, 70%, 10 , Hoagland

N 3 , 3mmol, 6mmol, 11mmol

/ 23/16 N
 7 7 2 3
 10
 , ,
 Glucose, Starch, NO₃⁻, NH₄⁺, T-N()
 . / 26/26 N
 1997 12 26 (F1 HYBRID
 WINTER LONG GREEN) , 1 10 . CG 108
 GROWTH CHAMBER() 가 , /
 26/26 가
 . 1 12 3 , 17 4 , 19 5
 / 26/26 N
 3mmol, 6mmol,
 11mmol N 3 , 09 18 1 1 23
 3 , , ,
 LCA-3 PLC
 , 09 18
 YSI MODEL 5300
 , Glucose,
 Starch, NO₃⁻, NH₄⁺ .

. /
 / CG 108 / 26/14 PGV 36
 / 20/14 . /
 ,

가 /

1998 3 25 (F1 HYBRID
WINTER LONG GREEN) 350 10 petri dish
2 28 INCUBATOR 38
0.5- 1.0cm

4 18

CO2 340 ± 10ppm
, 400 μ mol m-2 s-1, 70%, 10 ,
Hoagland CG 108 N 3mmol, 6mmol,
11mmol 3 , PGV36 N 6mmol . /

15 5 2 1 3 , N
3 , ,
, , Glucose, Starch, NO3-, NH4+

. N 6mmol, / 24/14 PGV 36
1998 4 29 10
, 4 29 5 1 . 5 1
PGV 36 / 24/14 , 5 23
. N 6mmol, 400 μ mol m-2 s-1,
15 6 6
3 6 (6 6 , 9 , 12 , 15 , 18 , 21) 3
, , , , ()
. , Glucose,

Starch, NO₃⁻, NH₄⁺

. / 26/14 N 6mmol
1998 4 29 (F1 HYBRID
WINTER LONG GREEN) 10 , 4 29 5 1
, 5 1 5 23 (22)
CG 108 / 26/14
N 6mmol (0%, 15%, 25%) 0%,
15%, 25% 3 ,
15 6 6 3 , ,
, , , , ,
Glucose, Starch, NO₃⁻, NH₄⁺

. / 24/14 , N 6mmol
Lamp 5
. 1998 6 4 10 (F1
HYBRID WINTER LONG GREEN) , 6 4 6 6
6 6 , 23 6 29
. PGV 36 / 24/14 , Halogen
Lamp 5 , 6mmol ,
/ 24/14 , N 6mmol Halogen Lamp 5
. 15 1
3 6 (7 14 , 17 , 20 , 23 , 26 , 29)
3 , , ,
, , () , Glucose,
Starch, NO₃⁻, NH₄⁺

. N
 1998 7 4 10
 , 7 4 7 6 38 , 7 6
 , 7 29 PGV 36 / 24/14
 . Halogen Lamp 5
 , Hoagland N 2 0.1
 1.0mmol .
 N
 , 7 29 10
 , 15 N 3
 3 , , ,
 , () , Glucose, Starch, NO₃⁻, NH₄⁺

2.

(F1 HYBRID
 WINTER LONG GREEN) 3
 6 3 ,

T-N(), NH₄⁺, NO₃⁻, GLUCOSE, STARCH가

가. T-N()

Kjeldahl 가
 80 dry oven 48 24
 70 dry oven 1

. 0.1g 가 Kjeldahl flask
 Blank 1g selenium 5Mℓ
 가 가 . 가
 Kjeldahl flask 380 3
 . 가 flask 가
 가 100Mℓ
 0.2Mℓ , 10M NaOH
 50Mℓ Na- nitroprusside, 50Mℓ Na- hypochlorite 2.5Mℓ
 10 660nm spectrophotometer

. Glucose
 0.1g 15Mℓ 80% ethanol 10Mℓ
 가 80 85 30
 4000RPM 10 50Mℓ .
 3 80 85
 2 3
 . 0.5Mℓ
 5Mℓ Anthrone 가 vortex mixer . 100
 7.5
 2 625nm spectrophotometer
 glucose .

. NH₄()
 glucose 0.25Mℓ , 0.125Mℓ
 cyanide/acetate buffer 가 0.125Mℓ 3% ninhydrine methoxy
 ethanol 가 15

2.5M 1:1 propanol/water 가

570nm

NH4+

. NO3-()

glucose

0.2M

0.8M 5g salicylic acid

가 100M 96% 가

20

19M NaOH 40g 500M

가

410nm

NO3-

. STARCH

glucose

dry oven 1

가 2M

가 100 15

2M 9.2N HClO4 가

15 vortex mixer

6M 가

4000RPM, 10

50M vol.flask

glucose

starch

3

1. /

/

/

가

/

가 7-1

/ 26/14

1 4

가

7-1. /

/ ()		(cm)												
		1	2	3	4	5	6	7	8	9	10	11	12	13
26/26	1 26	1.0	1.4	2.5	6.4	8.2	9.6	9.3	7.2	4.5	2.9	1.6	1.2	1.0
26/14	6 18	2.1	1.2	1.3	1.9	6.1	8.7	9.9	8.7	9.4	8.3	5.2	2.4	
24/14	7 29	1.3	1.2	2.4	8.4	8.4	9.1	9.7	9.4	7.8	4.0	1.8		

2. /

/ , 7-2 , 7-3
 가
 , 가 가 /
 /
 26/26 가 가 0.1357 , / 가 가
 26/14 가 0.1109 가 , ,
 / 가
 26/26 가 가 /

7-2. /

/ ()			_____			
			(g)			(cm ²)
23/16	7	7	1.04	.38	.23	311.4
		9	1.41	.45	.32	327.9
		12	1.76	.49	.30	490.9
		14	2.45	.77	.51	630.0
		17	3.96	1.18	.55	1028.6
		19	5.34	1.60	.62	1239.7
26/26	1	23	3.39	.79	.54	1044.1
		26	5.34	1.68	.66	1914.7
		29	8.32	3.15	1.05	2975.9
	2	1	11.22	4.21	1.45	4015.1
		4	15.66	5.96	3.62	5496.7
26/14	6	6	1.67	.36	.36	633.5
		9	2.48	.56	.45	889.5
		12	2.89	.92	.55	1259.3
		15	4.82	1.53	.71	2129.9
		18	5.67	1.94	.71	2618.8
		21	8.12	2.74	1.09	3355.3
24/14	7	14	1.00	.22	.16	323.8
		17	1.60	.33	.44	569.6
		20	2.51	.59	.54	895.7
		23	3.50	.98	.62	1236.2
		26	4.45	1.36	1.07	1699.8
		29	5.32	1.71	1.00	1893.1

7-3. /

/ ()					
23/16	.1313	.1346	.1213	.0816	.1237
26/26	.1357	.1268	.1650	.1526	.1354
26/14	.1109	.1038	.1370	.0682	.1152
24/14	.1184	.1120	.1429	.1140	.1184

3. N

가.

가 (Exponential growth model)

$$dW/dt = rW,$$

, W r .

,

3가 .

Hoagland N 11mmol N

11mmol N 3mmol N 6mmol

/ 23/16 26/26 ,

N 0.1mmol 1.0mmol

가 가 7-4, 7-5, 7-6 .

, 5%

가 .

7-7 .

N 가 6mmol

가 , 11mmol .

11mmol

N

7-8

N 가

Shoot/Root (S/R)

N 가

가

7-4. /

26/26

N

	N (mmol)	Shoot/Root (S/R)			
		(cm ²)	(g)		
1 23	3	920.4	3.035	.758	.515
	6	1044.1	3.391	.794	.543
	11	702.8	1.791	.445	.198
26	3	1866.6	5.153	1.635	.693
	6	1914.7	5.339	1.682	.663
	11	1419.7	3.349	1.019	.415
29	3	2329.4	6.367	2.493	.802
	6	2975.9	8.325	3.152	1.053
	11	1881.7	4.421	1.602	.482
2 1	3	2836.0	8.166	3.449	1.135
	6	4015.1	11.222	4.207	1.449
	11	2660.5	6.101	2.363	.678
4	3	3804.3	12.590	5.017	2.273
	6	5496.7	15.665	5.964	3.625
	11	3336.8	8.469	3.128	.963

		N (mmol)	————— (cm ²) (g)			
7	7	3	282.6	1.268	.421	.311
		6	311.4	1.041	.383	.227
		11	311.5	.960	.366	.197
9		3	375.6	1.306	.387	.281
		6	327.9	1.407	.452	.319
		11	337.4	1.316	.439	.271
12		3	494.3	1.750	.537	.322
		6	490.9	1.765	.486	.304
		11	533.1	1.603	.516	.268
14		3	489.9	1.831	.607	.395
		6	630.0	2.450	.771	.509
		11	689.0	2.058	.685	.379
17		3	872.1	3.296	1.165	.422
		6	1028.6	3.956	1.178	.547
		11	1083.4	3.563	1.178	.458
19		3	1136.7	4.524	1.365	.653
		6	1239.7	5.336	1.597	.615
		11	1154.2	4.069	1.385	.511

7-6. / 24/14 N

		N				
		(mmol)	(cm ²)	(g)		
7	29	0.1	236.9	.37	.13	.09
		1.0	263.1	.42	.15	.10
8	5	0.1	365.9	1.09	.20	.28
		1.0	551.0	1.41	.27	.28
8		0.1	529.7	1.25	.28	.34
		1.0	648.1	1.62	.40	.45
11		0.1	838.5	1.63	.47	.67
		1.0	1072.6	2.31	.65	.60
14		0.1	1259.4	2.81	.78	.95
		1.0	1623.5	3.43	.99	.98
17		0.1	1613.9	3.16	1.01	.86
		1.0	1958.8	4.12	1.26	1.06
20		0.1	1706.9	3.75	1.28	1.10
		1.0	2155.1	4.86	1.47	1.52

7-7.

/	N					
()	(mmol)					
23/26	3	.1083	.1074	.1109	.0612	.1105
	6	.1313	.1346	.1213	.0816	.1237
	11	.1200	.1217	.1153	.0770	.1206
26/26	3	.1202	.1102	.1509	.1154	.1085
	6	.1357	.1268	.1650	.1526	.1354
	11	.1318	.1236	.1580	.1218	.1248
24/14	0.1	.1205	.1177	.1324	.1284	.1162
	1.0	.1230	.1219	.1290	.1382	.1162

7-8.

, S/R SLA

/ ()	N (mmol)							(%)
								S/R SLA
23/26	3	66.3	21.2	12.4	87.6	7.384	262.7	
	6	67.1	20.9	12.0	88.0	7.749	260.0	
	11	66.3	22.5	11.2	88.8	8.229	306.0	
26/26	3	66.5	23.5	10.0	90.0	9.237	336.2	
	6	67.2	22.5	10.3	89.7	9.162	346.5	
	11	69.1	23.0	7.9	92.1	11.768	414.4	
24/14	0.1	63.4	17.8	18.8	81.2	4.428	475.5	
	1.0	64.9	18.2	16.9	83.1	4.982	467.7	

S/R (functional equilibrium)
(Brouwer and de Wit, 1969)

가 가
N 가 가
가 가
가

S/R 가
(Brouwer and de Wit, 1969;
Thornley 1972a, 1972b).

4. 가

가
CG 108 400 μmol m⁻² s⁻¹ 0%, 15%,

25% 3

, PGV 36

2 5

가 7-9 7-10

7-11

가

, S/R SLA,

7-12

, S/R

, N S/R

7-9. / 26/14 , N 6mmol

	/	(%)	26/14			
			(cm ²)	(g)		
6	6	0	633.5	1.67	.36	.36
		15	401.0	.92	.23	.18
		25	370.8	.93	.21	.22
9		0	889.5	2.48	.56	.45
		15	664.4	1.47	.39	.22
		25	636.4	1.48	.34	.29
12		0	1259.3	2.89	.92	.55
		15	1110.2	2.16	.62	.36
		25	899.0	1.98	.57	.36
15		0	2129.9	4.82	1.53	.71
		15	1298.4	2.26	.68	.36
		25	1345.1	2.99	.92	.46
18		0	2618.8	5.67	1.94	.71
		15	2011.3	3.61	1.16	.57
		25	1684.2	3.96	1.17	.47
21		0	3355.3	8.12	2.74	1.09
		15	1997.4	3.64	1.10	.51
		25	1559.2	3.64	1.14	.56

7-11.

/	()	(%)	26/14				
26/14		0	.1109	.1038	.1370	.0682	.1152
		15	.0949	.0916	.1065	.0768	.1096
		25	.1019	.0970	.1204	.0606	.1000
24/14		2	.0946	.0952	.0922	.0851	.1218
		5	.1184	.1120	.1429	.1140	.1184

7- 10. / 24/14 , N 6mmol

				(cm ²)	(g)		
6	6	2		180.2	.49	.15	.14
	9			216.6	.61	.18	.13
	12			348.8	.88	.24	.23
	15			528.5	1.13	.25	.31
	18			696.3	1.37	.42	.42
	21			1062.1	2.12	.62	.39
7	14	5		323.8	1.00	.22	.16
	17			569.6	1.60	.33	.44
	20			895.7	2.51	.59	.54
	23			1236.2	3.50	.98	.62
	26			1699.8	4.45	1.36	1.07
	29			1893.1	5.32	1.71	1.00

7- 12. , S/R SLA

/ ()	(%)	_____ (%)					
		S/R SLA					
26/14	0	.686	.200	.114	.886	8.158	415.1
	15	.690	.198	.111	.889	8.066	513.7
	25	.690	.191	.119	.881	7.749	431.0
24/14	2	.651	.184	.165	.835	5.210	432.7
	5	.681	.177	.142	.858	6.240	354.6

8 가

1

가 . 가
, 가
가 .
, ,
, 가 , ,
가 .
가

2

1998 , 가
5 , 40
4 21
9 .
,
4

3

4

. 3 8-1, 8-2, 8-3
 . 8-1 4 21 21 5 ,
 2, 3 , 1, 4, 5
 4 29 , 1
 가 가 . 6 4 22 가 2 가
 4 27 , 7 4 24 4 26
 가 2 가
 가 3 가 4 28 . 8-2
 17 4 24 1 2
 가 1 2 24 , 25 가
 . 5 , 1 2
 , 5 3, 4
 . 5 4 26 1
 4 25 6 7
 4 28 2 가 . 8-3
 19 5 1
 . 4 24 1
 3 , 2, 4
 , 4 22 6 4 27
 5 4 23 7
 . 20 25 가
 7 8 2 4

4 5

first-set fruit inhibition (Schaffer et al., 1996), Ells (1983),

9 10

가 , ,
가

가가 가 .

8-1.

(1)

		4/21	4/22	4/23	4/24	4/25	4/26	4/27	4/28	4/29
		21	21	22	23	24	24	25	26	27
1		61.0 7.4	67.0 9.9	70.0 10.0	70.0 9.9	70.0 10.0	70.0 9.9	69.0 9.9	67.0 9.9	67.0 10.9
2		96.0 18.0	126.0 23.2	149.0 26.3	195.0 30.6	210.0 37.5	220.0 41.0			
3		44.0 10.9	97.0 14.3	102.5 15.5	112.0 21.4	142.0 25.0	182.0 28.0	203.0 31.4	240.0 36.5	
4		51.0 5.0	57.0 7.4	57.5 7.7	59.0 7.6	60.0 7.6	57.0 7.6	59.0 7.7	57.0 7.5	54.4 7.4
5		50.0 6.0	52.0 6.5	53.0 7.0	55.3 7.0	55.0 7.0	55.0 7.0	56.5 7.2	57.0 7.2	59.0 7.5
6			34.5 4.4	37.0 4.6	43.7 5.7	49.0 6.0	55.0 6.5	59.0 8.3	69.0 9.2	95.0 12.0
7					32.0 4.4	35.0 4.4	35.0 4.4	45.0 5.1	53.0 5.7	67.3 7.4

8- 2.

(2)

		4/21	4/22	4/23	4/24	4/25	4/26	4/27	4/28	4/29
		17	19	21	22	22	23	24	24	25
1		90.9 14.4	107.0 18.2	136.0 21.2	190.0 27.7	214.0 31.5	240.0 36.0			
2		75.0 11.7	92.0 14.1	100.0 15.1	133.0 21.0	163.0 24.8	195.0 30.4	220.0 33.3	248.0 36.5	
3		57.0 7.7	62.0 9.0	64.0 9.6	65.0 9.7	65.0 6.2	64.4 9.0	65.5 6.1	64.0 9.1	64.0 9.4
4		54.0 5.5	60.0 7.3	59.0 6.6	62.0 6.9	62.0 6.6	62.4 7.5	63.0 7.4	64.0 7.2	62.8 7.0
5		32.0 4.5	42.7 5.8	47.0 5.5	53.0 6.5	57.0 7.9	70.0 7.4	77.0 7.3	95.0 7.2	132.6 16.0
6						42.2 5.8	45.7 5.9	50.0 6.0	59.0 7.0	76.4 8.8
7						36.0 4.4	38.6 5.0	43.0 5.3	49.0 6.3	62.4 7.5

8- 3.

(3)

		4/21	4/22	4/23	4/24	4/25	4/26	4/27	4/28	4/29
		19	19	20	21	22	23	23	24	24
1		140.0 20.7	173.0 25.4	230.0 29.3	230.0 34.0					
2		65.0 10.4	70.0 12.2	69.0 11.0	71.0 12.9	75.0 12.8	75.4 13.0	82.0 13.0	98.0 15.8	129.6 20.4
3		56.0 8.1	59.0 12.0	60.0 10.0	67.0 12.8	93.0 14.3	134.0 17.2	131.0 19.5	155.0 25.0	199.6 29.9
4		45.0 7.2	49.0 7.2	50.0 7.2	52.0 7.2	56.0 7.5	65.7 9.5	72.0 11.4	86.0 15.8	113.4 18.5
5		33.0 4.2	46.0 6.4	46.0 6.0	49.0 6.0	52.0 6.8	51.6 7.2	54.0 7.4	61.6 7.8	72.0 11.0
6			37.0 5.0	39.0 5.0	47.5 5.4	53.0 6.4	62.0 7.2	67.0 8.0	84.0 10.0	107.8 14.0
7					37.5 4.5	40.0 5.2	48.5 6.0	53.0 6.7	63.0 7.7	80.5 10.5

4

(V)

$$V = R L,$$

R

L

Marcelis (1992)

가

(EV)

(V)

$$EV = 1.1248 \text{ V}$$

가 (Fig. 8-1),

가

가

(FWF)

$$FWF = 0.8715 \text{ V}$$

(Fig. 8-2).

(DWF)

DWF = 0.0439 FWF

(Fig. 8-3).

8-4 . 1 4 24 4 23
 24 5.5g 가 , 2 4 26
 3.16g 가 , 3 4
 28 4.49g 가 .
 4 5g d-1 . 가 20
 75 dm² (1-11.)
 10 μmol CO₂ s⁻¹ m⁻² 15% , 10
 20 가 6.87g CH₂O d⁻¹ plant⁻¹
 90% 7.63g
 . 8-4 4 23 4 24 가
 7.4g d⁻¹ , , 2
 , 1 9 10
 .
 가 exponential growth curve
 3 가 Fig. 8-4 .
 가
 가
 . 8-4 가 1,2 3 가 4
 23 4 24 가 7.4g 3, 6, 7 8
 가 4 28 4 29 1 가 4.67g
 1 4 25 2.32g, 2
 4 27 0.94g 가

	(g)								
	1	2	3	4	5	6	7	8	
4/21	3.26	.41	.20	.06	.04	.02			3.99
4/22	5.75	.77	.35	.08	.07	.03			7.05
4/23	6.38	1.00	.31	.08	.07	.02			7.86
4/24	11.88	2.45	.69	.09	.07	.05	.03		15.26
4/25	11.88	4.08	1.37	.10	.07	.05	.03		17.58
4/26	11.88	7.24	2.65	.10	.06	.05	.03		22.00
4/27	11.88	7.24	3.48	.10	.08	.07	.05	.03	22.94
4/28	11.88	7.24	6.26	.10	.08	.11	.11	.04	25.81
4/29	11.88	7.24	10.75	.09	.08	.21	.18	.06	30.48

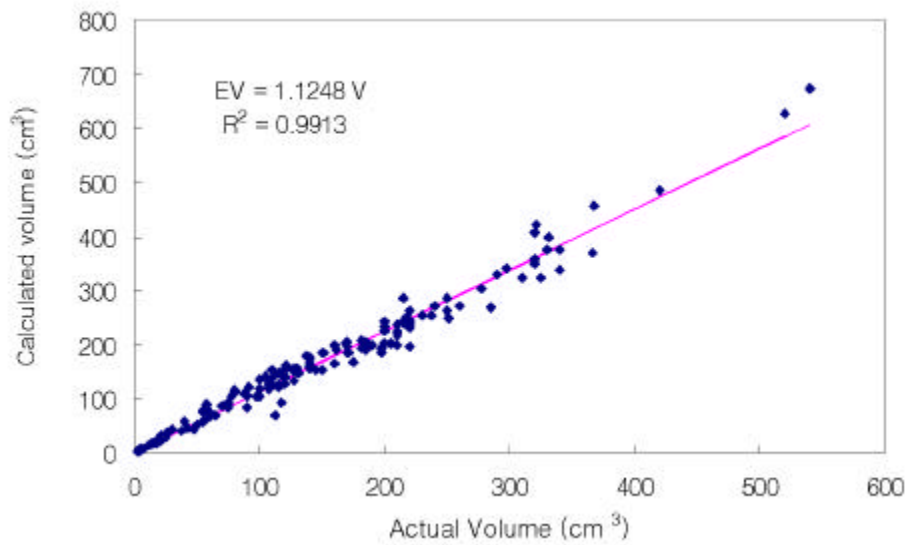


Fig. 8-1. Comparisons of values of actual volume of fruits with calculated values

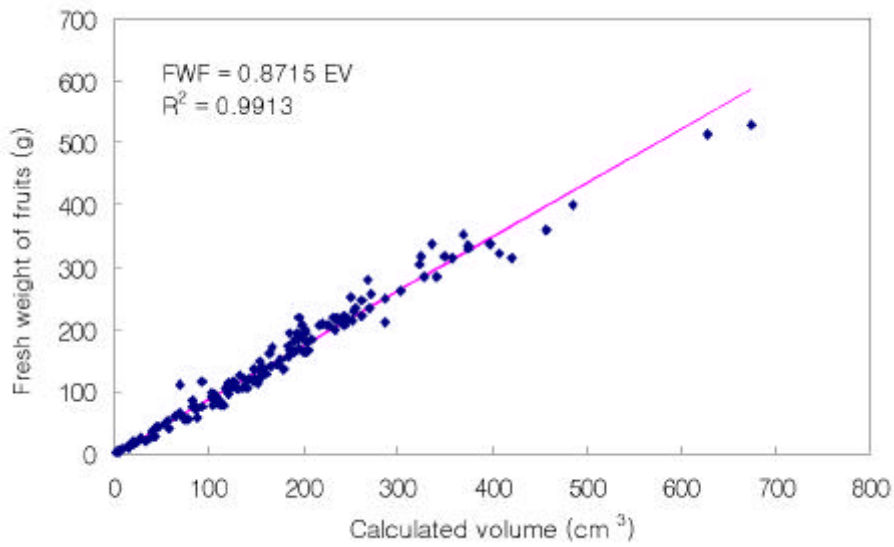


Fig. 8-2. Relationship between calculated volume of fruit and its freshweight.

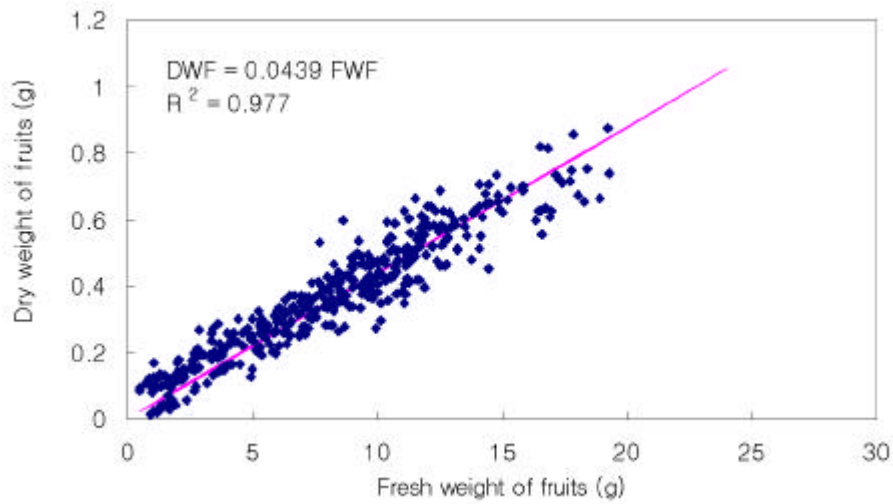


Fig. 8-3. Relationship between fresh weight of fruit and its dry weight

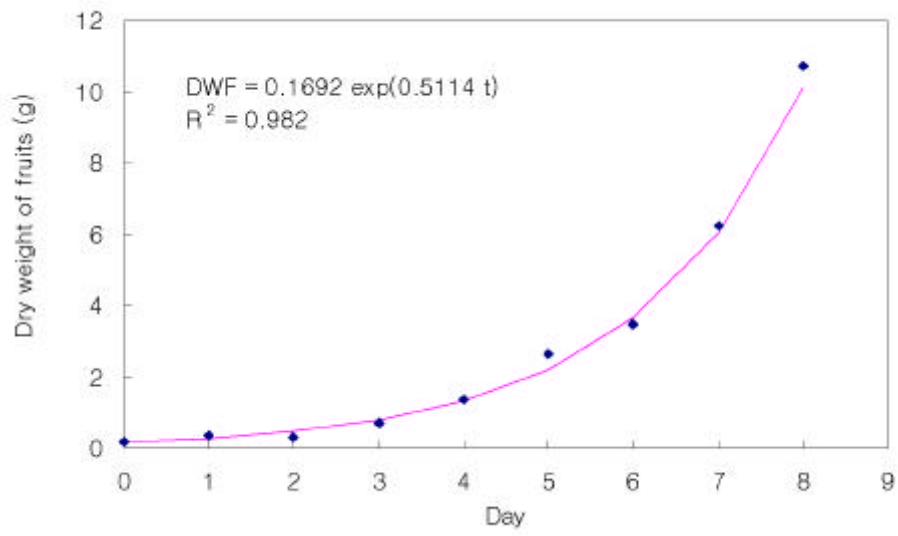


Fig. 8-4. Exponential growth of dry weight of individual fruit

9

1

가

Marcelis (1994)

13 15% 가

100

130mg CH₂O h⁻¹

Chaffer (1996)

2

Heinz Walz GmbH Gas Exchange Measuring

Station , 20
 , 가 3 12 4
 가 32 .
 가 8-4

3

1.

90% 2817mg CH₂O가
 20
 , , g g 9-1
 , 8-4
 0.34 0.71 0.55 .
 55%
 .
 mg

(Index of effectively metabolizing fruit cells, X)

X = fruit surface area / fruit dry weight

(X) g (FPS) (Fig. 9-1),

$$\text{FPS} = -0.0034 + 0.000293 X$$

g (FRS)

$$\text{FRS} = -0.0073 + 0.00056 X$$

(Fig. 9-2), g

가 3 12 4 가 32
가 9-2
0.54
가
가 12
가
가 32 2 3

g Fig. 9-3
 3 가 , 28
 32
 (temp) g (FPS)

$$FPS = 0.0071 / (1 + 19.0458 \exp(-0.1674 \text{ temp}))$$

g
 Fig. 9-4 g
 3 가
 가 g (FRS)

$$FRS = 0.0160 / (1 + 241.788 \exp(-0.2938 \text{ temp}))$$

가 가

9-1
 0.0863 μ mol CO₂ s⁻¹ fruit⁻¹
 223mg CH₂O d⁻¹ fruit⁻¹ (0.0863 x 10⁻⁶ x 44g/mol x 30/44 x 3600 sec/hr
 x 24 hr/d) 8-4 2
 446mg CH₂O d⁻¹
 plant-1 가 3.31g (8-4),

$$446/(2979) = .1497$$

15% 가
 . Marcellis (1994) 13 15% 가

2. (transpiration rate)

8-4 4 21 3.99g 8 4 29
 30.48g 가 가 3.31g d-1
 . 90% 가 가 2.98 g
 CH₂O d-1 .
 15% ,
 50% 7.5% 가

133 mg CH₂O
 h-1가 (2979mg CH₂O d-1 x 1.075/(24 h d-1)) . Chaffer (1996) 100
 130mg CH₂O h-1

9- 1. 20

(g)	1g		1g	
	($\mu\text{mol CO}_2$ fruit-ls-l)	($\mu\text{mol CO}_2$ fruit-ls-l)	($\mu\text{mol CO}_2$ g-ls-l)	($\mu\text{mol CO}_2$ g-ls-l)
7.891	.040530	.082410	.005136	.010444
7.485	.034950	.052050	.004669	.006954
8.464	.048840	.096960	.005771	.011456
20.547	.043680	.081360	.002126	.003960
17.931	.051270	.152760	.002859	.008520
19.969	.051990	.124440	.002604	.006232
12.056	.052710	.086130	.004372	.007144
10.814	.049050	.088020	.004536	.008140
9.432	.061260	.086610	.006495	.009183
5.243	.039900	.072510	.007610	.013830
4.701	.033690	.065550	.007167	.013944
4.563	.031410	.046890	.006883	.010275

9- 2.

()	(g)	($\mu\text{mol CO}_2$ fruit-ls-l)	($\mu\text{mol CO}_2$ fruit-ls-l)	lg ($\mu\text{mol CO}_2$ g-ls-l)	lg ($\mu\text{mol CO}_2$ g-ls-l)
12.0	4.450	.013380	.010740	.003007	.002413
12.0	5.901	.012900	.015060	.002186	.002552
12.0	6.559	.015480	.015660	.002360	.002388
15.9	4.450	.014340	.018210	.003222	.004092
16.0	5.901	.010980	.019680	.001861	.003335
16.0	6.559	.017520	.026820	.002671	.004089
20.0	4.450	.026910	.050160	.006047	.011272
20.0	5.901	.014400	.059970	.002440	.010163
20.0	6.559	.020010	.072000	.003051	.010978
23.9	4.450	.032430	.058530	.007287	.013153
24.0	5.901	.023520	.069270	.003986	.011739
24.0	6.559	.033360	.082350	.005086	.012556
27.9	4.450	.040950	.070800	.009202	.015910
27.9	5.901	.030690	.077250	.005201	.013092
27.9	6.559	.038850	.093300	.005923	.014225
31.9	4.450	.035670	.080850	.008016	.018168
32.0	5.901	.025350	.085980	.004296	.014571
32.0	6.559	.034590	.108150	.005274	.016490

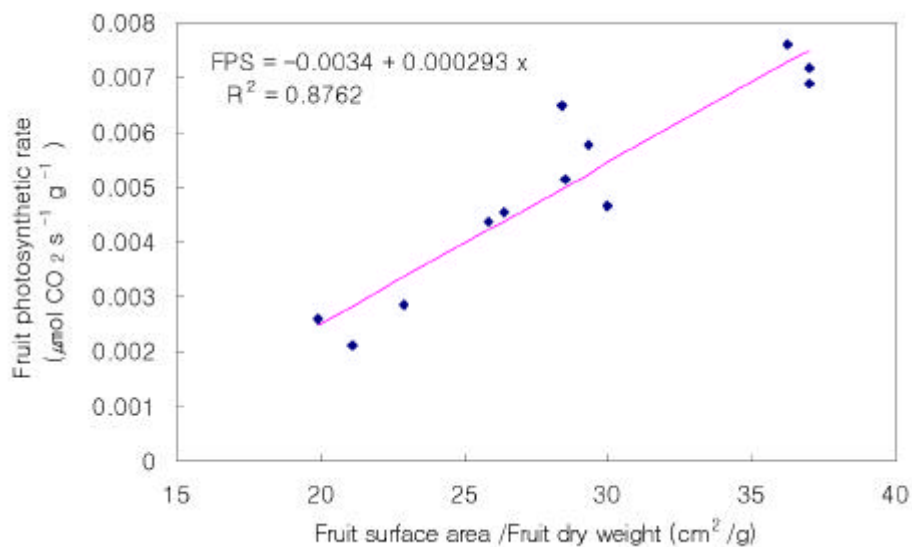


Fig. 9- 1. Relationship between fruit photosynthetic rate (FPS) and index of effectively metabolizing fruit cells (X).

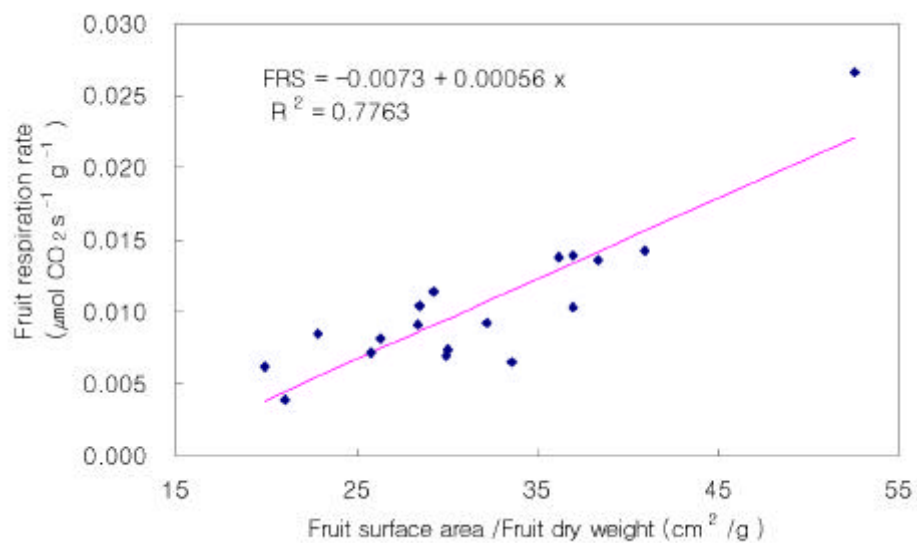


Fig. 9-2. Relationship between fruit respiration rate (FRS) and index of effectively metabolizing fruit cells (X).

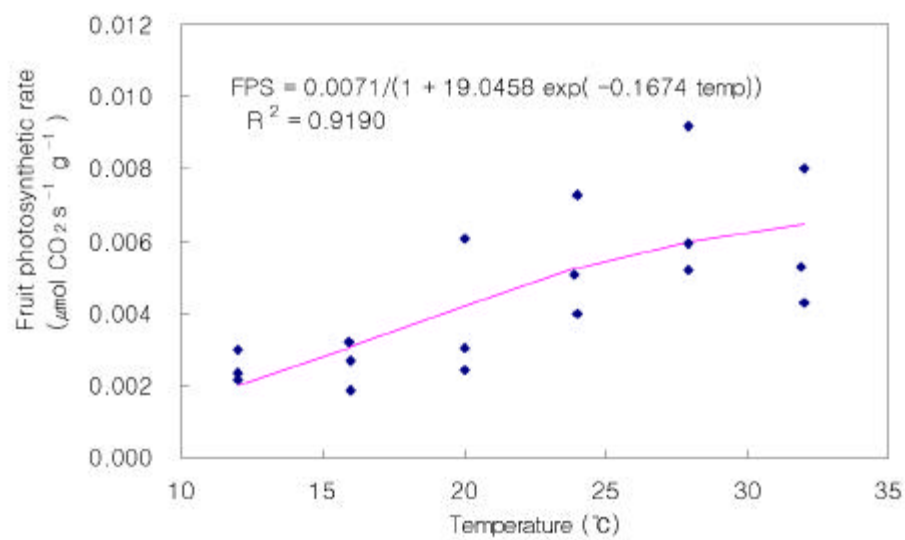


Fig. 9-3. Variations of fruit photosynthetic rate under different air temperature.

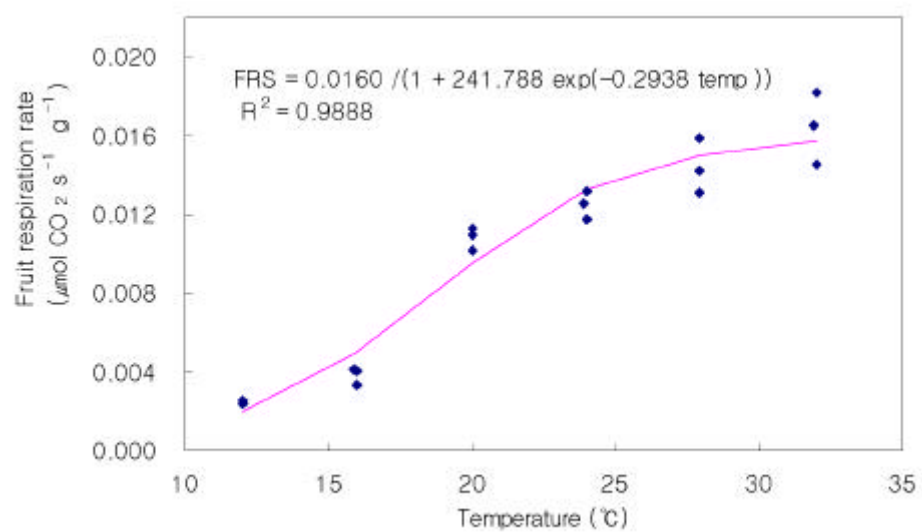
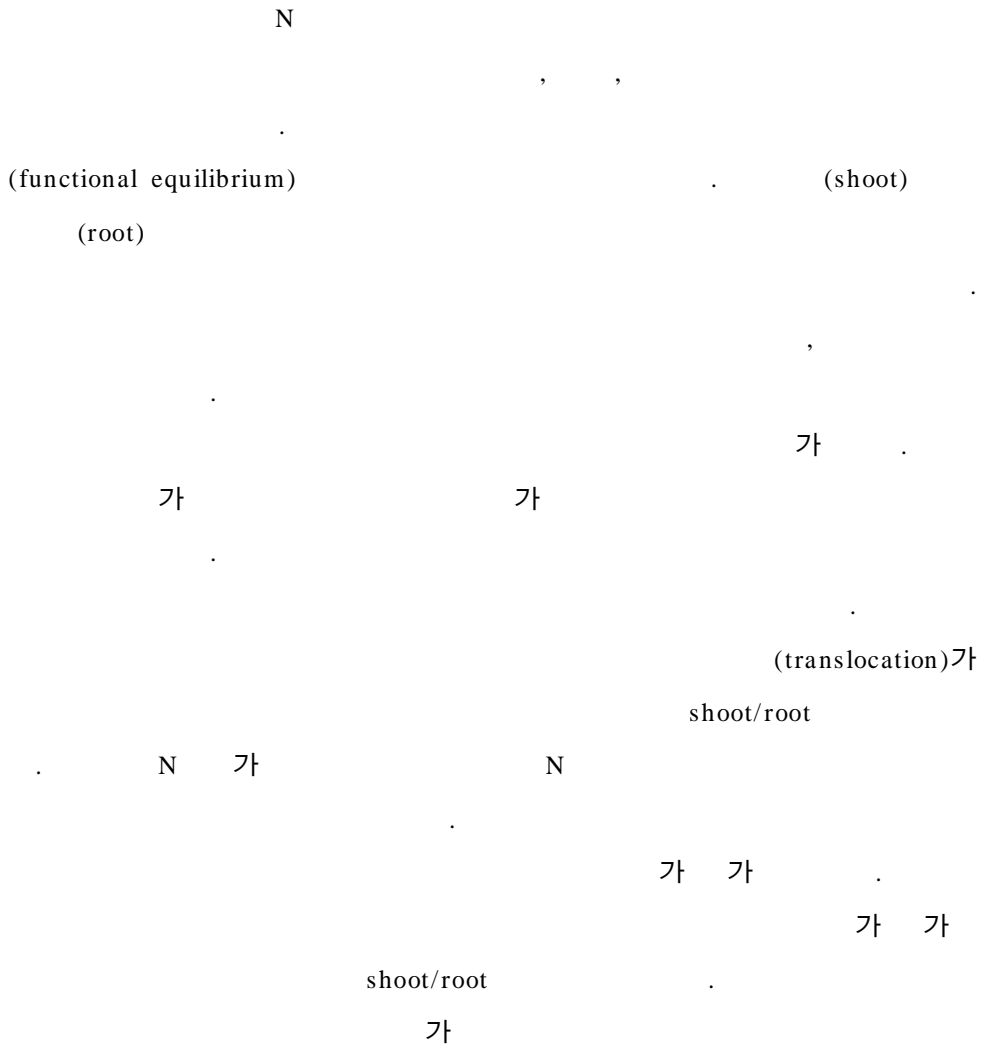


Fig. 9-4. Variations of fruit respiration rate under different air temperature.

10

1



shoot/root

shoot/root

shoot/root

shoot/root

가 shoot/root (Lim, 1990), (teleonomic approach of optimal resource allocation) (Johnson and Thornley, 1987), cost/benefit (Givnish, 1986) 가 , shoot/root , CO2 , N shoot/root 가

2

1.

가.

Fig. 10-1

(state variable) , (shoot dry weight), 가
 (soluble CH₂O) , 가 , 가
 , 가 (soluble N) , 가 , 가
 , (storage CH₂O) 10

Shoot/Root

W_s, W_r, W_f

$$dW_s/dt = k_s C_s N_s W_s,$$

$$dW_r/dt = k_r C_r N_r W_r,$$

$$dW_f/dt = k_f C_f N_f W_f$$

k_s, k_r, k_f , C_s, C_r, C_f , ,
 가 N_s, N_r N_f ,
 가 .

(T_{min}) (T_{max})

(AC)

$$AC = (T_{min} + T_{max})/2$$

2 3
(NL)

NL = -4.1782 + 0.0216 AC, (R2 = 0.9729, df=54)

620 625
가 가 8 9
가
9

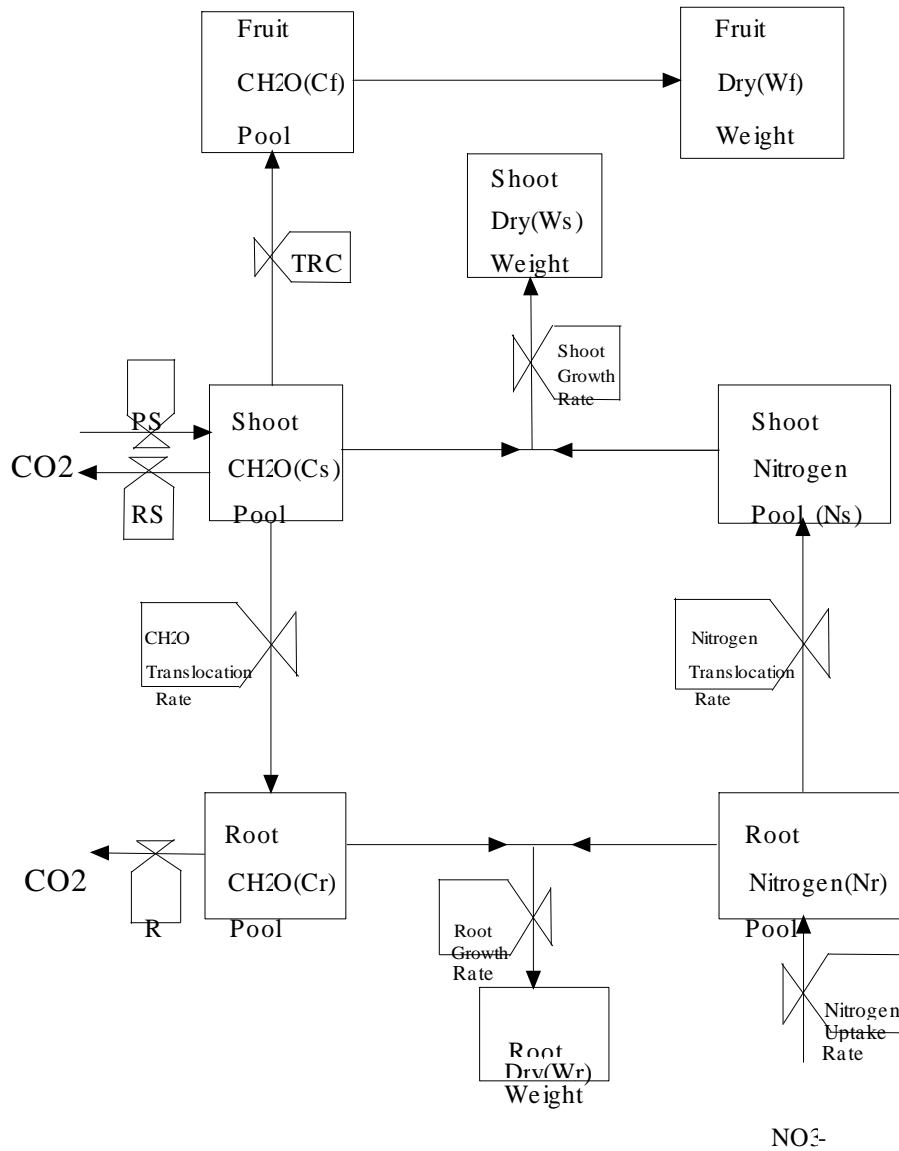


Fig. 10-1. System diagram

leaf/shoot

가 가

4

(Tilman, 1988).

(Rls)

(t)

$$Rls = 0.7372 - 0.00193 t$$

(Fig. 10-2),

(WL)

$$WL = Rls \cdot Ws$$

(LAI)

$$LAI = (11.831 + 1.6832 WL)/PS,$$

, PS

LAI

- 0.3427

LAI

$$I = I_0 \exp(-0.3427 LAI)$$

, IC

(Pg)

$$Pg = \int_0^{LAI} GPL(I)dl$$

, GPL , LAI , 1

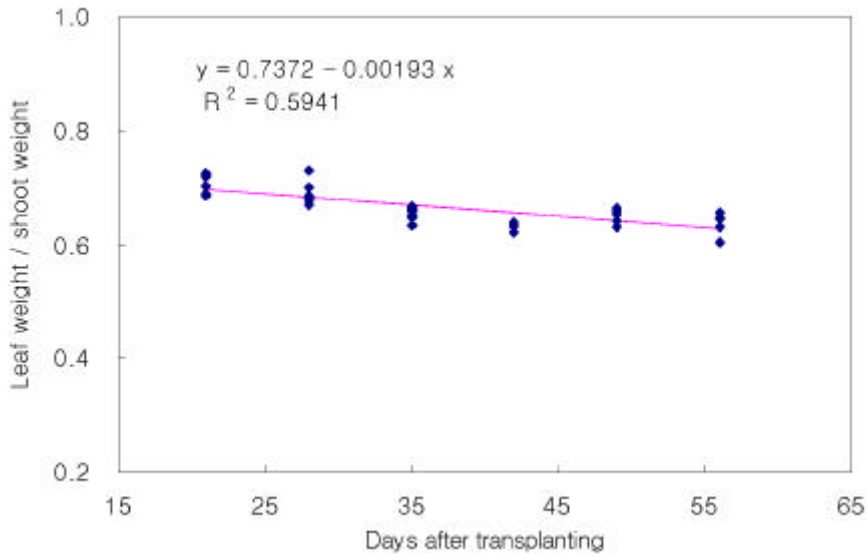


Fig. 10- 2. Temporal variation of leaf weight/shoot weight ratio.

, CO2 (GPL1)

$$GPL1 = 38.8688 T / (7.5397 + T) L / (240.1649 + L) (1 - 0.8865 \exp (-0.0018 CO_2)),$$

$$GPL2 = 24.743 / (1 + 6.0343 \exp (-0.3689 N_s))$$

. GPL1 GPL2 , , CO2

$$GPL = 1.7858 / (1 + 5.1729 \exp(-0.4161 N_s)) \cdot GPL_1, \quad (\mu \text{ mol CO}_2 \text{ (m}^2 \text{ leaf)}^{-1} \text{ s}^{-1}),$$

(Fig. 10-3), N_s .

$$\begin{aligned} P_g &= \int_0^{LAI} 1.7858 / (1 + 5.1729 \exp(-0.4161 N_s)) \cdot GPL_1 \, dl \\ &= 69.4119 T / (7.5397 + T) (1 - 0.8865 \exp(-0.0018 CO_2)) \cdot \\ &\quad 1 / (1 + 5.1729 \exp(-0.4161 N_s)) \int_0^{LAI} I / (240.1694 + I) \, dl \end{aligned}$$

Thornley (1990)

$$P_g = 69.4119 T / (7.5397 + T) (1 - 0.8865 \exp(-0.0018 CO_2)) \cdot 1 / (1 + 5.1729 \exp(-0.4161 N_s)) \cdot P, \quad (\mu \text{ mol CO}_2 \text{ (m}^2 \text{ ground)}^{-1} \text{ s}^{-1}),$$

$$P = 1/k \ln((k I_o + 69.4119(1-m)) / (k I_o \exp(-k LAI) + 69.4119(1-m)))$$

, k , (photochemical efficiency) , m

(transmission coefficient) .

$$P_g = P_m \cdot T / (7.5397 + T) (1 - 0.8865 \exp(-0.0018 CO_2)) \cdot 1 / (1 + 5.1729 \exp(-0.4161 N_s)) \cdot P, \quad (\text{g CH}_2\text{O (m}^2 \text{ ground)}^{-1} \text{ h}^{-1}),$$

$$P = 1/k \ln((k I_o + P_m(1-m)) / (k I_o \exp(-k LAI) + P_m(1-m)))$$

$$P_m = 69.4119 \cdot 10^{-6} \text{ mol} \cdot 44 \text{ g/mol} \cdot 0.68 \cdot 3600 \text{ s h}^{-1}$$

$$= 7.4765 (\text{g CH}_2\text{O (m}^2 \text{ ground)}^{-1} \text{ h}^{-1}) \text{ ----- (1)}$$

가 .

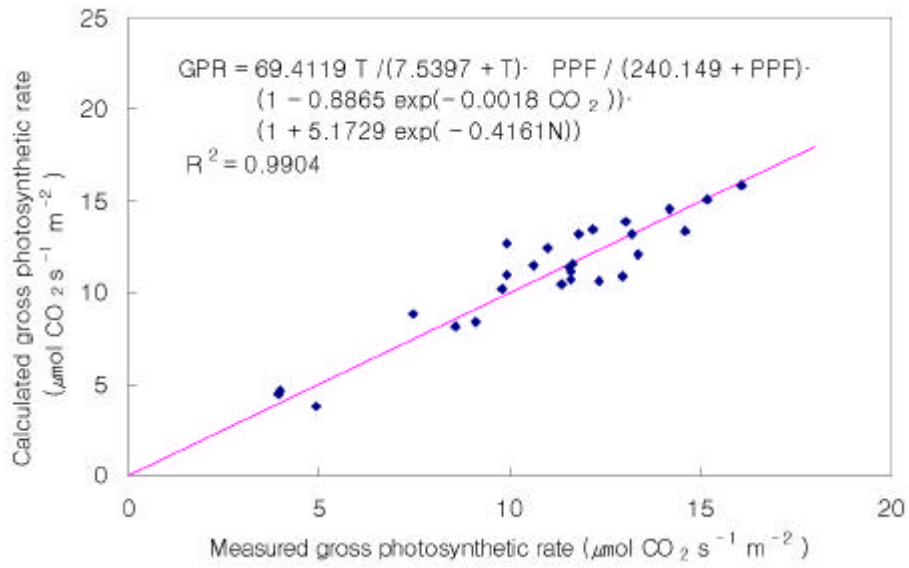


Fig. 10-3. Comparisons of measured gross photosynthetic rate and calculated values by the model equation including variations of light, temperature, CO₂ concentration and nitrogen content in leaves

(sink demand)

. Marcelis (1991)

(feedback inhibition)

end-product inhibition)

. Janoudi

Widders (1993)

25%

가

Barrett (1978), Ramirez (1988),
 Pharr (1985)
 sink demand가 가
 sink demand가
 (Thone and Koller, 1974). sink demand
 가 가
 가 , 가
 C_{smax} C_{smax} C_s
 가 sink demand가 sink demand
 가

$$T_{pg} = (C_{smax} - C_s) P_g,$$

, T_{pg} sink demand ,

(R)

(R)

$$R = 0.0734 \frac{dW}{dt} + 7.6618 \exp(0.093 T)W, (\mu\text{mol CO}_2 \text{ plant}^{-1} \text{ h}^{-1})$$

$$= 0.0734 \frac{dW}{dt} + 0.000229 \exp(0.093 T)W, (\text{g CH}_2\text{O plant}^{-1} \text{ h}^{-1})$$

(Rs1)

$$Rs1 = 0.0734 \frac{dWs}{dt} + 0.000229 \exp(0.093 T)Ws,$$

가 . 0.025 μmol
 $\text{CO}_2 \text{ g}^{-1} \text{ h}^{-1}$ 0.013 $\mu\text{mol CO}_2 \text{ g}^{-1} \text{ h}^{-1}$
 1/2 .
 20% 15%
 가 .
 (Rs) .

$$R_s = (a + b S) R_{s1}$$

, S , a b .

, (Rr)

$$R_r = 0.0734 \frac{dW_r}{dt} + 0.00339 \exp(0.093 T) W_r + R_N$$

, T () R_N .

(RN) .

$$R_N = 0.5552 \frac{dN}{dt}$$

15%

50%

(Rf) .

$$R_f = 0.075 \frac{dW_f}{dt}$$

Michaelis - Menten
 (Edwards and Asher, 1974 ; Clement 1978; Raper 1976 ;
 Pitman, 1976).

$$V = V_{max} \frac{N}{k_n + N}$$

$$V = V_{max} \frac{N}{k_n + N}$$

(Un)

$$U_n = V_{max} \frac{N}{k_n + N}$$

(Minotti and Jackson, 1970; Jackson , 1976b; Pearson
 and Steer, 1977),

$$V_{max} = \frac{Q C_r}{K_c + C_r}$$

$$V_{max} = \frac{Q C_r}{K_c + C_r}$$

Jackson (1976a) NO₃⁻
 NO₃⁻
 NO₃⁻
 N 가 ()
 가 N_{max} 가 ,

$$V_{max} = \varrho (N_{max} - N_r) C_r / (K_c + C_r)$$

가
 가 (CH₂O) ,
 가
 (net translocation rate)
 가 (net translocation rate) T
 , T (source strength) ,
 가 (sink
 demand) 가 C_{max} C_{max}

$$T_{cr} = \Phi_r C_s (C_{max} - C_r)$$

$$T_{cf} = \Phi_f C_s (C_{fmax} - C_f)$$

가 , T_{cr} T_{cf} , Φ_r Φ_f
 , C_{max} C_{fmax} 가 가

가

가
 F_{sc} F_{cs} F_{cs} 가
 F_{sc} F_{cs} 가

$$F_{cs} = \Phi_d C_s (S_{max} - S)$$

, Φ_d , S_{max} 가
 $S_{max} - S$ 가
 D ,

$$D = R_s + U_s + T_c + T_f + C_s \frac{dw_s}{dt}$$

가 , U_s , $C_s \frac{dw_s}{dt}$

가 F_{sc} D
 가 ,

$$F_{sc} = \Phi_n D (C_{smax} - C_s) S,$$

, Φ_n .
 . 가 가
 Penning de Vries (1979) 1g 0.92g

Us, Ur, Uf .

$$U_s = 0.92 \frac{dw_s}{dt},$$

$$U_r = 0.92 \frac{dw_r}{dt}$$

$$U_f = 0.92 \frac{dw_f}{dt}$$

Tolley-Henry and Raper(1986)

0.0171g/g

Hanway and Weber (1971)

1.0, 0.5 1.3%

1.5% 가 ,
 U_{sn}, U_m U_{fn}

$$U_{sn} = 0.015 \frac{dw_s}{dt},$$

$$U_m = 0.015 \frac{dw_r}{dt},$$

$$U_{fn} = 0.015 \frac{dw_r}{dt}$$

(Simpson , 1982).

(net translocation rate)

(N_{rs})

$$N_{rs} = \bar{h}_{rs} (N_{srax} - N_s) N_r$$

, \bar{h}_{rs} N_r , N_{srax} 가
 N , $N_{srax} - N_s$.
 (shoot)

N_{st}

$$N_{sf} = \mu_{sf} (N_{fmax} - N_f) N_s$$

$$, \quad \mu_{sf}$$

Fig. 10-1 compartment

, 가

$$d(W_s C_s)/dt = P_g - R_s - U_s - F_{cs} + F_{sc} - T_{cr} - T_{cf}$$

Total ,

$$dC_s/dt = (P_g - R_s - U_s - F_{cs} + F_{sc} - T_{cr} - T_{cf} - C_s dW_s/dt)/W_s$$

$$dC_r/dt = (T_{cr} - R_r - U_r - C_r dW_r/dt)/W_r,$$

$$dC_f/dt = (T_{cf} - R_f - U_f - C_f dW_f/dt)/W_f,$$

$$dN_s/dt = (N_{rs} - U_{sn} - N_{sf} - N_s dW_s/dt)/W_s,$$

$$dN_r/dt = (U_n - N_{rs} - U_m - N_r dW_r/dt)/W_r,$$

$$dN_f/dt = (N_{sf} - U_{fn} - N_f dW_f/dt)/W_f,$$

$$dS/dt = (F_{cs} - F_{sc} - S dW_s/dt)/W_s$$

2.

1998 2 .
 1998 2 5
 10 25 38 .
 2 7 , 7
 30 . 10
 3 ,
 4 9 . 3 7
 bench 20cm

1998 3 12 5 5 bench 3
 2 , 4 20 5 18 ,
 3 28 1 6 , , , ,
 , , , , ,
 , , , 10 .
 16 . Simplex
 (Nelder and Mead, 1963) (object function)

minimize $(y_{ij} - ey_{ij})^2, I=1,2,3, j=1,2, \dots, 6, (I= 1,2, \dots, 14)$

, $y_{ij} = j$ (i=1), $y_{ij} = j$ (i=2)
 $(i=3) (g \text{ dw } m-2) ey_{ij} = y_{ij}$.
 $10-1$, $10-2$
 3 7 5 18
 4 , , CO2

Fourth order Runge Kutta method

Simulation 1 step 0.1
 Simplex 10-3,
 Fortran 10-4 . Simplex

10-1. 1998 2

	(/)	1- 2W					
		(g m-2)	(g m-2)	(g m-2)	(g m-2)	(g m-2)	(g m-2)
1	3/28	4.31	1.68	0.51	6.60	3.00	0.74
	4/ 4	11.41	5.19	1.14	12.49	5.86	0.91
	4/11	16.20	8.11	1.21	23.13	13.27	1.31
	4/18	33.67	19.06	1.62	46.46	27.07	1.85
	4/25	60.20	31.35	2.42	76.20	40.27	2.63
	5/ 2	86.73	46.87	2.59	95.35	52.66	2.49
2	3/28	4.61	1.95	0.47	6.40	2.46	0.74
	4/ 4	10.94	5.15	1.01	15.52	5.72	1.08
	4/11	21.01	10.77	1.41	18.38	9.93	1.08
	4/18	35.29	20.20	1.58	43.67	25.25	1.95
	4/25	61.04	30.77	1.82	66.1	36.90	3.13
	5/ 2	81.62	44.48	2.63	97.5	56.77	2.90
3	3/28	3.74	1.58	0.51	4.6	1.82	0.57
	4/ 4	8.18	3.50	0.88	9.8	4.55	0.84
	4/11	17.98	9.26	1.35	14.7	7.95	0.94
	4/18	36.53	21.41	1.55	39.8	24.21	2.09
	4/25	65.86	33.74	2.32	62.0	35.99	2.36
	5/ 2	93.27	49.06	2.42	84.4	46.50	2.79
4	3/28	4.88	1.85	0.54	5.6	2.53	0.71
	4/ 4	10.54	5.02	1.21	11.4	5.62	0.98
	4/11	18.55	9.33	1.52	22.9	12.32	1.21
	4/18	42.22	23.67	2.05	42.7	25.96	1.78
	4/25	61.52	32.76	2.29	72.9	38.72	2.56
	5/ 2	88.99	48.08	3.10	102.8	67.20	3.23

(/)	1- 2W							
	1	2	3	4	1	2	3	4
4/20	.000	1.159	1.159	.000	3.478	14.346	2.319	.580
4/22	4.637	7.680	6.521	6.231	16.810	24.345	10.144	2.319
4/24	13.622	18.984	17.824	17.534	28.113	43.039	18.404	8.985
4/26	35.958	37.049	34.412	35.600	46.015	66.196	39.098	20.974
4/28	48.604	51.174	46.565	44.141	63.095	87.711	55.850	41.996
4/30	60.593	71.210	61.511	60.728	77.055	113.332	70.466	58.091
5/ 2	71.597	91.247	76.456	77.316	94.136	132.711	86.233	67.781
5/ 4	96.043	110.387	93.322	97.782	117.634	157.726	113.142	85.594
5/ 6	136.975	158.141	136.149	143.073	154.587	211.734	171.319	138.465
5/ 8	163.126	176.333	157.753	171.309	175.242	248.687	186.480	148.509
5/10	184.919	193.578	181.440	199.166	201.583	271.616	202.019	162.532
5/12	193.067	208.928	187.504	204.282	209.163	279.954	209.978	171.817
5/14	213.723	225.414	202.096	217.926	233.609	297.578	232.149	196.073
5/18	237.411	264.452	261.221	256.585	261.466	316.149	255.269	235.111

10- 3.

state variable	initial value
shoot dry weight	1.40 (g m ⁻²)
root dry weight	0.28 (g m ⁻²)
fruit dry weight	0.50 (g m ⁻²)
CH ₂ O conc. in shoot	0.10 (g g ⁻¹)
CH ₂ O conc. in root	0.05 (g g ⁻¹)
CH ₂ O conc. in fruit	0.25 (g g ⁻¹)
N conc. in shoot	0.04 (g g ⁻¹)
N conc. in root	0.02 (g g ⁻¹)
N conc. in fruit	0.03 (g g ⁻¹)
Starch conc. in shoot	0.07 (g g ⁻¹)

10-4. Simplex

(parametric value).

ks	0.099956	g (g CH ₂ O)-1 (g N)-1 h-1
kr	0.117864	g (g CH ₂ O)-1 (g N)-1 h-1
kf	0.631684	g (g CH ₂ O)-1 (g N)-1 h-1
Pm	44.030802	g CH ₂ O (m ² ground)-1 h-1
	12.572	(g CH ₂ O g-l)-1
a	0.130156	Demensionless
b	0.525	(g Starch g-l)-1
ϕ	0.437452	g N (g root)-1 h-1
kn	0.00680	mmol
kc	0.048524	g CH ₂ O g-1
ϕr	14.206585	g CH ₂ O (g CH ₂ O g-l)-2 h-1
ϕf	11.762246	g CH ₂ O (g CH ₂ O g-l)-2 h-1
C _{stmax}	0.30	g CH ₂ O g-1
C _{nrmax}	0.10	g CH ₂ O g-1
C _{frmax}	0.40	g CH ₂ O g-1
ϕd	7.0	g CH ₂ O (g CH ₂ O g-l · g Starch g-l)-1 h-1
ϕn	38.999418	(g CH ₂ O g-l · g Starch g-l)-1 h-1
ns	9.447467	g N (g N g-l · g N g-l)-1 h-1
nsf	0.39836	g N (g N g-l · g N g-l)-1 h-1
N _{sna}	0.15	g N g-1
N _{mex}	0.15	g N g-1
S _{max}	0.35	g Starch g-1

3

1. (validation of model)

Fig. 10-4 , Fig. 10-5 , Fig. 10-6 , Fig. 10-7 .
가 45c

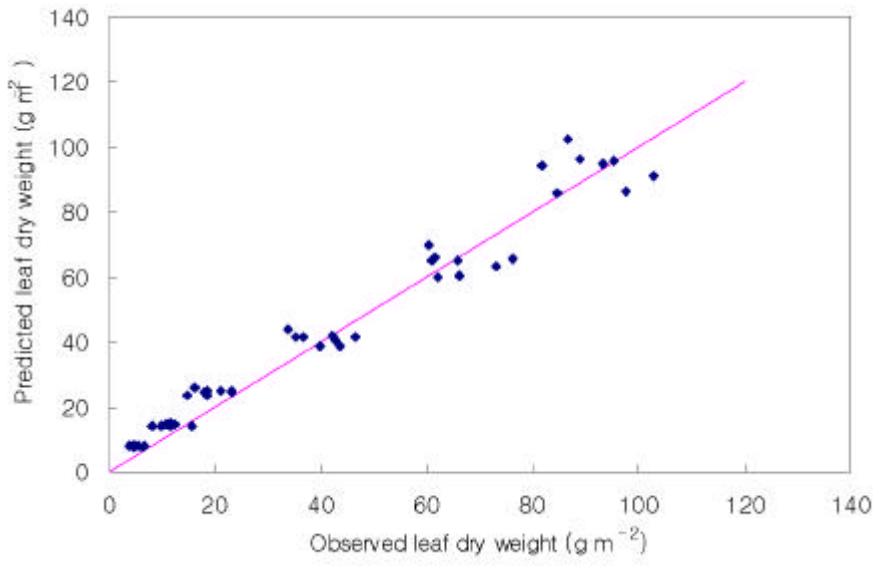


Fig. 10-4. Comparison between observed and predicted values of leaf dry weight by the model.

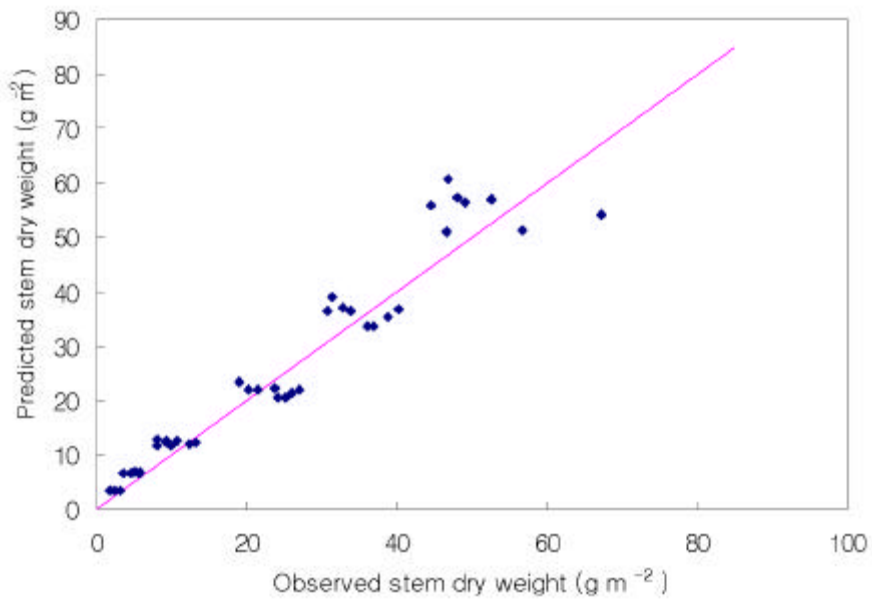


Fig. 10-5. Comparison between observed and predicted values of stem dry weight by the model.

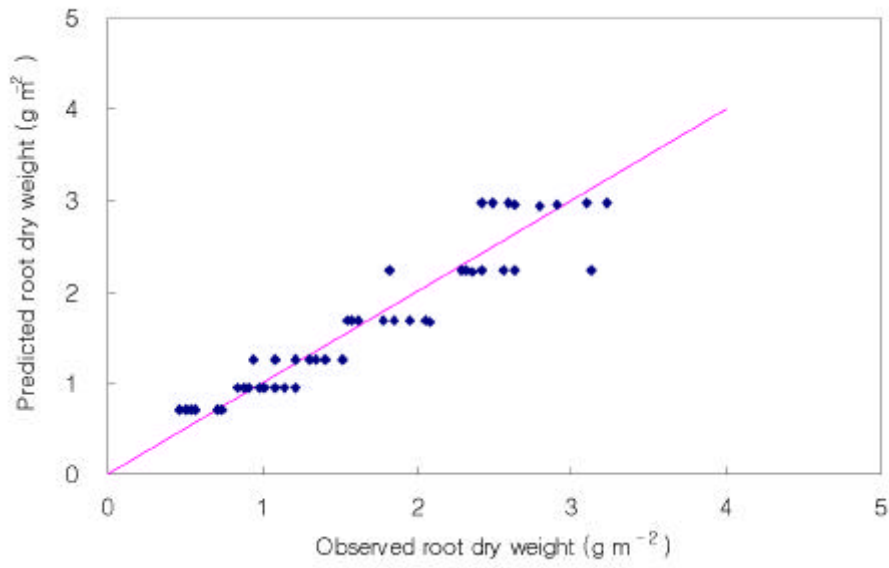


Fig. 10-6. Comparison between observed and predicted values of root dry weight by the model.

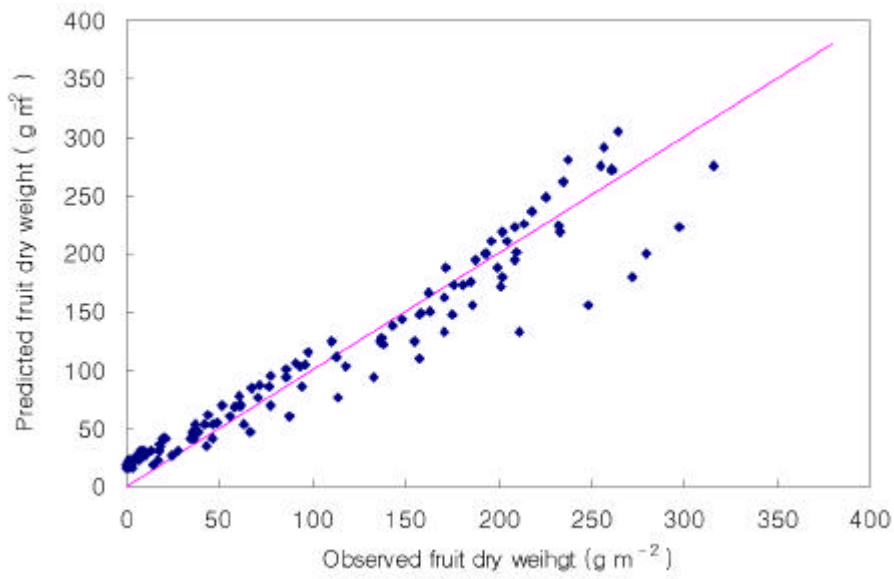


Fig. 10-7. Comparison between observed and predicted values of fruit dry weight by the model.

sink demand

$$T_{pg} = (C_{smax} - C_s) P_g,$$

$$T_{pg}/P_g$$

10-5

가

$$0.15878 \quad P_m=44.0308 \quad (10^{-3}) \quad 6.9912 \quad 1) \quad 7.4765$$

sink/source

10-5.

T_{pr}/P_g

	$(\mu \text{ mol m}^{-2} \text{ s}^{-1})$	T_{pr}/P_g
7:00	64.10	.37384
8:00	110.00	.23951
9:00	215.50	.16429
10:00	362.60	.12865
11:00	585.60	.07037
12:00	243.90	.06120
13:00	595.20	.06056
14:00	704.40	.06249
15:00	603.60	.07037
16:00	411.50	.10729
17:00	285.50	.13510
18:00	140.90	.23669

CO2

N

1

SLA LAI

RGR

가

. Marcelis (1994)

가

. Horie (1979)

가가

620 625

540 550

(NL)

$$NL = -4.1782 + 0.0216 AC \quad (R^2=0.9729, df=54)$$

, 5

6

$$NL = -4.265 + 0.0282 AC \quad (R^2= 0.9897, df=40)$$

(AC)

가

30

1

35

900

가 900

30

2.

가 $100 \mu\text{mol m}^{-2} \text{s}^{-1}$
 $1500 \mu\text{mol m}^{-2} \text{s}^{-1}$, 15
 12 1 32 , CO 100ppm
 100ppm 1500ppm , N 0.4mmol
 0.4mmol 6mmol
 N
 N Michaelis- Menten

$$V = V_{\text{max}} N / (k_n + N),$$

$$k_n \quad V \text{가 } V_{\text{max}} \quad 1/2 \quad N$$

$$k_n = 0.0068 \text{ mmol} \quad N$$

$$0.4\text{mmol} \quad N \quad N \quad \text{가} \quad N$$

$$(Rad) \quad (FDW)$$

$$FDW = 293.5428 + 0.2603 \text{ Rad} - 0.000113 (\text{Rad})^2,$$

$$2 \quad 1150 \mu\text{mol m}^{-2} \text{s}^{-1}$$

(Temp)

$$FDW = -108.3346 + 33.6904 \text{ Temp} - 0.43175 (\text{Temp})^2,$$

$$2 \qquad \qquad \qquad 39.0$$

CO2

$$FDW = 348.38 + 0.1366\text{CO}_2 - 0.00006 (\text{CO}_2)^2,$$

$$2 \qquad \qquad \qquad \text{CO}_2 \text{ 1138.3 ppm}$$

CO2

$$FDW = -218.5275 + 0.2170 \text{ Rad} + 29.7863 \text{ Temp} + 0.1271 \text{ CO}_2 \\ + 0.0032 (\text{Rad})(\text{Temp}) - 0.000034 (\text{Rad})(\text{CO}_2) + 0.00167 (\text{Temp})(\text{CO}_2) \\ - 0.000113 (\text{Rad})^2 - 0.4316 (\text{Temp})^2 - 0.00006 (\text{CO}_2)^2,$$

$$1365.8 \mu\text{mol m}^{-2} \text{ s}^{-1},$$

$$42.0 \qquad \qquad \text{CO}_2 \qquad 1256.7\text{ppm}$$

$$546.9 \text{ g m}^{-2} \qquad \qquad \qquad 546.9/0.0439 = 12.46 \text{ kg m}^{-2}$$

39

$$\text{가} \qquad \qquad \qquad 42$$

$$GPR = 19.071 (1 - 1.3704 \exp(-0.0571 \text{ temp})), (\mu\text{mol CO}_2 \text{ m}^{-2} \text{ s}^{-1})$$

$$\text{Resp} = 0.009862 - 0.000039 T + 0.000045 T^2, (\mu\text{mol CO}_2 \text{ g}^{-1} \text{ s}^{-1})$$

$$\text{LA} = 432.23 \text{ LDW} - 4.241 \text{ LDW}^2,$$

10-8

10-8

45

가

가

Shishido (1987)

44

가

가

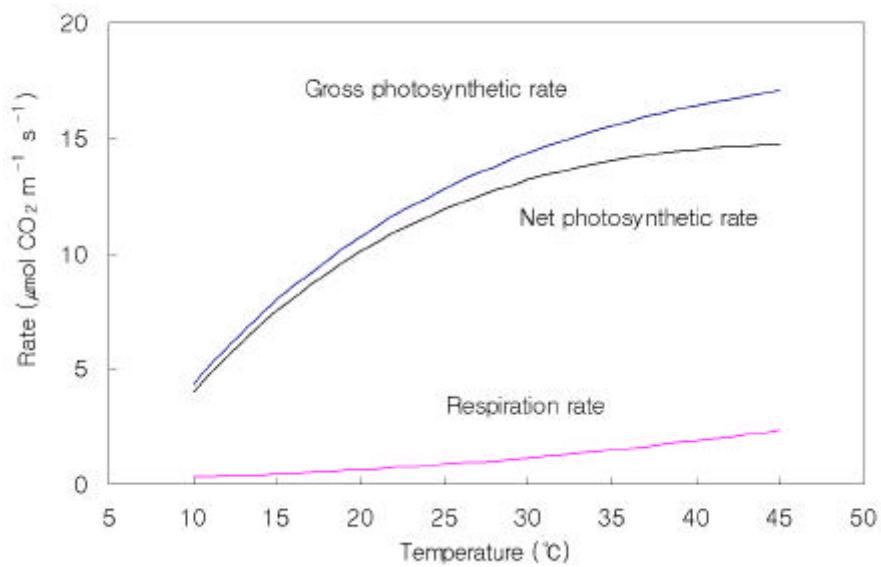


Fig.10-8. Variations in gross and net photosynthetic rate and respiration rate.

가
가

73 250g m-2

$$250 = - 218.5275 + 0.2170 \text{ Rad} + 29.7863 \text{ Temp} + 0.1271 \text{ CO}_2$$

$$+ 0.0032 (\text{Rad})(\text{Temp}) - 0.000034 (\text{Rad})(\text{CO}_2) + 0.00167 (\text{Temp})(\text{CO}_2)$$

$$- 0.000113 (\text{Rad})^2 - 0.4316 (\text{Temp})^2 - 0.00006 (\text{CO}_2)^2,$$

$$468.5275 = 0.2170 \text{ Rad} + 29.7863 \text{ Temp} + 0.1271 \text{ CO}_2$$

$$+ 0.0032 (\text{Rad})(\text{Temp}) - 0.000034 (\text{Rad})(\text{CO}_2) + 0.00167 (\text{Temp})(\text{CO}_2)$$

$$- 0.000113 (\text{Rad})^2 - 0.4316 (\text{Temp})^2 - 0.00006 (\text{CO}_2)^2,$$

가 , CO2

11 .

1 .

가 , , , 가

가

11 3

가 가

가

가

, , ,

,

3

가

가

가

가

가

가

, , 가 , 가
()

(1-2W) ()

2 .

1.

15m × 25m
 (1-2W) 15m × 24m ()
 1 가
 2 2 ,
 3 1 , 2 , 3
 1.8m
 , 1m CO2
 , 10cm 20cm .

3m

, , , ,

20cm, 40cm 70cm

11-1 11-2

, 11-3

11-1

, 11-2

11-4 (, , , , ,)

3 m . 11-5(a)

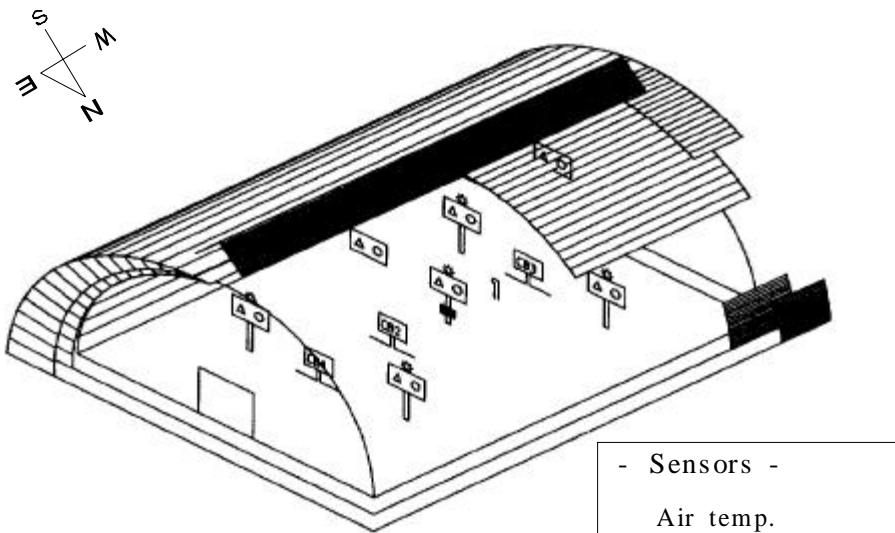
, , , 11-5(b)



11-1.

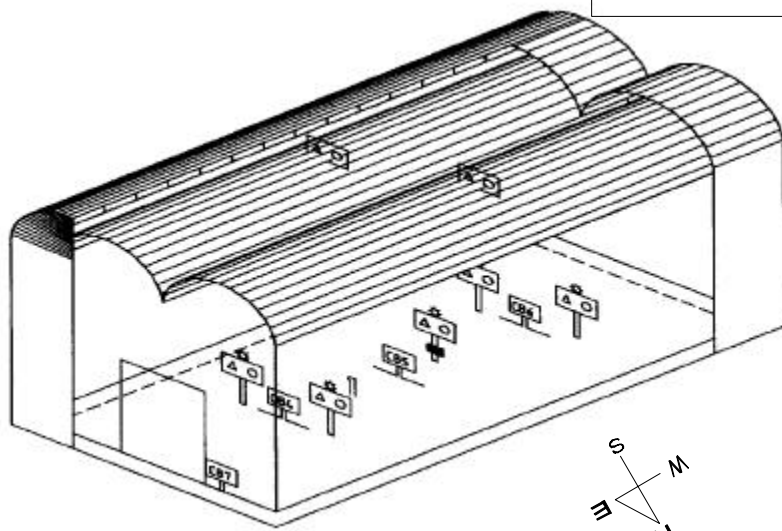


11-2.



(a)

- Sensors -
- Air temp.
 - Rel. Humidity
 - ☀ Radiation
 - CO2 Concentration
 - ∥ Air velocity
 - Soil temp.
 - CB: Control box



(b)

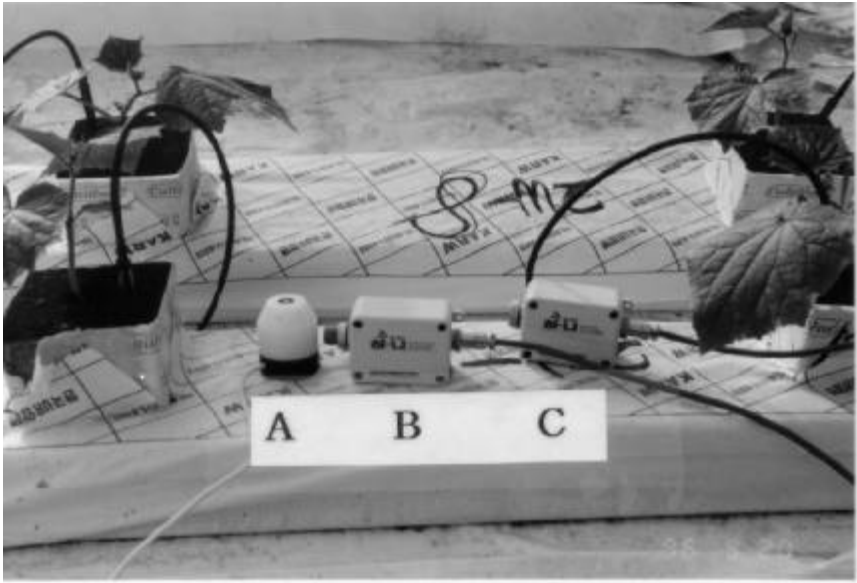
11-3.

168- 1.

Factor	Sensor type	Range	No. of sensors in each greenhouse
Soil temp.	RTD	- 10 +50	4
Air temp.	Semiconductor type	- 10 +50(60)	7
Rel. Humidity	Polymer electrolyte	0 100 %	7
Radiation	Photocell	0 3000 μ mol/m ² /s	5
CO ₂ concentration	Nondisperse infrared	0 2000 ppm	1
Wind velocity	Pt. RTD	0 5 m/s	1



11- 4.



(a) (A), (B), (C)



(b)

11-5.

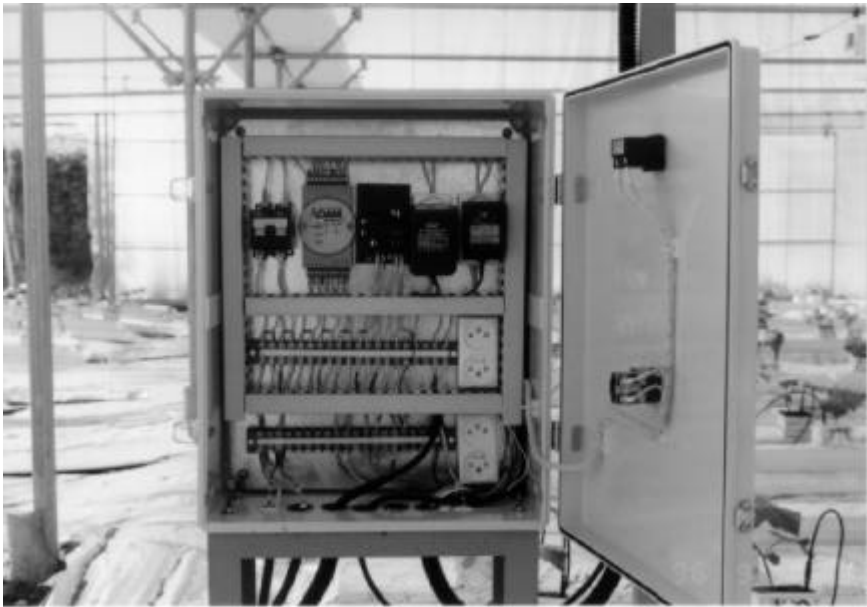
11- 69.

Factor	Sensor type	Range
Soil temp.	RTD	- 10 +50
Air temp.	Thermistor	- 10 +50(60)
Rel. Humidity	Capacitance type	0 100 %
Radiation	Silicon Photovoltaic Photocell	0 3000 μ mol/m ² /s
Wind direction	Variable resistance	0 360 °
Air velocity	Switch contact	0 45 m/s
Rainfall	Switch contact	-

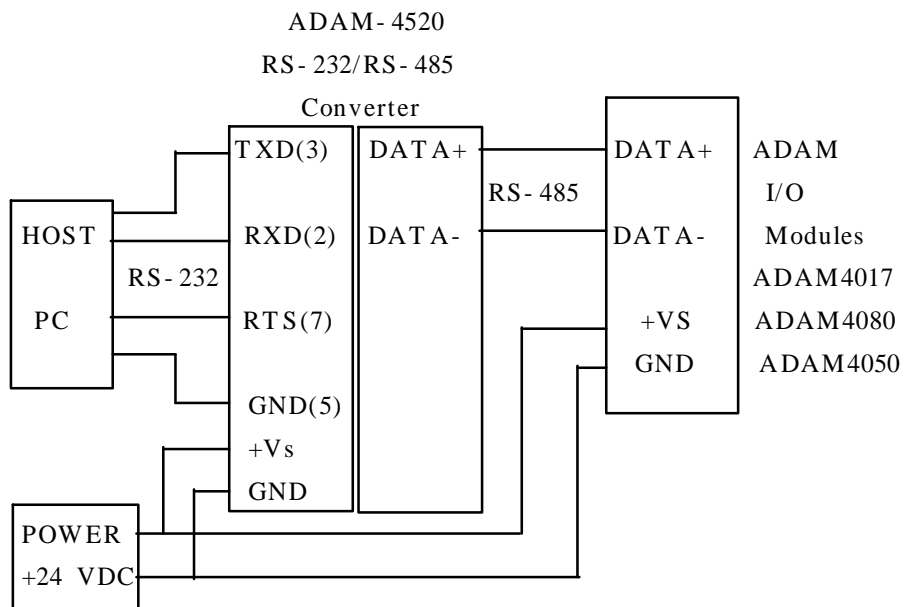
2.

64 62 / (A/D converter), (Pulse counter), (Data acquisition system) 8 16 bit A/D (ADAM 4017, Advantech, Taiwan) 11 , 2 32 bit 1 (ADAM 4080D, Advantech, Taiwan), 7 8 digital I/O (ADAM 4050, Advantech, Taiwan) 4 multi-drop RS- 485 , 11- 6 8 16 bit A/D (CPC- 5860M,) RS- 485/RS- 232 , 11- 7 , RS- 485/RS- 232 , 62 A/D 1 10 , 2

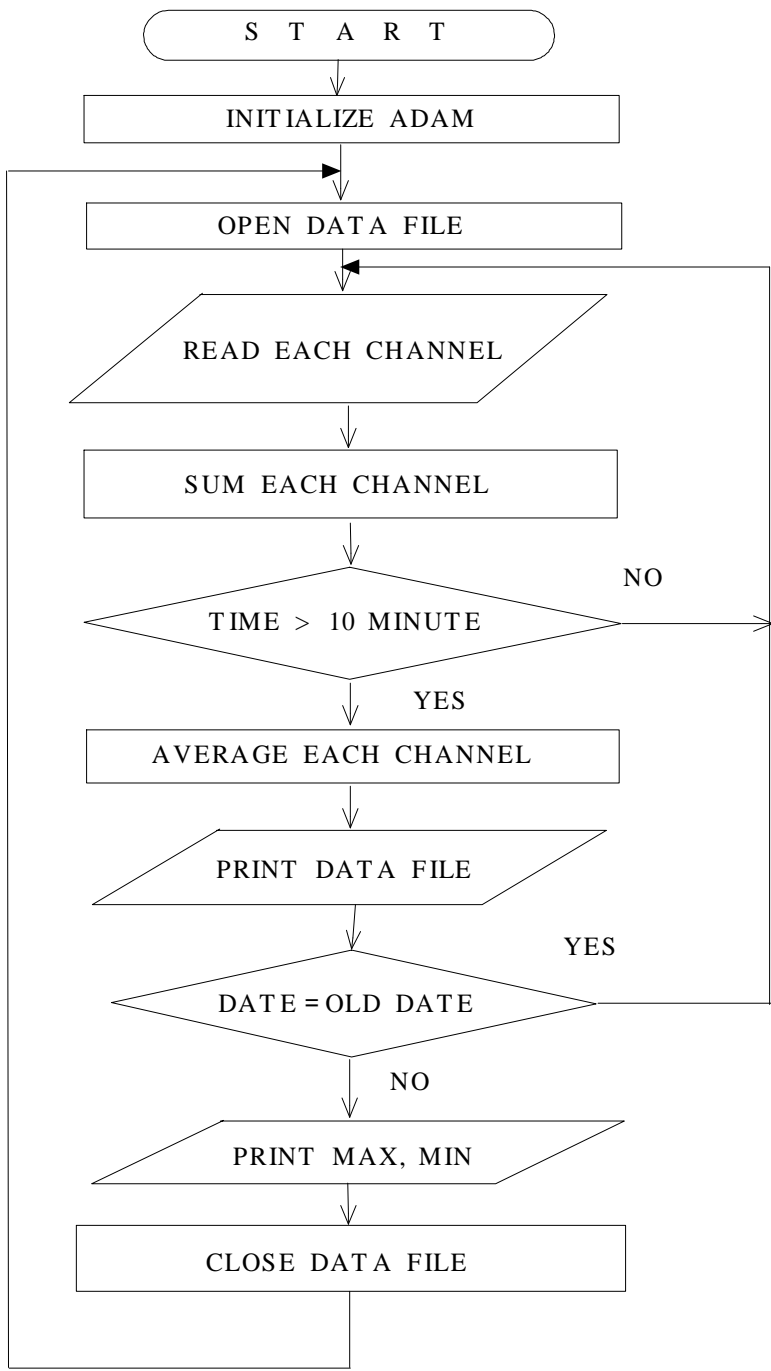
10
ASCII
5 10
Microsoft Visual BASIC 5.0
11-8



11-6. Control Box



11-7.



11- 8.

3

1.

가.

2 (, ())

80 가

(PAR-80, Decagon Devices Inc, USA) 9 ,

12 15

11-3

1 m (11-9)

5 cm ,

40 cm 1 cm 80 가

1 , 2 , 3 , 1 (net), 2

1997 9

19 9 30

11- 70.

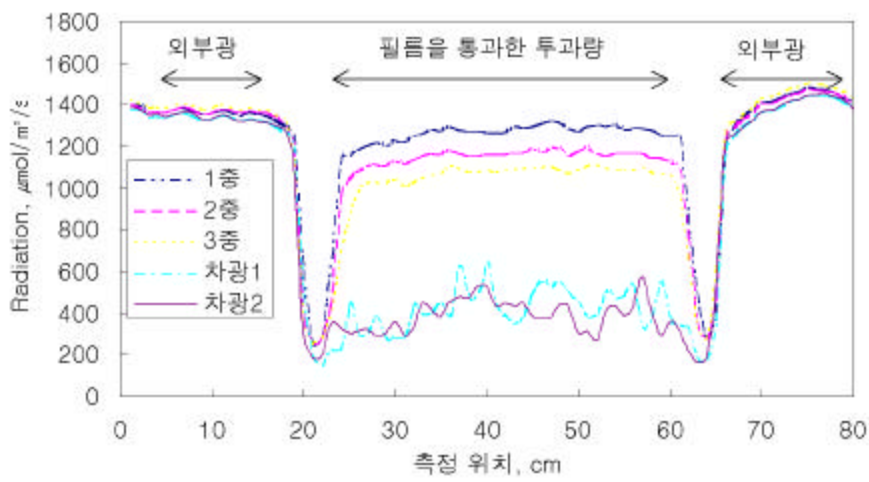
		()	
	(mm)		(mm)
	0.06		0.06
	0.06	E.V.A	0.06
	0.06		0.06
E.V.A	0.06		0.06
	0.06		0.07
	0.06		0.1
	0.06	가	0.15
P.E	0.06	-	-
	0.04	-	-



11- 9.

11- 10

1 가 , 2 , 3



11- 10. ()

11- 4 9 1 0.765 0.898
 가 가 7 15%
 . 3 0.51 0.736 . 1 2
 0.219 0.312

12 11-5 . 1 0.86
 1 0.92 9 .
 9 가 . 2 3
 0.77 0.847, 0.632 0.796 . 1
 0.26 0.362 , 2 0.219 0.29 .
 15 11-6 , 9
 . 1 , 2 , 3 0.657 0.884, 0.4
 9 0.884, 0.425 0.703 . 1
 0.215 0.344 , 2 0.19 0.325 .

11-4. (9)

Type of film	thickness (mm)	Single	Double	Triple	Single+screen	Double+screen
E. V. A	0.06	0.786	0.610	0.510	0.238	0.219
	0.06	0.765	0.636	0.520	0.224	0.236
	0.06	0.860	0.721	0.592	0.290	0.247
	0.06	0.853	0.708	0.591	0.273	0.237
	0.06	0.843	0.673	0.570	0.245	0.227
	0.06	0.868	0.751	0.659	0.261	0.270
	0.06	0.772	0.631	0.539	0.283	0.237
	0.06	0.898	0.808	0.736	0.252	0.295
P. E	0.04	0.846	0.732	0.645	0.258	0.263
	0.06	0.885	0.795	0.710	0.312	0.243
	0.06	0.879	0.760	0.679	0.312	0.272
	0.06	0.888	0.811	0.724	0.243	0.290
	0.06	0.875	0.762	0.662	0.252	0.266
	0.07	0.876	0.764	0.675	0.267	0.258
	0.10	0.858	0.726	0.614	0.273	0.264
	가	0.15	0.880	0.779	0.669	0.286

11- 5.

(12)

Type of film	thickness (mm)	Single	Double	Triple	Single+screen	Double+screen
	0.06	0.861	0.786	0.632	0.350	0.292
	0.06	0.890	0.784	0.674	0.315	0.290
	0.06	0.878	0.806	0.688	0.362	0.315
E. V. A	0.06	0.898	0.772	0.660	0.307	0.319
	0.06	0.880	0.770	0.653	0.320	0.30
	0.06	0.899	0.817	0.743	0.314	0.308
	0.06	0.868	0.772	0.679	0.309	0.266
P. E	0.06	0.900	0.821	0.747	0.289	0.310
	0.04	0.900	0.847	0.796	0.264	0.320
	0.06	0.898	0.819	0.747	0.326	0.314
	0.06	0.905	0.832	0.764	0.299	0.273
E.V.A	0.06	0.920	0.843	0.783	0.321	0.295
	0.06	0.910	0.818	0.740	0.328	0.290
	0.07	0.902	0.816	0.738	0.320	0.293
	0.10	0.887	0.792	0.694	0.311	0.290
가	0.15	0.880	0.794	0.308	0.308	0.293

11- 6.

(15)

Type of film	thickness (mm)	Single	Double	Triple	Single+screen	Double+screen
	0.06	0.795	0.660	0.530	0.238	0.219
	0.06	0.714	0.564	0.486	0.230	0.198
	0.06	0.710	0.564	0.476	0.220	0.199
E. V. A	0.06	0.700	0.530	0.480	0.221	0.204
	0.06	0.657	0.490	0.425	0.215	0.190
	0.06	0.883	0.753	0.640	0.263	0.310
	0.06	0.776	0.655	0.558	0.266	0.240
P. E	0.06	0.860	0.750	0.649	0.244	0.325
	0.04	0.806	0.695	0.597	0.250	0.254
	0.06	0.840	0.742	0.620	0.266	0.264
	0.06	0.860	0.773	0.673	0.320	0.310
E.V.A	0.06	0.884	0.844	0.703	0.329	0.325
	0.06	0.846	0.718	0.658	0.344	0.300
	0.07	0.831	0.700	0.635	0.315	0.310
	0.1	0.764	0.707	0.607	0.337	0.305
가	0.15	0.850	0.725	0.635	0.309	0.300

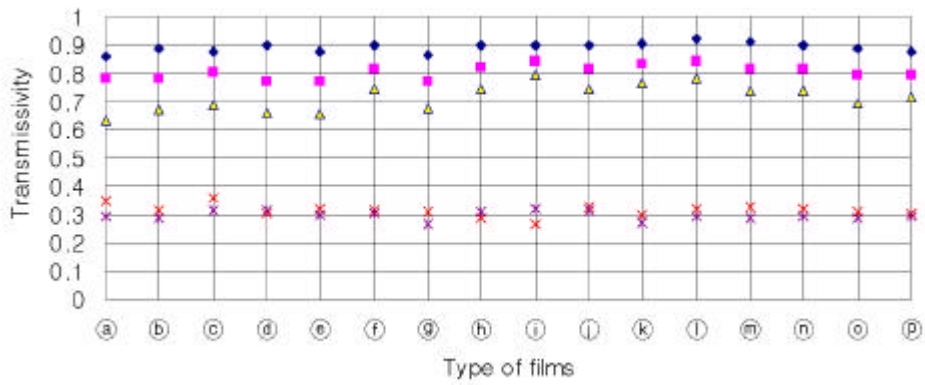
11-11 12

1, 2, 3

0.861 0.92, 0.77 0.847, 0.632 0.796

1 2

0.219 0.362



((single, double, triple, x single+screen, *double+screen)

11-11.

(12)

11-12 1

9, 12, 15

12

가

,

9

15

. 12

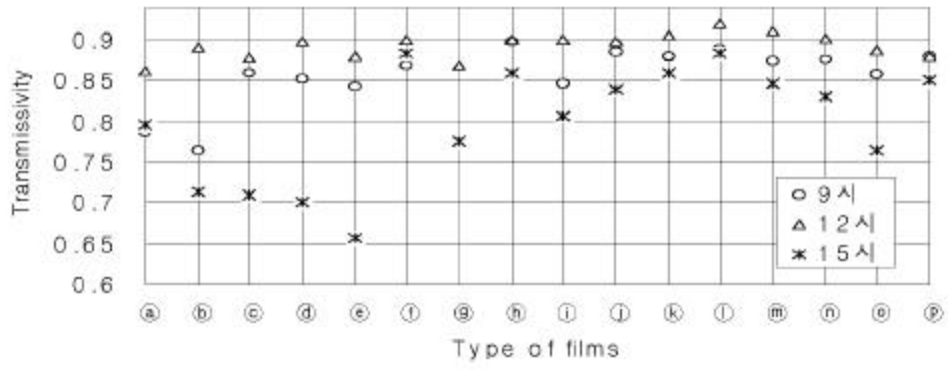
가

가 9, 15

9, 12, 15

0.765

0.898, 0.861 0.92, 0.657 0.884



11- 12. 가 1

2.

가.

가 , 가 가

80 가 (PAR- 80, Decagon Devices Inc, USA) . 80

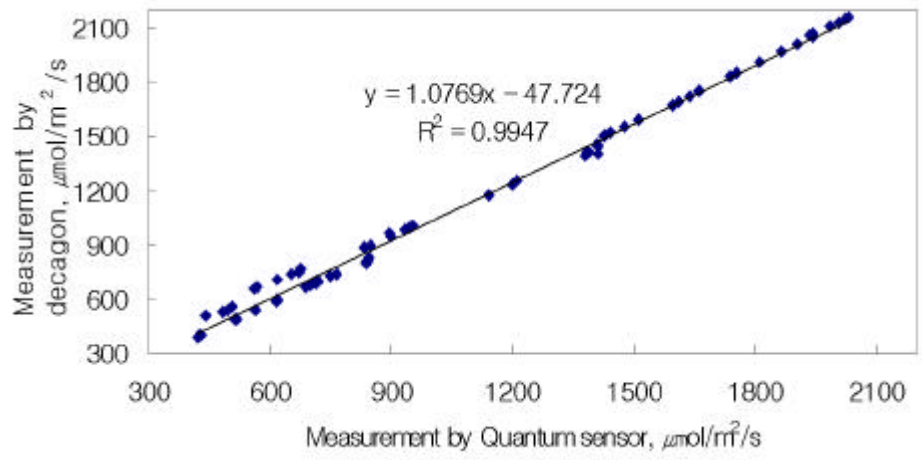
Decagon

LI-COR Quantum (11-13)
 . Decagon 80
 , 11-14
 R2 0.9947 .
 11-15 Decagon
 80 cm
 LI-COR



11-13. Decagon

Quantum

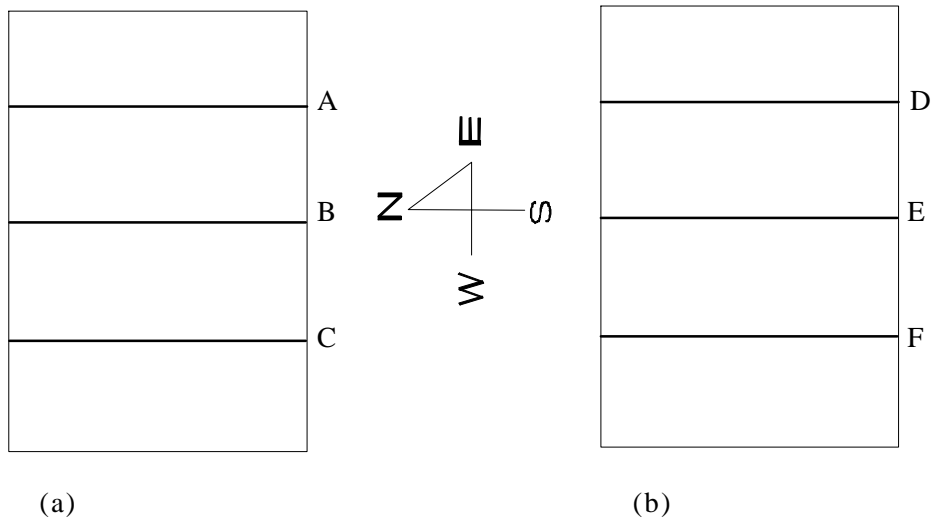


11- 14. Decagon PAR- 80 1



11- 15.

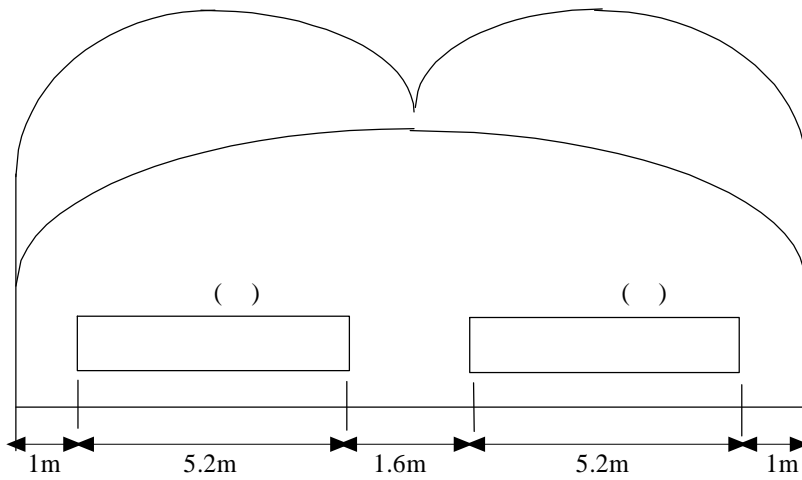
2
 9, 12, 15
 11-16
 - A, B, C, -D, E, F)
 1.2 m
 1997 5
 23 6 15



11-16.

11-17
 14m
 14m
 0.489, 0.442, 0.351
 5
 2 0.415, 1, 2
 , 3 가 가

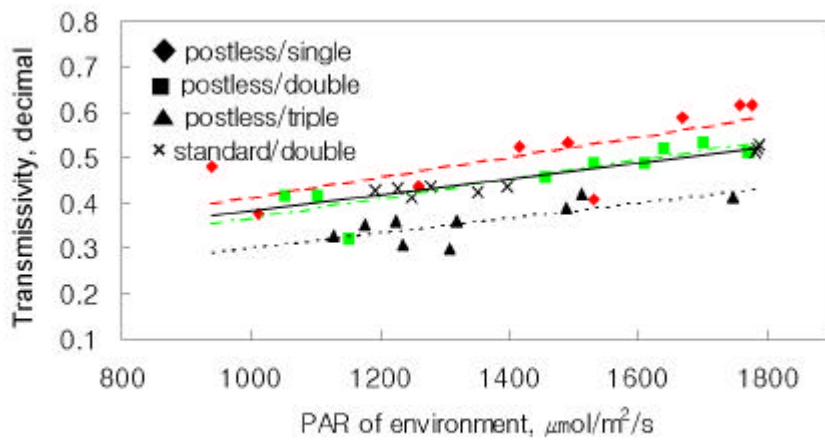
, 2
 0.461, 0.458 가 0.175
 1, 2, 3
 0.525, 0.441, 0.341 , 0.489, 0.442, 0.351 ,
 (11-7). 11-18



11-17.

11-7.

	(14m)	(5.2m)	(0.6m)	(5.2m)
- 2	0.415(100)	0.461	0.175	0.458
- 1	0.489(118)	0.525	0.437	0.489
- 2	0.442(107)	0.441	0.374	0.442
- 3	0.351(85)	0.341	0.368	0.351



11- 18.

11- 19

PAR

9

3

PAR

0.42

1

, 2

, 3

0.49, 0.44

0.35

1

PAR

18%

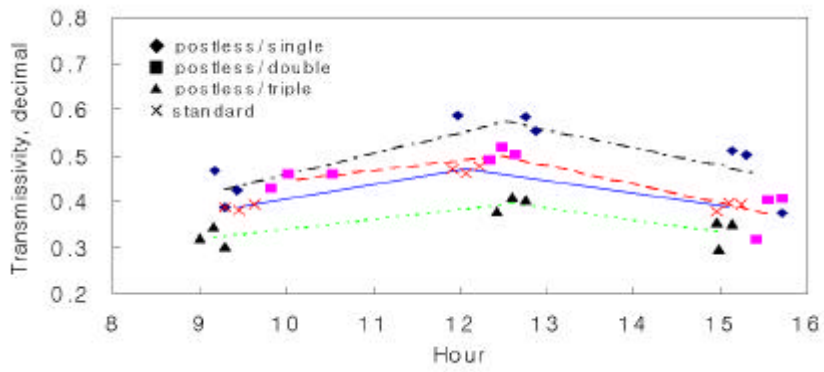
, 2

6.5%

3

PAR

15%



11-19.

3. CO2 가

가.

CO2 가

99.5% CO2가 20 kg

1/3

CO2 가

CO2

가 2000ppm

CO2

CO2 가 가

5 10

11-20

CO2

5

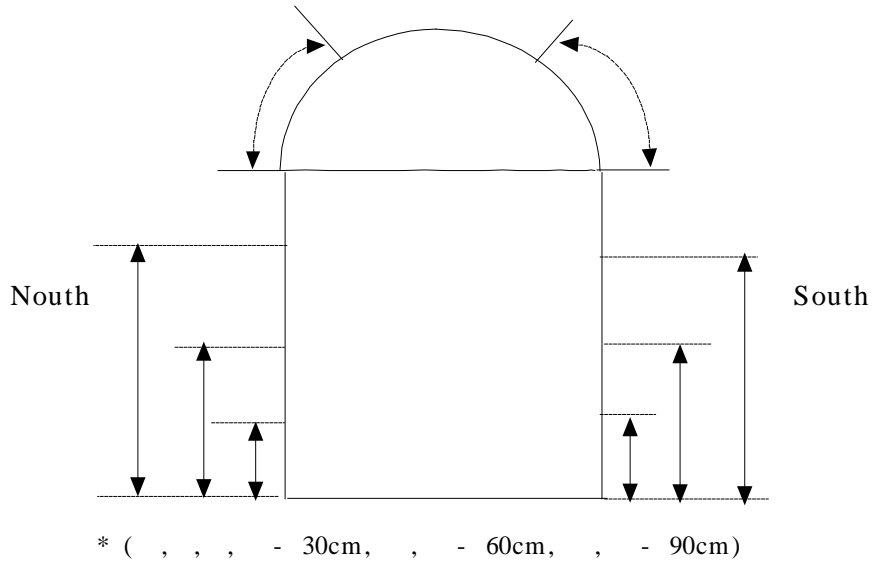
30cm, 60cm, 90cm

30cm, 60cm, 90cm

30cm, 60cm, 90cm

30cm, 60cm, 90cm

19가



11- 20.

1) CO2 가

11-8

가
가
가
가
1

11-8.

Experimental condition		Win (m/s)	Wout (m/s)	t ()	Cg(0) ppm	Cg(t) ppm	t (sec)	S (hr-1)	
stan- dard	with plant	day	0.10	1.61	19.29	1781	844	3840	0.97
		night	0.08	1.20	1.81	729	608	2585	0.50
	without plant	day	0.10	1.73	19.12	1896	922	4305	0.81
		night	0.10	1.18	4.08	1120	790	3800	0.51
post- less	with plant	day	0.10	0.15	19.82	1519	1205	1530	0.72
		night	0.10	0.70	3.75	2428	2104	4020	0.15
	without plant	day	0.10	1.14	21.54	2267	1184	3880	0.76
		night	0.10	1.09	5.89	1730	1121	4075	0.50

Win : wind velocity inside of the greenhouse Wout : wind velocity outside of the greenhouse

t : outside temperature - inside temperature Cg(0) : initial CO2 concentration

Cg(t) : CO2 concentration at time t S : ventilation rate.

2) CO2 가

(
11-20)
CO2 , CO2 , (11-9, 11-10,

11- 11, 11- 12).

11- 9.

Open method	t ()	Wcut (m/s)	Cg(0) (ppm)	Cg(t) (ppm)	t (sec)	S (hr-1)		
						measured	calculated	
top- vent(a,b)	16.85	1.14	1420	503	760	8.73	10.16	
top- vent closed	1	18.07	1.64	2134	579	660	10.80	11.88
	2	16.31	1.941	1312	506	270	22.90	25.11
	3	16.68	2.47	2057	508	300	27.28	26.37
	4	16.08	1.39	1424	500	430	15.60	13.78
	5	16.29	1.98	2140	501	490	17.33	15.51
	6	19.12	1.7	1184	494	110	54.11	56.53
	1,4	16.91	0.91	1544	500	210	33.69	32.66
	2,5	4.55	0.81	2785	497	355	27.27	31.00
top- vent opened	3,6	4.52	0.48	1525	501	240	29.19	30.51
	1	4.94	1.49	1552	496	385	18.67	17.14
	2	5.64	1.61	1774	503	485	15.74	19.74
	3	5.00	1.28	2190	502	435	19.73	34.55
	4	8.24	1.54	1867	502	420	18.80	27.82
	5	7.70	2.09	2182	499	295	29.19	22.62
	6	6.31	1.75	2835	509	500	18.98	35.74
	1,4	5.00	1.31	2162	500	320	26.73	27.25
	2,5	4.12	1.86	1841	497	210	37.73	33.10
3,6	3.82	1.51	1427	503	185	35.95	24.25	

t : outside temperature - inside temperature Wcut : wind velocity outside of the greenhouse

Cg(0) : initial CO2 concentration

Cg(t) : CO2 concentration at time t

S : ventilation rate.

11- 10.

Open method	t ()	Wcut (m/s)	Cg(0) (ppm)	Cg(t) (ppm)	t (sec)	S(hr-1)		
						measured	calculated	
top-vent(a,b)	7.00	1.63	2514	504	1035	8.81	5.17	
top-vent closed	1	16.64	1.72	1320	503	930	6.75	6.04
	2	18.44	1.83	1898	546	795	8.98	10.91
	3	18.75	2.07	1837	521	580	12.8	12.87
	4	19.22	1.86	992	523	765	5.81	6.28
	5	19.57	1.86	1843	523	635	11.69	10.55
	6	11.17	1.76	1803	500	710	10.95	11.65
	1,4	15.80	1.46	1797	554	1630	4.15	16.49
	2,5	15.55	2.16	1634	534	800	8.34	8.22
	3,6	16.23	1.62	1529	605	375	14.14	22.32
top-vent opened	1	18.94	1.61	1500	515	530	12.54	12.79
	2	16.88	1.52	1786	527	490	14.71	25.33
	3	16.71	1.54	1665	518	495	14.26	21.35
	4	17.35	1.45	1765	565	1000	6.51	7.39
	5	16.13	1.61	1880	547	1235	5.72	9.56
	6	16.07	1.41	1555	532	630	10.29	15.42
	1,4	13.35	1.63	1567	516	500	13.66	15.28
	2,5	12.75	1.53	1709	501	485	15.52	17.20
	3,6	13.66	1.45	1838	509	490	15.64	19.22

t : outside temperature - inside temperature Wcut : wind velocity outside of the greenhouse

Cg(0) : initial CO2 concentration Cg(t) : CO2 concentration at time t

S : ventilation rate.

11- 11.

Open method	t ()	Wcut (m/s)	Cg(0) (ppm)	Cg(t) (ppm)	t (sec)	S(hr-l)		
						measured	calculated	
top- vent(a,b)	11.18	1.07	2001	520	1654	5.34	6.78	
top-vent closed	1	17.66	2.23	1763	505	1105	6.84	5.71
	2	21.20	1.96	1787	499	720	10.77	12.70
	3	19.60	2.19	1683	503	655	11.31	13.64
	4	18.60	1.72	2119	500	845	10.01	7.33
	5	16.71	1.43	1822	502	385	20.16	13.79
	6	7.25	0.95	2049	503	700	11.79	9.41
	1,4	8.10	0.58	1983	501	1075	7.60	8.22
	2,5	8.82	0.85	1963	503	565	14.28	14.07
	3,6	9.01	0.52	2687	503	465	20.21	20.97
top-vent opened	1	10.40	1.35	1824	502	350	22.18	24.19
	2	12.80	1.09	1799	496	240	32.66	40.28
	3	13.74	1.31	1723	503	260	28.89	37.43
	4	11.88	1.59	1960	499	435	18.72	21.90
	5	12.28	1.26	1895	405	370	29.48	40.80
	6	10.32	1.46	1904	506	380	20.74	34.44
	1,4	12.67	1.30	1738	500	235	32.31	20.21
	2,5	12.73	1.09	1792	493	240	32.90	33.62
	3,6	12.86	1.58	1846	502	180	43.50	54.20

t : outside temperature - inside temperature Wcut : wind velocity outside of the greenhouse

Cg(0) : initial CO2 concentration Cg(t) : CO2 concentration at time t

S : ventilation rate.

11- 12.

Open method	t ()	Wcut (m/s)	Cg(0) (ppm)	Cg(t) (ppm)	t (sec)	S (hr-1)		
						measured	calculated	
top- vent(a,b)	16.10	1.21	2464	501	1385	6.56	7.78	
top-vent closed	1	17.86	1.80	1623	616	1805	3.01	5.37
	2	8.85	0.67	1945	567	1430	4.82	11.99
	3	15.26	1.23	1795	503	800	9.61	14.48
	4	18.60	1.76	1860	501	2090	3.77	6.39
	5	18.50	1.69	1686	533	1015	6.73	11.89
	6	17.37	1.91	2272	502	860	10.14	9.21
	1,4	18.43	1.48	2156	499	1630	5.25	4.31
	2,5	10.60	1.20	2380	503	775	11.49	13.92
	3,6	14.86	1.43	1788	501	355	21.71	13.61
top-vent opened	1	19.23	1.00	1754	502	280	27.15	13.99
	2	19.28	1.32	1692	498	180	41.86	20.63
	3	19.97	0.94	1698	508	180	40.82	14.79
	4	17.47	1.16	1779	501	400	19.21	8.77
	5	16.15	1.47	1820	501	280	27.86	9.26
	6	15.67	1.56	1818	505	235	32.80	10.94
	1,4	13.94	1.33	2058	503	410	20.23	15.24
	2,5	11.95	0.86	1822	505	230	33.59	16.84
	3,6	12.01	1.25	1928	499	295	27.38	23.87

t : outside temperature - inside temperature Wcut : wind velocity outside of the greenhouse

Cg(0) : initial CO2 concentration Cg(t) : CO2 concentration at time t

S : ventilation rate.

3)

$$S = a + b * Area + c * Wind + d * Temp$$

, Area

, Wind

(m/s) , Temp()

(11- 13,

11- 14, 11- 15, 11- 16).

11- 13.

Open method		a	b	c	d	R- square
Top-vent closed	South	82.680	3.252	- 6.959	- 3.701	0.839
	North	- 87.643	10.769	28.797	1.217	0.992
	or	- 26.330	9.175	- 17.813	2.689	0.632
	Both side	20.459	0.982	- 5.929	0.645	0.334
	, or	- 28.138	4.784	- 6.078	2.562	0.415
Top-vent opened	South	14.885	2.804	- 11.660	0.238	0.678
	North	- 15.161	6.519	- 9.263	0.908	0.787
	or	- 4.562	3.804	- 0.963	0.242	0.604
	Both side	21.639	- 0.227	9.104	- 1.176	0.845
	, or	18.963	0.763	2.657	- 0.5907	0.316
All		12.224	1.659	- 0.995	0.267	0.238

Opening method : South- 30cm, 60cm, 90cm : North- 30cm, 60cm, 90cm
: Both side- 30cm, 60cm, 90cm All : Everything opening method

11- 14.

Open method		a	b	c	d	R- square
Top-vent closed	South	- 29.033	1.525	7.670	0.816	0.868
	North	- 87.643	10.769	28.797	1.217	0.992
	or	6.061	1.526	- 5.523	0.500	0.402
	Both side	22.272	1.247	- 12.712	- 1.144	0.903
	, or	6.417	1.035	- 3.596	0.382	0.568
Top-vent opened	South	- 5.462	4.078	- 9.324	- 9.324	0.860
	North	0.883	3.257	- 11.686	1.045	0.744
	or	- 4.988	3.322	- 9.302	1.287	0.826
	Both side	- 32.440	3.802	- 9.856	2.978	0.900
	, or	- 4.988	3.322	- 9.302	1.287	0.826
All		- 9.217	3.118	- 5.511	1.117	0.714

Opening method : South- 30cm, 60cm, 90cm : North- 30cm, 60cm, 90cm
: Both side- 30cm, 60cm, 90cm All : Everything opening method

11- 15.

Open method		a	b	c	d	R- square
Top-vent closed	South	- 3.082	1.917	2.122	0.227	0.956
	North	14.529	1.724	- 8.235	0.317	0.922
	or	6.317	2.279	- 2.009	0.010	0.782
	Both side	- 0.294	- 1.320	- 19.159	3.658	0.840
	, or	9.466	1.372	- 3.813	0.107	0.555
Top-vent opened	South	16.833	0.557	- 12.274	0.913	0.724
	North	- 11.924	2.252	6.843	- 0.191	0.818
	or	- 58.572	0.975	10.402	2.991	0.778
	Both side	- 19.426	0.957	8.298	1.216	0.964
	, or	- 16.222	2.416	- 2.039	1.005	0.679
All		5.877	1.395	- 4.457	0.330	0.581

Opening method : South- 30cm, 60cm, 90cm : North- 30cm, 60cm, 90cm
: Both side- 30cm, 60cm, 90cm All : Everything opening method

11- 16.

Open method		a	b	c	d	R- square
Top-vent closed	South	- 3.082	1.917	2.122	0.227	0.956
	North	17.825	1.280	1.951	- 0.963	0.959
	or	- 1.730	2.150	0.130	0.146	0.892
	Both side	- 9.226	3.447	5.076	- 0.169	0.989
	, or	- 3.869	2.834	1.423	0.031	0.938
Top-vent opened	South	- 121.923	4.629	17.350	5.578	0.983
	North	- 29.479	6.640	- 0.873	0.769	0.963
	or	- 88.618	6.018	10.043	3.784	0.956
	Both side	- 12.874	3.009	- 5.271	1.238	0.615
	, or	- 75.453	4.653	7.098	3.762	0.785
All		- 28.207	4.059	- 4.968	1.960	0.765

Opening method : South- 30cm, 60cm, 90cm : North- 30cm, 60cm, 90cm
: Both side- 30cm, 60cm, 90cm All : Everything opening method

(11-21(a))

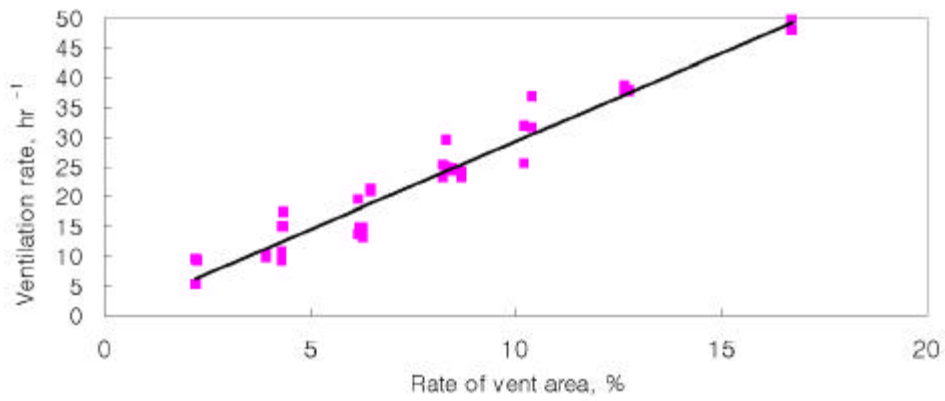
$$S = 3.111(AREA) - 5.511(WIND) + 1.117(TEMP) - 9.217$$

($R^2 = 0.7139$)

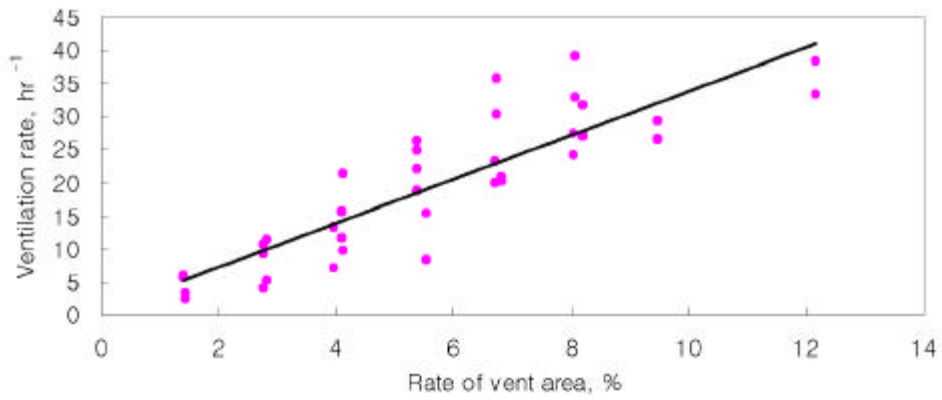
(11-21(b))

$$S = 4.059(AREA) - 4.968(WIND) + 1.959(TEMP) - 28.207$$

($R^2 = 0.7646$)



(a)



(b)

11-21.

4 가

가 , ,
가
. 가 , , ,
,
1998 8 22 9 4 2 , 23 가 .

1. 가

400 1,200 , 648
. 15.8 ,
10 가가 87% .

2.

가.

(95.6%) , 1
. 30.4% , 69.6% .
, 2 , 3
가 13% ,
가 , 가가 ,
가

3 70% 가 ,

가 47.8% .
 (2 , 3) 1.9 71% 가가
 , (1) 1.1 93% 가가
 .
 가 , 60.9% ,
 83% 가 .
 가가 56.5% ,
 ,
 ,
 . 가 (73.9%)
 (21.3%).
 . 가 (34.8%),
 (30.4%), (30.4%), (17.4%) (11- 17).

11- 17.

(%)	34.8	30.4	30.4	17.4	16

3.

가.

1 (82.6%),
 가가 2 . 11- 18

11 56.5% 가 , 가 가
(60.8%).

가 , 20 23 (21.7%) . 가가 60.8%
43.8%, 18 20 21.7% , 13 17
가 가
가 65.2% 가 ,
가 가 (8%).
가 .

11- 18.

	8	9	10	11	12
(%)	13	8	17.4	56.5	4
	()				

가 20
(13%), 25 (26%), 30 (52.2%) 3 (82.6%) 가
, 4 (13%) 5 가 . 150
170cm(56.5%), 120 130cm(34.7%) 14 15cm(60.8%) 10
12cm(21.7%)
25 28 (56.5%) 15 18 (65.2%)
가가 .

가가 ,
25 28 (65.2%),
14 15 (78.3%)

가가

, , , ,
, , 가 , , ,
가
(34.8%), (26%), (13%), ,

가 ,
2 1 6
(34.8%) 가 , 5 (30.4%), 7 (26.1%), 4 (8%)

5

1.

가.

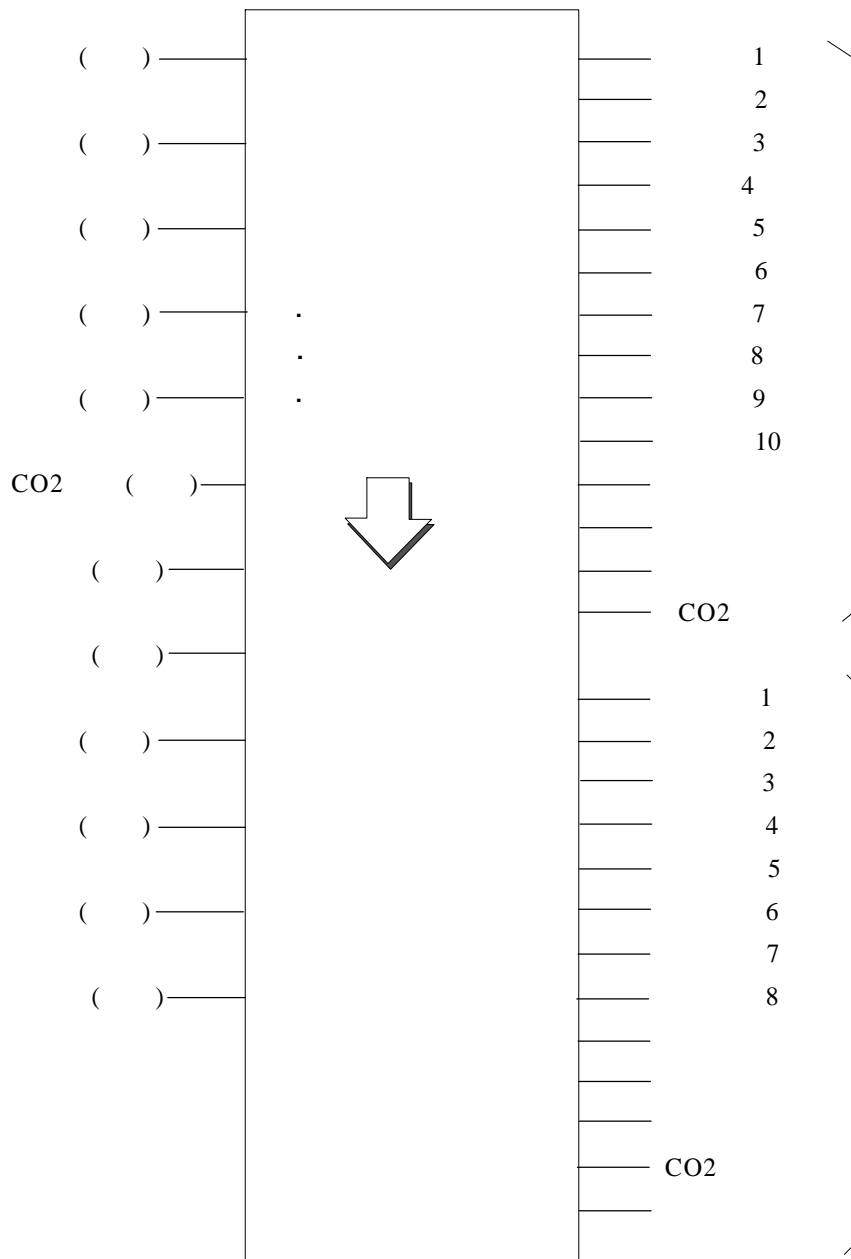
1 2 1

. 3

,
가
가
CO2 가
/ 가
1
CO2 가
(Sensonix, Model GH- 250E)
11- 22

8 (AdvanTech, Model Adam- 4050)
, RS485
multi- drop
가 11- 23
11- 24 11- 25
ON/OFF ADAM- 4050
(Axion Ax756B, Taiwan)
0 가 OFF

11- 26

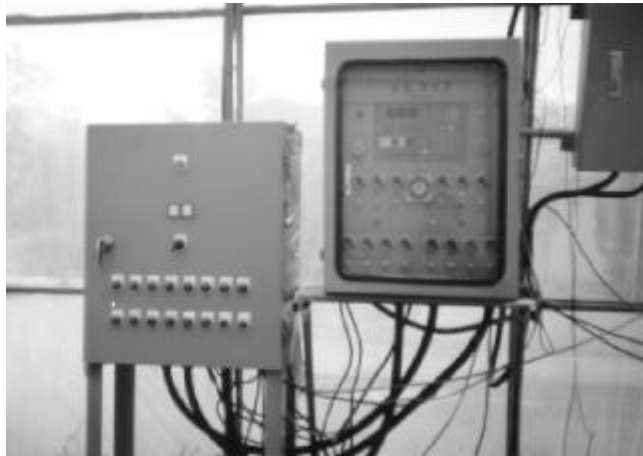


11- 22.

/



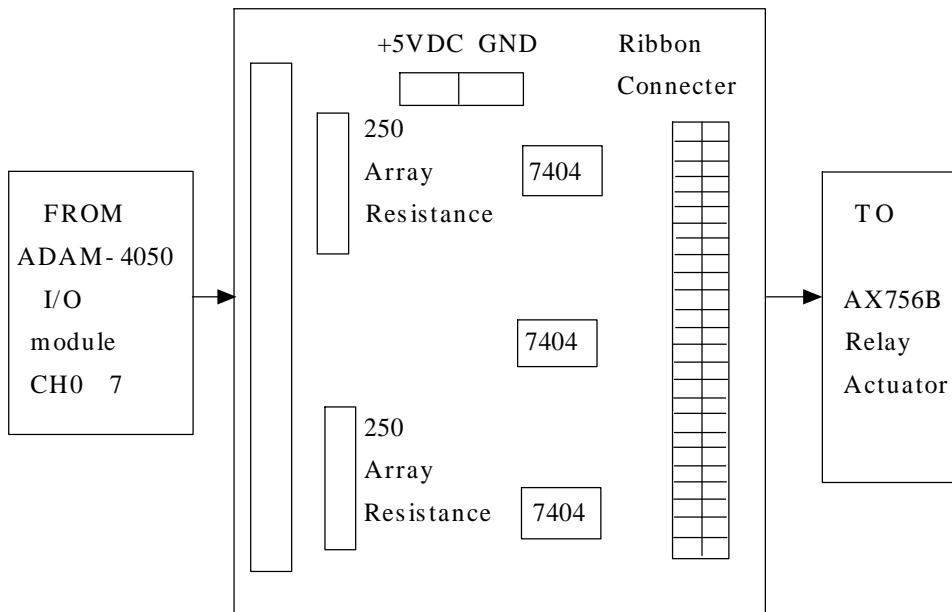
11- 23.



11- 24.



11- 25.



11- 26. TTL

2.

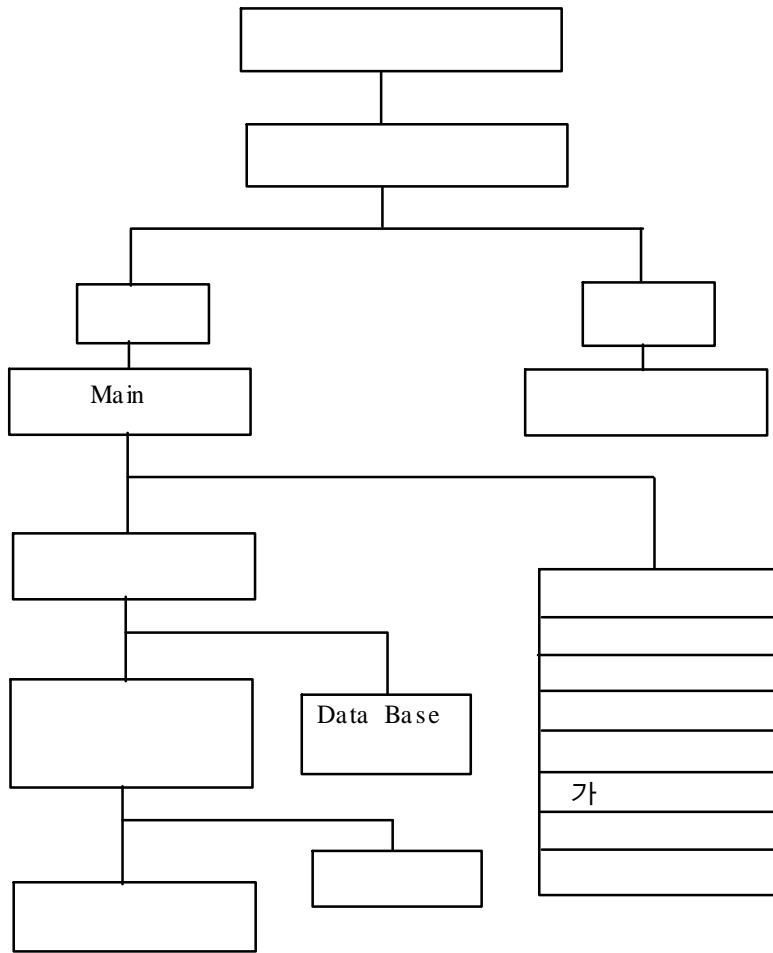
가.

PC
Microsoft Visual Basic 5.0 Windows .
가

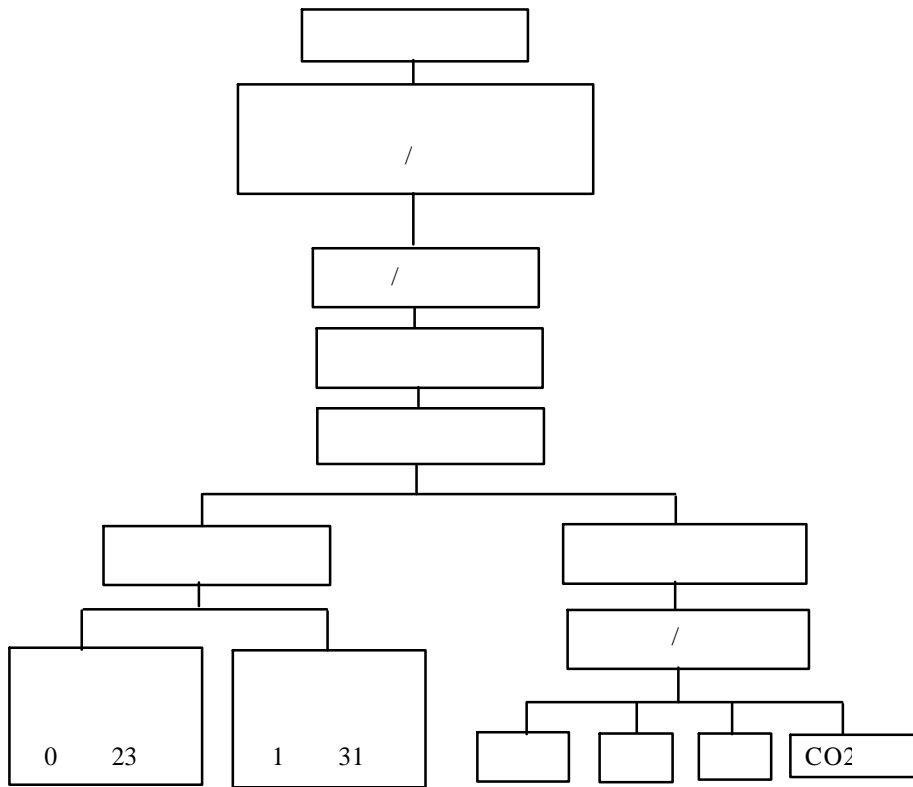
Data Base ,
가

11-27 .

11-28 .



11- 27.



11- 28.

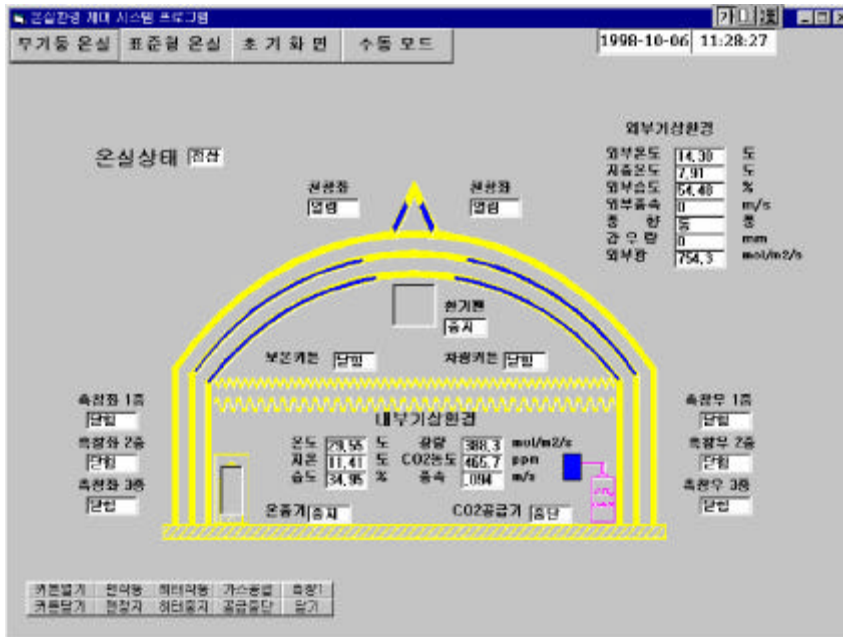
. PC
1)
PC Main
A/D
, , , , , ,
, 가 , 가 가 가 ,
, ,
A/D Main
A/D
11-27 01 12 A/D
, 21 24
10 10
가



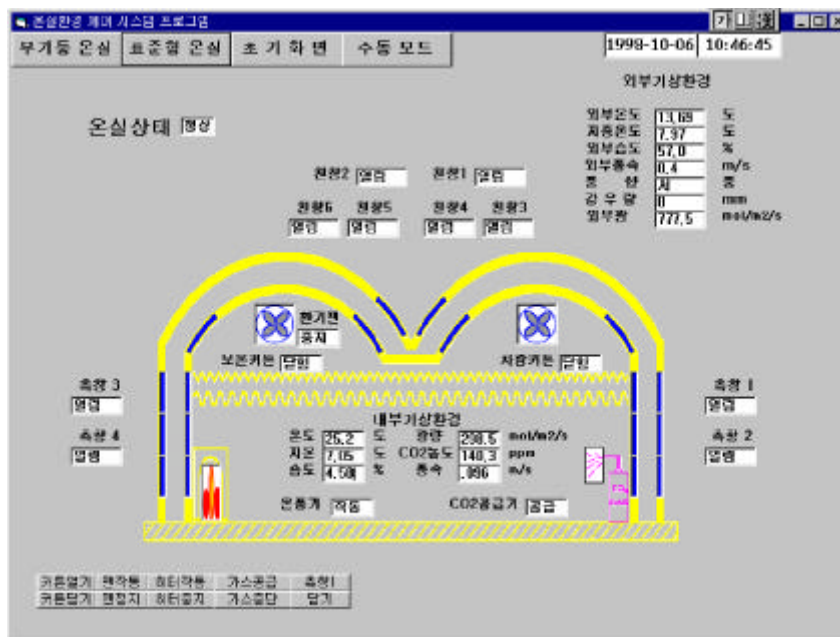
11- 27.

2)

· , , , CO2 ,
 , , CO2 , , ,
 , , , , , , , ,
 (11- 28, 11- 29).
 Main 가 .
 가



11- 28.



11- 29.

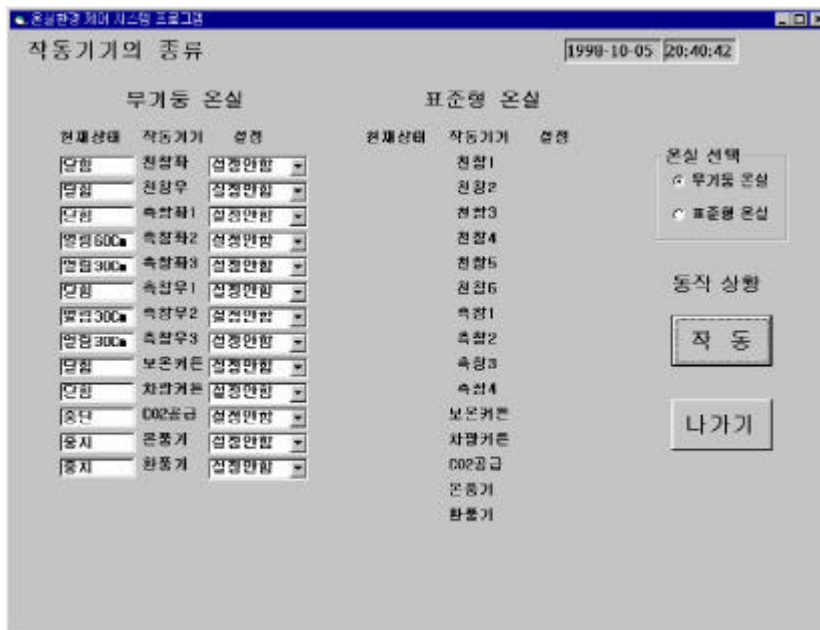
3)

PC

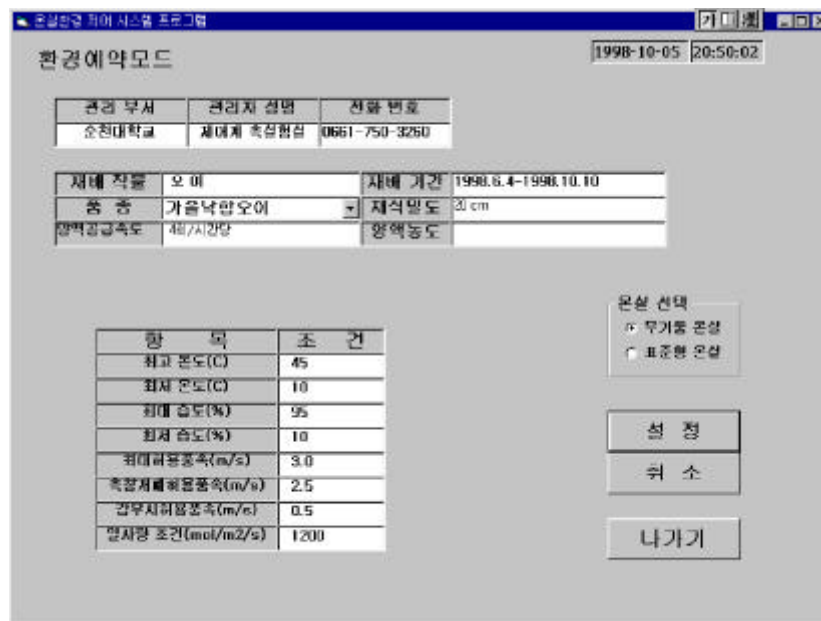
. 11-30
, , 1, 2, 3, 1, 2, 3,
, , CO2 , ,
, 1, 2, 3, 4, 5, 6, 1,
2, 3, 4, , CO2 , ,
. ,
3 , ,
30cm, 60cm, , 30cm, 60cm ,
가

4)

, CO2 ,
, CO2 .
, CO2 Logic
Logic (11-31).



11- 30.



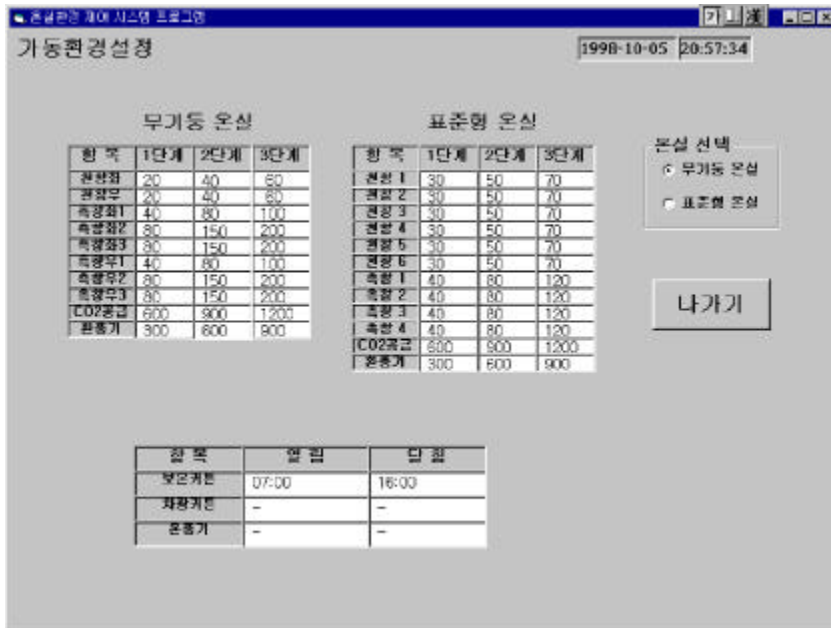
11- 31.

5) 가

1, 2, 3 PC, CO2 ON/OFF (11-32).

6)

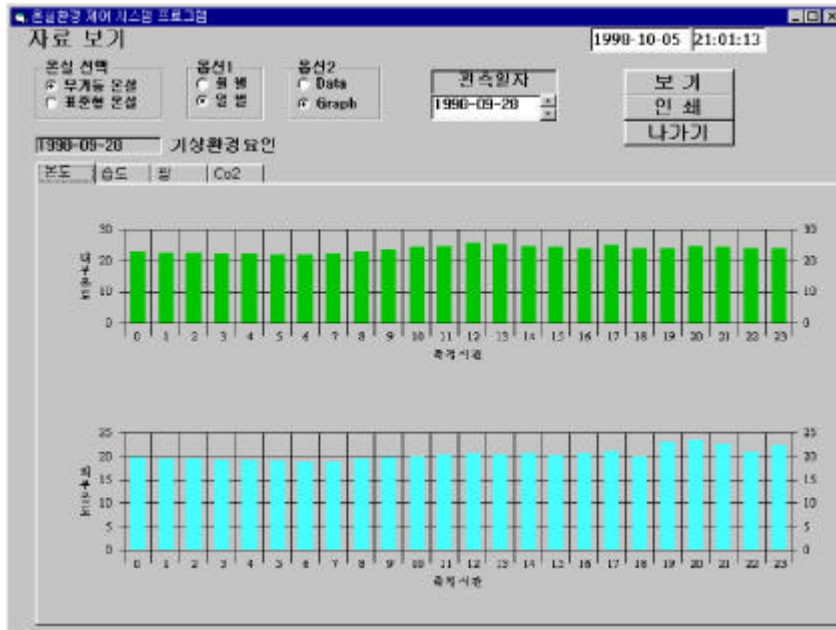
ASCII DB
가
/ / , 1 /
, 2
(11-33, 11-34).
, CO2 ,



11- 32. 가



11- 33. ()



11- 34. ()

7)

, , , ,

(11- 35).



11- 35.

3.

Logic

, PC

가 CO2

RAM

, CO2

Sub Logic 가

Logic Main Logic Sub

Logic Main Logic

, Main Logic 가

Sub Logic 가

Logic

가. 가

가

가

Sub Logic

가

가

가

가

가

가

가

가

가

가

가

Sub Logic

가

, 가

가

가

가

, 가

2

2

Ram

4.

」

가

가

1.

, 1-2W 가 .

1-2W 가 , 6 14

가 1-2W , 7 12

1-2W 가 .

가

, ,

1-2W 가 ,

. 10 4 1-2W 가

, 11 1 .

. , 1-2W

, 가 8 9

2.

(2)

1-2W 20cm 53.7kg 가

, 49.9kg , 1-2W

가 . (5) 1-2W

, , 15cm(34 /bench)

25cm(20 /bench) 가 , 15cm 20cm(26 /bench)

20cm 25cm 가 .

15cm 20cm 25cm ,

15cm 20cm 가 .

15cm 20cm .

3.

, , ,

가

, .

, 가 40% .

20% ,

가 .

. 가 가 , 가

, 가 가

. 가

, . 가

, .

가 , 가 .

, ,

가, , 가 ,
 가, 가

4. , , CO2 가
 10 20 $\mu\text{mol s}^{-1}\text{m}^{-2}$, 700 $\mu\text{mol s}^{-1}\text{m}^{-2}$

$$\text{GPR} = 21.4512 \text{ PPF} / (287.784 + \text{PPF})$$

가 , 24 32 가
 20 40ppm , CO2 1200 1300ppm , CO2

$$\text{GPR} = 15.5554 (1 - 0.9636 \exp(-0.0024 \text{ CO}_2))$$

가 , 가 , 가 ,
 가 logistic

$$\text{GPR} = 24.743 / (1 + 6.0343 \exp(-0.3689 \text{ N}))$$

, , CO2 (GPR)

$$\text{GPR} = 69.4119 \text{T} / (7.5397 + \text{T}) \cdot \text{PPF} / (240.149 + \text{PPF}) \\
 (1 - 0.8865 \exp(-0.0018 \text{CO}_2)) \cdot (1 + 5.1729 \exp(-0.4161 \text{N}))$$

5.

가 ,

(Resp)

$$\text{Resp} = 0.0734 \frac{dW}{dt} + 7.6618 \exp(0.093 \text{temp}) \cdot W$$

14.6%

$$0.5552 \text{g CH}_2\text{O}/(\text{gN})$$

5.

0.3427

(Ws)

(LDW) (t)가

$$\text{LDW} = (0.7372 - 0.00193t) W_s$$

(LAI), (LDW) (PS)

$$\text{LAI} = (11.831 + 1.6832 \text{LDW}) / \text{PS} \quad \text{가}$$

(Pg)

$$P_g = \int_0^{\text{LAI}} \text{GPR} \, dl$$

$$= 69.4119T / (7.5397 + T)(1 - 0.8865 \exp(-0.0018 \text{CO}_2))$$

$$1 / (1 + 5.1729 \exp(1 - 0.4161N)) \cdot \int_0^{\text{LAI}} 1 / (240.1694 + I) dt$$

7. 가 N

가 ,

8. 가 가
4 5 g d-1 가 ,

20 , 2

가

9. 가

가

50%

15%

133mg CH₂O h-1

10.

Simplex

Runge-

Kutta fourth-order

가

simulation 가 73 y gm-2

$$y+ 218.5275= 0.2170 \text{ Rad} + 29.7863 \text{ Temp} + 0.1271 \text{ CO}_2$$
$$+ 0.0032 (\text{Rad})(\text{Temp}) - 0.000034 (\text{Rad})(\text{CO}_2) + 0.00167 (\text{Temp})(\text{CO}_2)$$
$$- 0.000113 (\text{Rad})^2 - 0.4316 (\text{Temp})^2 - 0.00006 (\text{CO}_2)^2,$$

11.

(RS485)

10

MS Visual BASIC

가

가

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A. 가

< | > | _____
 :
 :
 :
 (): _____
 : _____
 (): _____

< | _____ , _____ | > |

1. _____ ? _____
2. () ?
 1 : _____ 2 : _____ 3 : _____ : _____
3. ?
 ()
4. ?
 () : _____
5. (1) ?
 _____m _____m _____m _____m _____
6. ? /
 : _____
7. ?
 () / ()
8. ?
 1 2 3 ()
9. , ? /
10. , , ?
 (- : _____ , : _____m, : _____)
 (- : _____ , : _____m, : _____)
11. ? /
12. ?
 (: _____)
 (: _____)
13. ?
 ()
14. ?

- ()
15. ?
16. ?
17. ?
18. ?
)
)
19. ?
() ()
20. ? ()
21. 가 ? ()
22. CO2 ? /
23. CO2 ? / (: _____ppm)
24. ?
:
:
:
:
- < | > |
25. 2 4 6 ? 9 12
26. () ? _____
27. ?
2 -
4 -
6 -
9 -
12 -
- < | > |
28. : _____ , : _____

29. 가?

30. ?

31. ?

< >

32. () ?

(kg/300)

(300)

(: ____ kg, : ____ kg, : ____ kg, : ____ kg)

33. 가?

15 20 25 30 ()

34. 가? ()

35. ?
_____ cm _____ cm ()

36. ?
(: => :)

37. ? : ____ , : ____

38. ? : ____ % , : ____ %

< >

39. ? (300)

(: ____ kg, : ____ kg, : ____ kg, : ____ kg)

40. 가? /

41. ?
(: _____)

42.

:
) : ____ , : ____ % , : ____) : ____ , : ____ % , : ____
:
) : ____ , : ____ % , : ____) : ____ , : ____ % , : ____
:
) : ____ , : ____ % , : ____) : ____ , : ____ % , : ____

43. ? _____ , _____

44. 가?

45. ? ()

46. ?
()

47. 가 ?
: _____ : _____

48. ? _____

49. ?
()

50. 가 : ?
:
:
:
():

51. :

< | > ? _____

52. ? _____

53. : _____ , : _____ % , : _____

54. 가

B.

```
IMPLICIT DOUBLE PRECISION (A-H,O-Z)
REAL*8 MIN,NL
DIMENSION P(13),FUN(14),STEP(13),S(14,13),PC(13),PR(13)
DIMENSION PE(13),PO(13),W(2,4,6,2),EW(2,4,6,2),DW(2,4,6,2)
DIMENSION EF(2,4,14),DWF(2,4,14),WG(2)
COMMON W,DWF,EW,EF,AC,TEMP,RAD,CO2,NL,NDY
DATA WG/2.0D0,100.0D0/
```

C

C NP : NUMBER OF PARAMETER

C P : PARAMETER VECTOR

C

```
NP=13
```

```
NPS=NP+1
```

C ALP : REFLECTION COEFFICIENT

C BETA : CONTRACTION COEFFICIENT

C GAMMA : EXPANSION COEFFICIENT

C

```
ALP=1.0
```

```
BETA=0.5
```

```
GAMMA=2.0
```

```
MIN=100000.0
```

```
ITR=0
```

C

C PARM.TXT IS A FILE WITH INITIAL VALUES OF P VECTOR AND

C INCREMENT OF P, WHICH IS CALLED STEP

C 982HCL.TXT IS A FILE WITH HOURLY VALUE OF RAD, TEMP,

C CO2 FROM MAR. 7 TO MAY 18.

```
OPEN(5,FILE='PARM.TXT',STATUS='OLD')
```

```
OPEN(6,FILE='SIM.OUT',STATUS='NEW')
```

```
OPEN(10,FILE='982HCL.TXT',STATUS='OLD')
```

```
DO 1 I=1,NP
```

```
READ(5,*)P(I),STEP(I)
```

1 CONTINUE

C

C I=1, 1-2W HOUSE

C I=2, POSTLESS HOUSE

C

```
DO 4 I=1,2
```

```

DO 3 J=1,4
DO 2 K=1,6
READ(5,*)(DW(I,J,K,L),L=1,2),W(I,J,K,2)
W(I,J,K,1)=DW(I,J,K,1)+DW(I,J,K,2)
DO 7 L=1,2
W(I,J,K,L)=W(I,J,K,L)*WG(L)
7 CONTINUE
2 CONTINUE
3 CONTINUE
4 CONTINUE
DO 6 J=1,4
DO 5 K=1,14
5 READ(5,*)(DWF(I,J,K),I=1,2)
6 CONTINUE
C
C S : MATRIX OF SIMPLEX POINTS
C
DO 10 I=1,NP
10 S(1,I)=P(I)
DO 30 I=2,NPS
II=I-1
DO 20 J=1,NP
S(I,J)=P(J)
IF(J.NE.II)GO TO 20
S(I,J)=P(J)+STEP(J)
20 CONTINUE
30 CONTINUE
40 CONTINUE
DO 60 I=1,NPS
DO 50 J=1,NP
50 P(J)=S(I,J)
FUN(I)=F(P)
60 WRITE(6,61)(S(I,J),J=1,NP),FUN(I)
61 FORMAT(4F15.6)
70 ITR=ITR+1
C
C FMAX : MAXIMUM VALUE OF OBJECT FUNCTION
C FMIN : MINIMUM VALUE OF OBJECT FUNCTION
C
FMAX=- 1.0E+10

```



```

    FMIN=1.0E+10
    DO 110 I=1,NPS
    IF(FUN(I).LE.FMAX)GO TO 100
    FMAX=FUN(I)
    IH=I
100  IF(FUN(I).GT.FMIN)GO TO 110
    FMIN=FUN(I)
    IL=I
110  CONTINUE
    DO 90 J=1,NP
    PC(J)=0.0
    DO 80 I=1,NPS
    IF(I.EQ.IH)GO TO 80
    PC(J)=PC(J)+S(I,J)
80   CONTINUE
    PC(J)=PC(J)/NP
90   CONTINUE
    SUM=0.0
    SS=0.0
    DO 112 I=1,NPS
    SUM=SUM+FUN(I)
112  SS=SS+FUN(I)*FUN(I)
    VAR=(SS - SUM*SUM/NPS)/NP
C
C   SD : STANDARD DEVIATION OF OBJECT FUNCTIONS
C
    SD=DSQRT(VAR)
    IF(SD.LT.1.0E- 10)GO TO 270
    DO 120 I=1,NP
120  PR(I)=PC(I)+ALP*(PC(I)- S(IH,I))
    FR=F(PR)
    IF(FR.GE.FUN(IL))GO TO 150
    DO 130 I=1,NP
130  PE(I)=PC(I)+GAMMA*(PR(I)- PC(I))
    FE=F(PE)
    IF(FE.GE.FUN(IL))GO TO 250
    DO 140 I=1,NP
140  S(IH,I)=PE(I)
    FUN(IH)=FE
    GO TO 70

```

```

150  IN=0
      DO 160 I=1,NPS
      IF(LEQ.IH)GO TO 160
      IF(FR.GT.FUN(I))IN=IN+1
160  CONTINUE
      IF(IN.LT.NP)GO TO 250
      IF(FR.GT.FUN(IH))GO TO 180
      DO 170 I=1,NP
170  S(IH,I)=PR(I)
      FUN(IH)=FR
180  CONTINUE
      DO 190 I=1,NP
190  PO(I)=PC(I)+BETA*(S(IH,I)-PC(I))
      FC=F(PO)
      IF(FC.LE.FUN(IH))GO TO 230
      DO 200 I=1,NP
200  P(I)=S(IL,I)
      DO 220 I=1,NPS
      DO 210 J=1,NP
210  S(I,J)=(S(I,J)+P(J))/2.0
220  CONTINUE
      GO TO 40
230  CONTINUE
      DO 240 J=1,NP
240  S(IH,J)=PO(J)
      FUN(IH)=FC
      GO TO 70
250  CONTINUE
      DO 260 J=1,NP
260  S(IH,J)=PR(J)
      FUN(IH)=FR
      GO TO 70
270  WRITE(6,280)ITR,FMIN
280  FORMAT(//10X,'OPTIMIZATION BY NELDER-MEAD METHOD',//,
* 17X,'NO OF ITERATIONS',I4//15X,'MINIMAL FUNCTION VALUE',
* F10.4)
      WRITE(6,290)
290  FORMAT(//10X,'PARAMETER',5X,'ESTIMATED AS')
      DO 300 I=1,NP
300  WRITE(6,310)I,S(IL,I)

```

```

310  FORMAT(/13X,I2,9X,F12.4)
      DO 350 I=1,2
      DO 340 J=1,4
      DO 330 K=1,6
      DO 320 L=1,3
320  WRITE(6,360)I,J,K,L,W(I,J,K,L),EW(I,J,K,L)
330  CONTINUE
340  CONTINUE
350  CONTINUE
360  FORMAT(4I3,2F10.3)
      DO 390 I=1,2
      DO 380 J=1,4
      DO 370 K=1,14
370  WRITE(6,400)I,J,K,DWF(I,J,K),EF(I,J,K)
380  CONTINUE
390  CONTINUE
400  FORMAT(3I3,2F10.3)
      STOP
      END
      DOUBLE PRECISION FUNCTION F(P)
      IMPLICIT DOUBLE PRECISION (A-H,O-Z)
      INTEGER PL, HOUSE
      REAL*8 NL
      DIMENSION P(13),W(2,4,6,2),EW(2,4,6,2),IND1(6),IND2(14)
      DIMENSION Y(10),F1(10),F2(10),F3(10),F4(10),TF(10)
      DIMENSION DWF(2,4,14),EF(2,4,14)
      COMMON W,DWF,EW,EF,AC,TEMP,RAD,CO2,NL,NDY
      DATA IND1/22,29,36,43,50,57/
      DATA IND2/45,47,49,51,53,55,57,59,61,63,65,67,69,73/
      N=10
      H=0.1
      IP=10
      REWIND 10

C
C  Y : THE VECTOR OF THE STATE VARIABLES
C
C  Y(1) : SHOOT DRY WEIGHT (G)
C  Y(2) : ROOT DRY WEIGHT (G)
C  Y(3) : FRUIT DRY WEIGHT (G)
C  Y(4) : CH2O CONTENT IN SHOOT( G CH2O/G DW )

```

```

C   Y(5) : CH2O CONTENT IN ROOT( G CH2O/G DW )
C   Y(6) : CH2O CONTENT IN FRUIT( G CH2O/G DW )
C   Y(7) : SOLUBLE N CONCENTRATION IN SHOOT
C   Y(8) : SOLUBLE N CONCENTRATION IN ROOT
C   Y(9) : SOLUBLE N CONCENTRATION IN FRUIT
C   Y(10): STORAGE CH2O CONTENT IN SHOOT
C   INITIAL VALUES OF STATE VARIABLES ARE AS FOLLOWS
C
10  FORMAT(/1X,'DAY',2X,'SHOOT WT',3X,'ROOT WT'/)
C
C   LDAY  : THE LAST DAY OF SIMULATION
C
      LDAY=73
C   WRITE(7,90)X,Y(4),Y(5)
      DO 104 HOUSE=1,2
      DO 102 PL=1,4
      Y(1)=1.40
      Y(2)=0.28
      Y(3)=0.5
      Y(4)=0.1
      Y(5)=0.05
      Y(6)=0.25
      Y(7)=0.04
      Y(8)=0.025
      Y(9)=0.03
      Y(10)=0.07
      AC=20.0
      K=0
      K1=0
      DO 100 NDAY=1,LDAY
      NDY=NDAY
      TMAX=- 100.0
      TMIN=100
      NL=- 4.1782 + 0.0216*AC
      DO 80 NTIME=1,24
      READ(10,*)TEMP,RAD,CO2
      IF(TEMP.GE.TMAX)TMAX=TEMP
      IF(TEMP.LE.TMIN)TMIN=TEMP
      DO 70 NT=1,IP
      CALL FCN(P,F1,Y)

```

```

C
C CALCULATE F1
C
      DO 20 I=1,N
      F1(I)=H*F1(I)
20    TF(I)=Y(I)+0.50*F1(I)
      CALL FCN(P,F2,TF)
C
C CALCULATE F2
C
      DO 30 I=1,N
      F2(I)=F2(I)*H
30    TF(I)=Y(I)+0.5*F2(I)
      CALL FCN(P,F3,TF)
C
C CALCULATE F3
C
      DO 40 I=1,N
      F3(I)=H*F3(I)
40    TF(I)=Y(I)+F3(I)
      CALL FCN(P,F4,TF)
C
C CALCULATE F4
C
      DO 50 I=1,N
50    F4(I)=H*F4(I)
C
C CALCULATE Y(N+1)
C
      DO 60 I=1,N
      TF(I)=(F1(I)+2.0*F2(I)+2.0*F3(I)+F4(I))/6.0
60    Y(I)=Y(I)+TF(I)
70    CONTINUE
80    CONTINUE
      AC=AC+(TMAX+TMIN)/2.0
      DO 82 I=1,6
      IF(NDAY.EQ.IND1(I))GO TO 84
82    CONTINUE
      GO TO 92
84    K=K+1

```

```

EW(HOUSE,PL,K,1)=Y(1)*2.0D0
C   EW(HOUSE,PL,K,2)=Y(1)*(1.0- (0.7372- 0.00193*NDY))*3.0D0
EW(HOUSE,PL,K,2)=Y(2)*100.0D0
90  FORMAT(I3,10F8.3)
    GO TO 100
92  CONTINUE
    DO 94 I=1,14
    IF(NDAY.EQ.IND2(I))GO TO 96
94  CONTINUE
    GO TO 100
96  K1=K1+1
    EF(HOUSE,PL,K1)=Y(3)
100 CONTINUE
    NDY1=NDAY- 1
    WRITE(6,90)NDAY1,(Y(KK),KK=1,10)
102 CONTINUE
104 CONTINUE
    F=0.0
    DO 140 L=1,2
    DO 130 I=1,2
    DO 120 J=1,4
    DO 110 K=1,6
    F=F+(W(I,J,K,L)- EW(I,J,K,L))*2
110 CONTINUE
120 CONTINUE
130 CONTINUE
140 CONTINUE
    DO 170 I=1,2
    DO 160 J=1,4
    DO 150 K=1,14
150 F=F+(DWF(I,J,K)- EF(I,J,K))*2
160 CONTINUE
170 CONTINUE
    RETURN
    END
    SUBROUTINE FCN(P,F,Y)
    IMPLICIT DOUBLE PRECISION (A- H,O- Z)
    DIMENSION F(10),Y(10),P(13),W(2,4,6,2),EW(2,4,6,2)
    DIMENSION DWF(2,4,14),EF(2,4,14)
    REAL*8 LAI,NRS,NSF,NL

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COMMON W,DWF,EW,EF,AC,TEMP,RAD,CO2,NL,NDY
C
C Y : VECTOR OF THE STATE VARIABLES
C F : VECTOR OF THE DERIVATIVE OF THE STATE VARIABLES
C WL: LEAF WEIGHT
      WL=(0.7372- 0.00193*NDY)*Y(1)
C
C PS : PLANTING SPACE
C
      PS=20.0
      LAI=(11.831+1.6832*WL)/PS
C PG : GROSS PHOTOSYNTHETIC RATE
C EX : EXTINCTION COEFFICIENT
      EX=0.3427
      IF(RAD.EQ.0.0)GO TO 10
      DENO=0.0773*EX*RAD*DEXP(- EX*LAI)+P(4)*0.8583
      PG=P(4)/EX*DLOG((0.0773*EX*RAD+P(4)*0.8583)/DENO)
      PG=PG*TEMP/(7.5397+TEMP)*1.0/(1.0+5.1729*DEXP(- 0.4161*Y(7)))
      PG=PG*(1.0- 0.8865*DEXP(- 0.0018*CO2))
      GO TO 20
10   PG=0.0
C RM : MAINTENANCE RESPIRATION RATE ( G CH2O/G DW/DAY )
C GR : GROWTH RESPIRATION COEFFICIENT ( G CH2O/G DW )
C UR : THE ENERGY COST FOR N UPTAKE ( G CH2O/G N )
C
C      WRITE(*,21)Y(10)
20   PG=PG*(0.3- Y(4))*P(5)
21   FORMAT(F10.3)
C
C F(1) : GROWTH RATE OF SHOOT
C F(2) : GROWTH RATE OF ROOT
C F(3) : GROWTH RATE OF FRUIT
C
      F(1)=P(1)*Y(4)*Y(7)*Y(1)
      F(2)=P(2)*Y(5)*Y(8)*Y(2)
      F(3)=P(3)*Y(6)*Y(9)*Y(3)
      IF(NL.LT.9.0)F(3)=0.0
22   FORMAT(2X,'GROWTH RATE',3F10.3)
C
C RS : SHOOT RESPIRATION RATE

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C RR : ROOT
C RF : FRUIT
C

$$RS=0.0734 * F(1) + 0.000229 * \text{DEXP}(0.093 * \text{TEMP}) * Y(1)$$

$$RR=0.1002 * F(2) + 0.000229 * \text{DEXP}(0.093 * \text{TEMP}) * Y(2)$$

$$RF=0.075 * F(3)$$

$$RS=(0.15 + 3.571233 * Y(10)) * RS$$
C
C UN : NITROGEN UPTAKE RATE
C RN : ENERGY COST FOR NITROGEN UPTAKE
C

$$UN=P(6) * (0.15 - Y(8)) * Y(2) * Y(5) * 11.0 / (11.0068 * (P(7) + Y(5)))$$

$$RN=0.552 * UN$$

$$RR=RR+RN$$
C
C TCR : TRANSLOCATION RATE OF CH₂O FROM SHOOT TO ROOT
C TCF : TO FRUIT
C

$$TCR=P(8) * Y(4) * (0.1 - Y(5))$$

$$TCF=P(9) * Y(4) * (0.40 - Y(6))$$
C
C US : UTILIZATION OF SOLUBLE CH₂O FOR SHOOT GROWTH
C UR : ROOT
C UF : FRUIT
C

$$US=0.92 * F(1)$$

$$UR=0.92 * F(2)$$

$$UF=0.92 * F(3)$$
C
C USN : UTILIZATION OF SOLUBLE N FOR SHOOT GROWTH
C URN : ROOT
C UFN : FRUIT
C

$$USN=0.015 * F(1)$$

$$URN=0.015 * F(2)$$

$$UFN=0.015 * F(3)$$
C
C D : SHOOT DEMAND FOR CH₂O
C FCS : PARTITIONING OF CH₂O TO STARCH POOL
C FSC : FLOW CH₂O FROM STARCH POOL TO SOLUBLE CH₂O


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C
  D=RS+US+TCR+TCF+Y(4)*F(1)
  FCS=P(10)*Y(4)*(0.35- Y(10))
  IF(RAD.EQ.0.0)FCS=0.0
  FSC=0.0
  IF(RAD.EQ.0.0)FSC=P(11)*D*(0.3- Y(4))*Y(10)
C
C DSN : NITROGEN DEMAND FOR SHOOT GROWTH
C NRS : NITROGEN TRANSLOCATION RATE FRON ROOT TO SHOOT
C DFN : NITROGEN DEMAND FOR FRUIT GROWTH
C NSF : NITROGEN TRANSLOCATION RATE FRON SHOOT TO FRUIT
C
  DSN=(0.015+Y(7))*F(1)
  NRS=P(12)*(0.15- Y(7))*Y(8)
  DFN=(0.015+Y(9))*F(3)
  NSF=P(13)*(0.15- Y(9))*F(3)
  IF(NL.LT.9.0)NSF=0.0
C
C F(4) : RATE OF CHANGE OF SHOOT CH2O
C F(5) :                               ROOT
C F(6) :                               FRUIT
C
  F(4)=(PG- RS- US- FCS+FSC- TCF- TCR- Y(4)*F(1))/Y(1)
  F(5)=(TCR- RR- UR- Y(5)*F(2))/Y(2)
  F(6)=(TCF- UF- RF- Y(6)*F(3))/Y(3)
C
C F(7) : RATE OF CHANGE OF SHOOT SOLUBLE N
C F(8) :                               ROOT
C F(9) :                               FRUIT
C
  F(7)=(NRS- USN- NSF- Y(7)*F(1))/Y(1)
  F(8)=(UN- URS- URN- Y(8)*F(2))/Y(2)
  F(9)=(NSF- UFN- Y(9)*F(3))/Y(3)
C
C F(10) : RATE OF CHANGE OF SHOOT STORAGE CH2O
C
  F(10)=(FCS- FSC- Y(10)*F(1))/Y(1)
  RETURN
  END

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